FINAL
TECHNICAL MEMORANDUM NO. 4
SITE MODEL FOR HYDROGEOLOGIC/
CONTAMINATION DISTRIBUTION
FOR TRENCH T-3; IHSS 110; OU-2
OU-2 SUBSURFACE IM/IRA
SOIL VAPOR EXTRACTION PILOT TEST
SITE NO. 1

VOLUME 1
TEXT AND FIGURES

Rocky Flats Environmental Technology Site

(Operable Unit No. 2)

U.S. DEPARTMENT OF ENERGY

Rocky Flats Environmental Technology Site Golden, Colorado



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RF/ER-95/0073.UN EG&G ROCKY FLATS ENVIRONMENTAL Manual: Final **TECHNOLOGY SITE** Revision No.: i of xix Final OU-2 Subsurface IM/IRA Page: Operable Unit No. 2 Closure Organization: Technical Memorandum No. 4 May 26, 1995 Effective Date: APPROVED BY: 5-26-95 Project Manager **Environmental Restoration** APPROVED BY: FETR ANNETTE PRIM ROSE Date Department/Group Manager **Environmental Restoration** APPROVED BY:

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LIST OF ACRONYMS

μg/l micro

micrograms per liter

1,1-DCE

1,1-dichloroethene

1,1,1-TCA

1,1,1-trichloroethane

1,2-DCA

1,2-dichloroethane

1,2-DCE

1,2-dichloroethene

ASTM

American Society for Testing and Materials

BGS

below ground surface

BH

borehole

Ca

calcium

CCl₄

carbon tetrachloride

CEARP

Comprehensive Environmental Assessment & Response Program

CHCs

chlorinated hydrocarbons

CHCl₃

chloroform

CH₂Cl₂

methylene chloride

COCs

chemicals of concern

DNAPL

Dense Non-aqueous Phase Liquid

DOE

Department of Energy

EM

electromagnetics

EPA

Environmental Protection Agency

ERM

Environmental Restoration Management

GC/MS

gas chromatography/mass spectrometry

gpm

gallons per minute

GPR

ground-penetrating radar

GSSI

Geophysical Survey Systems, Inc.

HRR

Historical Release Report

HSU

hydrostratigraphic unit

IHSS

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IM/IRAP Interim Measures/Interim Remedial Action Plan

K hydraulic conductivityKa Arapahoe FormationKl Laramie Formation

LHSU lower hydrostratigraphic unit

mg/kg milligrams per kilogram
mg/l milligrams per liter

Mg magnesium
MSL mean sea level

Na sodium

NA not applicable

NAPL Non-aqueous Phase Liquid

OVM organic vapor monitor

PAH polynuclear aromatic hydrocarbon

PCB polychlorinated biphenyl

PCE tetrachloroethene

pCi/g picocuries per gram

PID photoionization detector

ppm parts per million
Pu-239/240 plutonium-239/240
Pu-239 plutonium-239

Qc colluvium

Qrf Rocky Flats Alluvium

RCRA Resource Conservation and Recovery Act

RFA Rocky Flats Alluvium

RFEDS Rocky Flats Environmental Database System

RFETS Rocky Flats Environmental Technology Site

RFFO Rocky Flats Field Office

RFI/RI RCRA Facility Investigation/Remedial Investigation

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RFP Rocky Flats Plant

RI remedial investigation

SAP Sampling and Analysis Plan

SGS Soil Gas Survey

SPSH Six Phase Soil Heating

SOP Standard Operating Procedure

SVE Soil Vapor Extraction

SVOC semivolatile organic compound

TCE trichloroethene

UHSU Upper Hydrostratigraphic Unit

VOC volatile organic compound

VOACLP Volatile Organic Analysis Contract Laboratory Procedure

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EXECUTIVE SUMMARY

Technical Memorandum No. 4 was prepared to assemble and evaluate historical, geological, hydrogeological, and chemical data collected for Trench T-3, Individual Hazardous Substance Site (IHSS) 110, in support of the Operable Unit Number 2 (OU-2) Subsurface Interim Measures/Interim Remedial Action (IM/IRA).

Based on information contained in the Historical Release Report (DOE 1992a), sanitary sewage sludge contaminated with uranium and plutonium and flattened drums potentially contaminated with uranium were reportedly buried in the east trenches, which included Trench T-3. On at least one occasion, it is also believed that 2,400 gallons of water and lathe coolant was possibly disposed of in the east trenches. It is unknown whether this disposal was a direct discharge or the waste was containerized. Trench T-3 was used for disposal purposes from 1955 to 1968 (DOE 1992a). Geological and geophysical data indicate that Trench T-3 is approximately 5 to 10 feet deep, 135 to 140 feet long, and ranges in width from 19 to 23 feet.

The uppermost geologic unit in the vicinity of Trench T-3 is the Rocky Flats Alluvium (RFA), an alluvial fan deposit approximately 15 feet thick beneath Trench T-3. A laterally extensive caliche layer exists in the RFA on the north side of Trench T-3. This caliche layer has the potential to minimize vertical migration of precipitation in this area. However, the caliche layer was disturbed during the excavation of Trench T-3 and could enhance the vertical migration of precipitation through the trench. The RFA is underlain by the Arapahoe Formation, which consists of claystone beneath the west end of Trench T-3, and sandstone (No. 1 Sandstone) beneath the east end. The Arapahoe Formation No. 1 Sandstone ranges in thickness from approximately 20 to 35 feet in the vicinity of Trench T-3. Results of hydraulic conductivity testing conducted on samples collected in the vicinity of Trench T-3 ranged from 6.60E-04 cm/sec to 9.40E-08 cm/sec.

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The upper hydrostratigraphic unit (UHSU) in the vicinity of Trench T-3 consists of saturated portions of the RFA and/or the Arapahoe Formation No. 1 Sandstone. During most of the year, the RFA beneath Trench T-3 is dry, and the uppermost saturated unit of the UHSU is the Arapahoe Formation No. 1 Sandstone. However, during high groundwater level periods (such as second quarter of 1992), the RFA may become saturated beneath Trench T-3. Due to fluctuating groundwater levels, depth to UHSU groundwater beneath Trench T-3 varies between 10 to 30 feet bgs. The yearly average is 23 ft bgs (as measured during 1992). The groundwater flow direction in the RFA in the vicinity of Trench T-3 is primarily to the northeast along the medial bedrock paleoscour. The groundwater flow direction in the No. 1 Sandstone in the vicinity of Trench T-3 is primarily to the north.

Void spaces and flattened drums were observed in boreholes which were drilled and abandoned during the Trench T-3 drilling and characterization investigation in November 1994. Void spaces were observed in boreholes 25194 and 25294 at depths from 4 to 5.3 feet bgs and 4 to 6.5 feet bgs, respectively. Flattened drums were encountered in boreholes 25294, 25494, 25594, and 25694. Electromagnetic geophysical surveying also identified potential metallic objects below grade.

Subsurface soil analytical data and soil gas survey data collected from Trench T-3 indicate that the trench contains volatile organic compound (VOC) contamination (1,1,1-TCA, 1,2-DCA, CCl₄, CHCl₃, PCE and TCE). Trench T-3 appears to be a source of CCl₄, CHCl₃, PCE and TCE to the UHSU groundwater. These VOCs are observed primarily in the No. 1 Sandstone groundwater flow system north of Trench T-3. Concentrations of VOCs in subsurface soils decrease with depth to the water table. The soil gas survey data collected in Trench T-3 indicate that a CCl₄ soil gas plume is located in the west end of the trench. PCE and TCE soil gas plumes are located in the west-central part of the trench.

Minor contamination consisting of polynuclear aromatic hydrocarbons (PAHs), other semivolatile organic compounds (SVOCs), and low concentrations of Aroclor-1254 also exists

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at Trench T-3. Concentrations of arsenic, lead, and silver were observed above background in soil samples collected from within Trench T-3. Activities of Am-241, Pu-239/240, U-233,-234, U-235 and U-238 above background were observed in the soil samples collected from within Trench T-3.

Non-aqueous phase liquid (NAPL) was observed in subsurface materials at several locations within Trench T-3. During drilling of borehole 25194 in the western portion of Trench T-3, a void space filled with liquid was encountered at an approximate depth of 4 to 5.3 feet. Samples showed a stratified liquid in three distinct layers; a black floating layer on top; a yellowish-brown layer in the middle; and a black sinking layer on the bottom. Analytical testing performed on the floating and middle layers indicated the presence of chlorinated hydrocarbons (e.g., PCE), PAHs, phenols, phthalates, and organic hydrocarbons in the gasoline range (C₆ through C₁₂) and the diesel range (C₁₂ through C₂₄). In addition to these organic compounds, elevated activities (ranging from approximately 100 to 3,250 pCi/g) of the uranium-isotopes (U-233,-234, U-235, and U-238) were observed in the liquid collected from borehole 25194. Am-241 and Pu-239/240 activities were approximately 1 pCi/g in the liquid collected from borehole 25194.

NAPL was also observed in several additional boreholes. A yellowish-brown liquid suspected to consist of free-phase chlorinated hydrocarbons (CHCs) observed in borehole 10191 at an approximate depth of 2.8 feet. This borehole is located in the western portion of Trench T-3. Residual NAPL was observed in borehole 24793 at an approximate depth of 6.5 to 10 feet. The liquid observed in borehole 10191 was similar in appearance to the liquid observed in 25194. Residual NAPL was also observed in boreholes 25594 and 25694 at depths of 7 to 16 feet BGS and 11.8 to 12 feet BGS, respectively. NAPL in these two borings appeared as black asphalt-like lumps that impregnated the soil matrix and coated the gravels. A clear liquid was encountered at an approximate depth of 2.5 feet on the downhole equipment during the installation of three monitoring probe locations (APM20, APM24 and APM25).

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To evaluate possible remedial technologies that may be applicable to NAPL occurring at Trench T-3, a distillation test was conducted on a liquid sample collected from borehole 25194. The distillation test was conducted to identify the boiling range and chemical makeup of the liquid collected from borehole 25194 with respect to temperature.

Based on the field investigations and testing conducted at the site, an overview of potential contaminant pathways was developed for Trench T-3. The primary migration pathway for contaminants found in the trench occurs vertically through the vadose zone beneath the trench to the UHSU groundwater and then laterally within the saturated alluvium, when present, and within the No. 1 Sandstone. The VOCs in UHSU groundwater migrate to the north-northeast in the No. 1 Sandstone and potentially discharge at seeps in the South Walnut Creek Drainage. Contaminant migration in the South Walnut Creek Drainage may occur in groundwater seeps in the colluvium on the north facing slope towards Ponds B-1 and B-2. The contaminants may then discharge to the ground surface then flow downslope towards Ponds B-1 and B-2, or the contaminants may discharge directly from the No. 1 Sandstone into Ponds B-1 and B-2.

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1.0 INTRODUCTION

1.1 PROJECT OVERVIEW

In September 1992, the U.S. Department of Energy/Rocky Flats Office (DOE/RFO) released a Final Subsurface Interim Measures/Interim Remedial Action Plan (IM/IRAP) for investigating the removal of suspected volatile organic compound (VOC) contamination in the subsurface within three areas of Operable Unit Number 2 (OU-2) at the Rocky Flats Plant (RFP), subsequently renamed the Rocky Flats Environmental Technology Site (RFETS). Specifically, the OU-2 Subsurface IM/IRAP identified Soil Vapor Extraction (SVE) as an applicable technology for remediation of VOCs at the 903 Pad, Mound and East Trenches Areas. The IM/IRAP specified activities for investigation of the effectiveness of the SVE technology by pilot testing conventional and enhanced systems, and was designed to gain site-specific remedial information to support final remedial actions at OU-2.

The location for Pilot Test Site No. 1 (Site No. 1), of the Pilot Test Program, was selected within Individual Hazardous Substance Site (IHSS) 110 (also known as Trench T-3) located in the East Trenches Area of OU-2. Figure 1.1-1 provides the locations of IHSS 110 in relation to the other IHSS's at OU-2 and the RFETS facility. The location was selected based on soil gas survey results that indicated subsurface VOC contamination was present at sufficient levels to provide a meaningful evaluation of the SVE technology performance. A series of pilot tests conducted at Site No. 1 employed a conventional SVE system utilizing granular activated carbon (GAC) as an off-gas treatment system. Individual pilot tests were conducted in the Rocky Flats Alluvium and the No. 1 Sandstone Unit geologic units at Site No. 1. The Draft Test Site No. 1 Test Report (DOE 1994a) provides the results of those tests.

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1.2 TECHNICAL MEMORANDUM OBJECTIVE

The purpose of Technical Memorandum (TM) No. 4 is to assemble and provide an evaluation of the most current geologic and contamination distribution data for the Northeast Trenches, and particularly Trench T-3, IHSS 110.

1.3 ORGANIZATION

The following is a brief summary of the TM No. 4 document organization:

1.0 Introduction

This section presents a project overview, and includes the TM No. 4 objectives and organization.

2.0 Site Characteristics

This section contains background information on IHSS 110, and presents and evaluates the most current available data for the site.

3.0 Contaminant Migration Pathways

This section discusses potential contaminant migration pathways for IHSS 110 based on the available data for the site.

4.0 Summary

This section summarizes the physical parameters and chemical data for Trench T-3.

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5.0 References

This section contains the references cited in this report.

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2.0 SITE CHARACTERISTICS

Trench T-3 (IHSS 110) is located north of Central Avenue, east of the inner fence, and south of South Walnut Creek at the RFETS. The following sections present the trench operational history and field investigations performed to date to characterize the trench, including the Test Site No. 1 optimization drilling results; geology of the trench; hydrogeology; nature and extent of contamination; results of geophysical surveys conducted; and the three-dimensional visualization efforts conducted for the area around the trench.

2.1 SITE HISTORY

The site history presented in this section is based on information presented in the Historical Release Report (DOE 1992a).

Trench T-3 (IHSS 110) was used primarily for the disposal of sanitary wastewater treatment plant sludge and operated sometime during the period of July 2, 1955, through August 14, 1968. The sludge removed from the RFETS wastewater treatment plant was first placed on sludge drying beds and, once dried, was removed and placed in a number of disposal trenches on site (Trench T-2 and the East Trenches [Trenches T-3 through T-11]). The trenches are reported to be approximately 10 feet deep with two feet of soil cover. It was reported that the estimated amount of sludge disposed in Trenches T-2 through T-11 was 125,000 kilograms (kg). Some uranium and plutonium contamination was present in this sludge. It was reported that the older sludge had primarily uranium contamination with newer sludge having an increased amount of plutonium contamination. Total long-lived alpha activity present in the sludge was reported between a minimum of 382 picocuries per gram (pCi/g) in August 1964 and a maximum of 3,591 pCi/g in June 1960. It has not been determined whether the sanitary sludge contained other contaminants such as VOCs. Since the RFETS wastewater treatment plant received influent from the entire site, it is possible that VOCs (e.g., degreasing/cleaning solvents) were discharged to the treatment plant, introduced to the

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system from direct disposal in sinks and drains in laboratory, production, and/or maintenance areas of the plant site resulting in potential VOC contamination of treatment plant sludge.

Past operational practices at RFETS also included the burning of oils contaminated with uranium in open pits located on the plant site. Drums were used and reused to transport waste oils from various facility operations on the plant site to the oil burn pits, where the oils were dumped and ignited. The materials contained in the drums were machining coolants, still bottoms, and waste oils from facility operations. Although Trench T-3 was not operated as an oil burn pit, the drums which transported the waste oils were flattened and buried in the trench. The total number of flattened drums disposed of in the trenches is estimated at up to 300, and could be present in any of the East Trenches or Trench T-2. It is unknown how much residual material may have remained in the drums at the time of burial, or whether machining and waste oils transported in the drums contained other waste constituents such as organic solvents used to clean machined parts and tools.

In addition, on at least one occasion, it is believed that 2,400 gallons of water and lathe coolant were also disposed of in either Trench T-3 or one of the other disposal trenches in the area. It is unknown whether or not the material was discharged directly or disposed of in drums. The waste coolant was generated in Building 444 from the machining of depleted uranium and had an average activity of 150,000 dpm/l, believed to be total alpha activity. The activity of this material was reported as 1.35 x 108 dpm with approximately 1.3 kg of depleted uranium present in the waste. The radionuclide screen performed on a NAPL sample collected from borehole 25194 in the western portion of the trench in November 1994 indicated a gross alpha activity of 749,000 pCi/l (1.65 x 106 dpm/l) and a gross beta activity of 803,000 pCi/l (1.77 x 106 dpm/l). (Refer to Section 2.6.4 for further discussion).

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2.2 SITE INVESTIGATIONS

Numerous site investigations have been performed at OU-2 to define the nature and extent of contamination from past waste disposal practices discussed in Section 2.1. The investigations have identified Trench T-3 as a source of VOCs to the surrounding subsurface soils and the upper hydrostratigraphic unit (UHSU) groundwater. These investigations included the following:

- Phase I Resource Conservation and Recovery Act (RCRA) Facility Investigation/Remedial Investigation (RFI/RI) conducted in 1987.
- Phase II Alluvial and Bedrock RFI/RIs conducted in 1991, 1992, and 1993, respectively.
- Two soil gas surveys conducted in 1993.
- The SVE Pilot Test Site No. 1 program conducted in 1993 and 1994.
- Additional Trench T-3 drilling characterization investigation conducted in 1994.

The Phase I RFI/RI involved drilling and sampling of two boreholes in and around Trench T-3 (BH3897 and BH4087). The Phase II (Alluvial) RFI/RI included the drilling and sampling of one borehole (10191) in Trench T-3 and the installation of two groundwater plume characterization wells (02991 and 12191) south of Trench T-3. The Phase II (Bedrock) RFI/RI investigation included the drilling and sampling of one pilot borehole (21693), one lower hydrostratigraphic unit (LHSU) monitoring well (23293), and one abandoned monitoring well (22493) north of Trench T-3. The SVE Pilot Test Site No. 1 investigation consisted of drilling and sampling of two boreholes and nine groundwater monitoring wells

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installed near Trench T-3 (24093 through 25093). Constituents analyzed included VOCs, SVOCs, pesticides/PCBs, metals, and radionuclides. The two soil gas surveys included sampling of near-surface and deeper (5- to 10-foot sampling interval) subsurface soil gas in and around Trench T-3 (including IHSSs 109, 111.1, 112, and 113). Additional Trench T-3 drilling characterization investigation consisted of drilling and sampling six boreholes and the conversion of one borehole to a NAPL extraction well in Trench T-3 (25194 through 25694). VOCs, SVOCs, TPH and selected radionuclide analyses were performed on the subsurface soil and NAPL samples collected during the Trench T-3 drilling characterization investigation conducted in 1994. Section 2.2.1 discusses the drilling and sampling during the Trench T-3 drilling characterization investigation. The evaluation of site geology (Section 2.4) and site hydrogeology (Section 2.5) presented in this document is based on information collected during the investigations listed above. Section 2.6 discusses the nature and extent of contamination identified from these investigations.

2.2.1 Additional Trench T-3 Drilling Characterization Field Activities and Sample Analyses

To investigate the NAPL, or liquids, encountered in Trench T-3 during previous field activities and to characterize the western portion of Trench T-3, six boreholes were drilled between Alluvial Pressure Monitor (APM) 25 and borehole 10191 in November 1994. One of the boreholes drilled was converted to a NAPL extraction well. Figure 2.4-1 shows the locations of these boreholes and the extraction well. Borehole logs are presented in Appendix A1.

Drilling and sampling of each soil borehole was performed using hollow-stem augers in compliance with RFETS SOP GT.02, Drilling and Sampling Using Hollow Stem Auger Techniques. Boreholes were to be drilled to an approximate depth of 10 feet BGS using 3.5-inch inside diameter (ID) hollow stem augers. Variation in the drilling depths are discussed in the borehole drilling summaries. Boreholes were continuously sampled to the total depth

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using a 2-foot split spoon sampler. Discrete samples were collected for volatile organic analysis (VOA) by EPA Method 8240 using stainless-steel liners inside the split spoon. The two VOA samples exhibiting the highest organic volatile meter (OVM) reading were selected for analysis from each borehole. If no organic compounds were detected by the OVM, VOA samples were planned for collection from the 5-foot and 10-foot intervals. One composite sample for total organic carbon (TOC) analysis was planned for collection from each borehole over a 2-foot interval. Samples for radionuclide screening were collected for each sampling interval. Samples for semivolatile organic compound (SVOC) analysis by the EPA Method 8270 were planned for collection at 5-foot and 10-foot intervals in each borehole. Samples for total petroleum hydrocarbons (TPH) analysis by EPA Method 8015 were planned for collection if discolored or stained soil was encountered in the borings. The geotechnical analysis, soil moisture content, was to be performed on selected samples depending on the amount of core recovered. All samples were collected in the field according to RFETS SOP FO.13, Containerization, Preservation, Handling, and Shipping of Soil and Water Samples. Table 2.2-1 provides a summary of soil samples collected and analyses requested. Laboratory analytical results are discussed in Section 2.6-4 and presented in Appendix C5-1 through C5-3.

Following the drilling and sampling, the boreholes were abandoned in accordance with RFETS SOP GT.5, Abandonment and Plugging of Boreholes. However, if void spaces were encountered or the borehole failed to be filled with the grout in the subsurface during the drilling of the borehole, the borehole was plugged at an approximate depth of 2 to 3 feet bgs. The plug was constructed by fabricating a 2- to 3-foot long metal rebar cage. The steel rebar cage was placed in the borehole to approximate depth of 2 feet below ground surface then a cement/bentonite grout was placed into the cage to the ground surface. The plug was intended to prevent the closing of the void space and to allow for later removal of the plug, if necessary.

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The following is a description of the drilling and sampling of each borehole within Trench T-3 during the drilling characterization investigation that occurred in November 1994.

Borehole 25194

Borehole 25194 was drilled and sampled to a depth of 4 feet below ground surface (BGS). Upon removal of the core barrel from the 2- to 4-foot sampling interval, liquid was observed dripping from the core barrel (OVM reading of 659 ppm). The borehole was measured to a depth of 5.3 feet BGS and liquid was observed to be dripping from the measuring tape when removed. The 1.3 feet difference between the drilling depth and the measure depth is believed to be due to a void space below grade in the trench. A four foot long, two-inch diameter clear teflon sample bailer was lowered down the borehole to collect a grab sample of the liquid. When the bailer was removed it was approximately half full with stratified liquid. Four stratified layers (Figure 2.2-1) were observed:

- very viscous black layer on the bottom
- yellowish-brown and less viscous layer in the middle
- clear layer above the yellowish-brown
- black layer on top

Additional grab samples of the liquid were collected from the borehole for chemical analysis. Field measurements of the liquid by the OVM were off the scale of the instrument (i.e., greater than 2,000 ppm). The radionuclide screen sample was submitted to the Building 371 laboratory for analysis. Prior to shipment off-site, the radionuclide screen results showed total alpha activity of 749,000 pCi/L and total beta activity of 803,000 pCi/L. Upon receipt of the sample at the laboratory, two separate layers remained. The laboratory performed analytical testing using EPA Methods 8260, 8270, and modified 8015 on the top layer (i.e., floating) and the middle layer (i.e., aqueous layer) separately.

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An extraction well was constructed in borehole 25194 with the installation of approximately 4 feet of 4-inch diameter schedule 40 PVC casing and two feet of 4-inch diameter screen with 0.05 inch slots. One centralizer was placed on the outside of the casing at a depth of 2 to 2.5 feet BGS, which was above the liquid in borehole 25194. Empty concrete bags were packed above the centralizers. Then approximately 1.5 feet of bentonite pellets were placed above the bags. The bentonite pellets were hydrated with 5 gallons of potable water. Concrete was then placed above the grout to the ground surface. No filter pack was placed in this borehole. Protective casing was installed.

The following is a summary of the additional sampling and analysis requested for the liquid collected in December 1994 from extraction well 25194:

- The liquid sample was collected from extraction well 25194 using a clear 4foot, 2-inch diameter bailer. The liquid in the bailer was stratified into two
 distinct layers, a floating black layer on the top [referred to as the floating
 layer (1), sample number C0639] and a yellowish-brown layer on the bottom
 (referred to as the aqueous layer, sample number C0640). The two layers were
 decanted separately into the appropriate sample containers. A radionuclide
 screen analysis was performed prior to shipment.
- During shipment of sample number C0640 to the laboratory, the original sample stratified into a top [referred to as floating (2)] and bottom layer.
 Table 2.2-2 presents the sample number, corresponding laboratory sample number, sample description, and the requested analysis for the three different samples.
- In addition to the requested analysis, a distillation test was performed on sample number C0640. No distillation tests were performed on sample

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number C0639. The following presents the procedures used to perform the distillation analysis.

- The sample was delivered to the laboratory.
- Two liters of initial sample were placed into the distillation unit.
- The temperature was increased to predetermined increment and held for approximately 15 minutes. Samples at specific temperature ranges (i.e., 97° to 205°C) were distilled off, condensed, and tested.
- The volume which volatized from the initial sample was collected and measured, cooled to room temperature, and the sample was evaluated to identify if the liquid stratified into layers.
- If the fraction of the volatized material was stratified into layers, the volume of each stratified layer was also measured.
- Each distillation sample, and if present each stratified layer(s), in the distillation sample were analyzed for VOA (Method 8260), SVOA (Method 8270), and TPH (Modified Method 8015).
- Table 2.2-3 presents summary information on the distillation analysis (such as the sample description, temperature range, volume of distillate, miscibility in water, and laboratory analyses requested).

Results for analyses conducted on distillate samples are discussed in Section 2.6-5 and presented in Appendix C5-1 through C5-3.

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Borehole 25294

Borehole 25294 was drilled to a depth of 8.0 feet BGS (Table 2.2-1). During drilling and sampling of borehole 25294, a large cobble was encountered near the ground surface which prevented the collection of a soil core in the borehole to an approximate depth of 4 feet. The OVM reading was 11 ppm downhole at the 4 foot depth. Muddy water was observed dripping from the core barrel at approximately the 4-foot depth. After the cobble was pushed aside, a drum was encountered which prevented the collection of soil core to a depth of 8 feet. At this depth, drilling was stopped and an attempt was made to abandon the borehole using a bentonite grout slurry (4 bags of bentonite, approximately 30 gallons). When the required amount of bentonite slurry failed to fill and seal the borehole, field personnel pulled the augers to investigate why the borehole was not sealed. Once the augers were removed, a large void space was observed in the borehole from an approximate depth of 4 to 6.5 feet BGS. In addition to the large void space, three flattened drums were observed in the borehole at depths greater than 4 feet. A downhole camera was lowered into the borehole to view the void space. On Thursday, November 3, 1994, EG&G personnel videotaped borehole 25294 with the downhole camera. The camera clearly indicated a void space from 4 to 6.4 feet BGS. The borehole was plugged using a metal rebar plug filled with a cement/bentonite slurry.

Borehole 25394

Borehole 25394 was drilled and sampled to an approximate depth of 9 feet BGS (Table 2.2-1). A caliche layer was encountered at approximately 6 to 7 feet BGS indicating that the base or bottom of the trench is above this depth. Similar to conditions at borehole 25294, the bentonite grout slurry did not fill and seal the borehole. The borehole was then plugged using a metal rebar cage and concrete.

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Borehole 25494

Borehole 25494 was drilled and sampled to an approximate depth of 3.5 feet (Table 2.2-1). A large void space was encountered at a depth of 3.5 feet. Due to limited recovery, no samples were collected for analytical testing. There was an OVM reading of 19 ppm at a depth of 3.5 feet. Upon removal of the augers, the field crew observed three flattened drums in the borehole. Cement/bentonite was poured into the borehole to the ground surface to abandon the borehole.

Borehole 25594

Borehole 25594 was drilled and sampled to a depth of 16 feet (Table 2.2-1). Drums were encountered at an approximate depth of 2.5 feet, which prevented the recovery of core. The center bit from the hollow stem auger was used to drill through the drums from a depth of 2.5 to 7 feet. Discolored soil was encountered at a depth of 9 to 9.25 feet (OVM reading of 1300 ppm). The discolored soil was described as a black asphalt-like which had impregnated the matrix and coated the gravels. Samples were collected from the discolored soil for laboratory analysis. No soil core was collected from 10 to 14 feet, so the center bit was used to drill from 14 to 15 feet. Bedrock described as clayey siltstone was encountered at a depth of 15.5 feet. Two five-gallon buckets of bentonite pellets were placed down the borehole and hydrated to seal the bottom of the hole to prevent potential vertical migration of contaminants. A metal rebar plug filled with a concrete/bentonite slurry was then placed at an approximate depth of 3 feet BGS.

Borehole 25694

Borehole 25694 was drilled and sampled to a depth of 14 feet (Table 2.2-1). No core was recovered from a depth of 7 to 8 feet BGS, so the center bit was used to drill from 8 to 10 feet. Black discolored soil was observed in the core from an approximate depth of 10 to 13

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feet. Bentonite pellets were placed on the bottom of the borehole and hydrated to prevent potential vertical migration of contaminants down the borehole. The borehole was abandoned using a metal rebar plug filled with a cement/bentonite slurry.

2.2.2 Well Abandonment of SVE Arapahoe Formation No.1 Sandstone SVE Extraction and Monitoring Wells

Prior to the abandonment of the SVE Arapahoe Formation No. 1 Sandstone wells (24193, 24393, 24993, and 25093) located near Trench T-3 (Figure 2.4-1), groundwater analytical samples were collected for analytical testing. A televiewer camera was also lowered down the casing in well 24193, 24393, and 24993 to document the condition of the well prior to abandonment.

The groundwater analytical samples were collected from each well at the bottom of the well and at the top of groundwater. Samples were collected at the bottom of the well using a bottom sampling bailer, while the top of groundwater sample was collected with a 4-foot bailer. Table 2.2-4 shows where each sample was collected (i.e., top or bottom), the depth to groundwater from the top of the well casing and its elevation as measured from mean sea level (MSL). Groundwater samples were analyzed for VOCs by EPA Method 524.2 and dissolved metals. Analytical results are discussed in Section 2.6.2 and presented in Appendix C4.

2.3 MICROBIAL ECOLOGY

The microbial ecology of the Trench T-3 area has not been characterized to date. Information on the Trench T-3 area microbial population, and other factors, will assist in determining the use of biodegradation for the potential site remediation. Based on the results of numerous studies presented in the literature, it is known that chlorinated solvents such as those found in OU-2 are either oxidized or dechlorinated by microorganisms (Egli et al. 1988, Egli et al.

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1990, Fogel et al. 1986, Gossett 1985, Janssen et al. 1988, Kastner 1992, Little et al. 1988, Nelson et al. 1987, Oldenhuis et al. 1989, Vogel et al. 1987, Wackett et al. 1989). Also, studies have shown that these solvents or similar solvents can be completely degraded to nonregulated products under controlled laboratory conditions (Norris et al. 1994).

However, there is a lack of information on successful application of biodegradation of chlorinated solvents in situ since this is a relatively new area of study. Therefore, at this time, it is not possible to predict the potential for successful biodegradation of chlorinated solvents using in situ treatment in OU-2.

Though it is biologically possible to degrade chlorinated solvents, the types of microorganisms, physical features, soil chemistry, contaminant concentration and availability, permeability of the soil matrix to water and nutrients, and redox conditions of OU-2 will determine whether microorganisms can be used to treat the solvents in OU-2. A thorough evaluation of these factors requires a treatability study and is beyond the scope of this evaluation. However, a treatability study on the biodegradation of chlorinated solvents in OU-2 soil is underway at RFETS.

2.4 GEOLOGY

2.4.1 OU-2 and Trench T-3 Stratigraphy

The geology beneath Trench T-3 was evaluated based on the available information collected from the Phase I, Phase II (alluvial and bedrock), SVE Site No. 1 field, and the Trench T-3 drilling characterization investigation. Phase I and Phase II borehole and monitoring well construction logs are presented in the Preliminary Draft Phase II RFI/RI Report for OU-2 (DOE 1993a), while the SVE Site No. 1 and Trench T-3 drilling characterization investigation draft borehole and monitoring well construction logs are presented in Appendix A1 of this report. The locations used to evaluate the geology beneath Trench T-3 are listed in Table

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2.4-1 and shown on Figure 2.4-1. Table 2.4-1 lists survey coordinates, ground surface elevations, stratigraphic, and well/borehole completion information. The main geologic units of concern beneath Trench T-3 are the Rocky Flats Alluvium, the Arapahoe Formation, and upper portion of the Laramie Formation (uppermost five feet). Figure 2.4-2 shows the generalized stratigraphy of these units in the vicinity of RFETS. Cross-sections have been constructed to illustrate the subsurface conditions around Trench T-3 (Figures 2.4-5 through 2.4-8). Figures 2.4-3 and 2.4-4 show the locations of those cross-sections (A-A', B-B', C-C', D-D', and E-E'). The cross-sections were constructed to show the geology of the geologic units of concern, including a caliche layer within the Rocky Flats Alluvium, the No. 1 Sandstone Unit within the Arapahoe Formation, and a highly friable saturated sandstone layer within the No. 1 Sandstone Unit. The cross-sections also show the approximate extent of Trench T-3, void space, and flatten drums area.

The East Trenches, including Trench T-3, are underlain by RFA that is the topographically highest and oldest unconsolidated deposit beneath RFETS (DOE 1993a), as shown on Figure 2.4-2. The RFA was deposited as large, laterally coalescing alluvial fans along the base of the adjacent mountain front (Hurr 1976). The thickness of the RFA is approximately 15 feet in the vicinity of Trench T-3, and is comprised of clayey, silty, and sandy gravel (GC, GM, and GW) with interbedded clay lenses (CL), clayey silty, gravelly sands (SC and SM), and a laterally extensive caliche layer.

The gravel and sand layers in the vicinity of Trench T-3 range in grain size from fine-grained sands to cobbles, are angular to subrounded, have low plasticity, usually have a trace to some fines (clays and silts) or caliche as a binder in matrix, and are generally brown to reddish-brown in color.

The contact between the RFA and the underlying bedrock (Arapahoe and Laramie units) is highly irregular, due to the erosion of the top of bedrock surface, as shown on Figure 2.4-16. Figure 2.4-17 shows the enlarged view of the top of bedrock in the vicinity of Trench T-3.

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Therefore, the thickness and geometry of the Rocky Flats Alluvium is controlled by certain top of bedrock features.

The caliche layers, in general, contain about 50 percent calcium carbonate, range in grain size from fine-grained sand to cobbles, are angular to subrounded, have low plasticity, and are white to a very pale brown in color. The caliche was encountered in the boreholes around Trench T-3 at an approximate depth of 2 to 4 feet, with caliche thickness ranging from 1 to 6 feet, as shown on Figures 2.4-5, 2.4-6, and 2.4-8. However, the caliche layer was encountered at a depth of approximately 11 feet with a thickness of approximately 1.5 feet in well 24993, as shown on Figure 2.4-5. A caliche layer was encountered at a depth of approximately 6 feet in borehole 25394. The caliche in this borehole indicates that the base of the trench is above this depth in the vicinity of borehole 25394. The caliche layers may retard infiltration of precipitation to the vadose zone around Trench T-3. Likewise, where the caliche layers have been disturbed due to the excavation of Trench T-3, infiltration of precipitation may be enhanced relative to surrounding areas.

The material in Trench T-3 has been described as disturbed ground, primarily clayey or sandy gravels with some silt (GC, GM, or GW). Due to numerous flatten drums and void space, recovery of core was limited in the boreholes drilled within Trench T-3. Boreholes 25294, 25494, and 25594 encountered the void space and/or flatten drums at approximate depths from 2 to 7 feet BGS, as shown on Figures 2.4-9 and 2.4-10. A detailed discussion of the boreholes drilled into Trench T-3 is presented in Section 2.2.1 of this report. The void space encountered at an approximate depth of 4 feet BGS, extending to depth of 5.3 feet BGS in borehole 25194, was filled with a stratified liquid (NAPL) as shown on Figure 2.4-6.

The Arapahoe Formation unconformably underlies the RFA, and is comprised of sandstones, siltstones, and claystone, as shown on Figure 2.4-2. The Geological Characterization Report (DOE 1991a) states that the Arapahoe Formation beneath the RFETS site is a fluvial deposit comprised of channel, point bar, and overbank deposits. The sandstone channel sequence of

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the Arapahoe Formation beneath and around Trench T-3 is referred to as the No. 1 Sandstone Unit. Lithologically, the No. 1 Sandstone Unit consists predominantly of an interbedded sequence of sandstone, silty to clayey sandstones, and sandy claystone.

The No. 1 Sandstone Unit is heterogeneous, moderately to highly friable, pale olive to light gray in color (oxidized sections are yellowish orange), and has a range of grain size from very fine to medium-grained sand. Matrix grains are predominantly quartz with traces of feldspar, mafics, and micas. Stacked fining upward sequences in grain size are common in the No. 1 Sandstone Unit. A single fining upward sequence typically consists of a lower bed of sandstone or silty sandstone with sand grain size ranging from medium to very fine-grained, overlain by a bed of clayey sandstone or sandy claystone containing predominantly very fine-grained sand. Material from the highly friable saturated sandstone layers in the No. 1 Sandstone Unit commonly flows into the open borehole during drilling. The highly friable saturated sandstone layer is predominantly medium-grained sand with a trace of fine and coarse-grained sands, dusky yellow in color, and has pitted and frosted grains of quartz with some iron staining. Estimated porosity of this unit is approximately 25 percent porosity. Figures 2.4-5 through 2.4-8 show the location and correlation of this highly friable sandstone (Ka No. 1) layer.

The geometry, lateral extent, and top of the No. 1 Sandstone Unit in OU-2 are shown on Figures 2.4-11 and 2.4-12. Figures 2.4-13 and 2.4-14 show enlarged views in the vicinity of Trench T-3. Thinner sections of sandstone generally occur towards the channel margins, and thicker sections occur toward the center of the channel. The thickness of the No. 1 Sandstone Unit ranges from about 20 to 35 feet in the vicinity of Trench T-3, with the thickness increasing toward the east end of Trench T-3, as shown on Figure 2.4-14. The No. 1 Sandstone Unit is believed to be in contact with the RFA (subcropping condition) in the areas south and east of Trench T-3 (DOE 1993a), as shown on Figure 2.4-15. Core logging of locations 24093 through 25093 and 25594 (Figure 2.4-1) indicates that the No. 1 Sandstone Unit subcrops beneath Rocky Flats Alluvium near the central and eastern parts of Trench T-3,

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as shown on Figure 2.4-15. However, in the western part of the trench (near borehole 10191), the Rocky Flats Alluvium and No. 1 Sandstone Unit are separated by approximately 10 feet of claystone and/or siltstone.

The basal contact between the No. 1 Sandstone Unit and the Upper Laramie Formation is usually abrupt and non-gradational. It is believed that the No. 1 Sandstone Unit was incised into the Laramie Formation during deposition. The presence of claystone clasts in the No. 1 Sandstone Unit similar to the underlying claystone appears to support this theory. The depth to the basal contact of the Arapahoe and Laramie Formations in the vicinity of Trench T-3 is approximately 45 to 50 feet.

The Upper Laramie Formation depositional environment has been defined by Weimer and Land (1975) to be part of a delta plain complex along the western edge of the Western Interior Seaway. The most common lithologies of the Upper Laramie Formation are claystones and silty claystones. In addition to the claystone, sandy and clayey siltstones, and alternating sequences of sandstone and siltstones are present in the Upper Laramie Formation. The claystones and silty claystones are light to medium olive-gray, and occasionally olive-black. The sandstones are light gray and olive-gray, very fine to medium-grained, moderately sorted, subangular to subrounded, silty, clayey, and quartzic. These fine-grained sediments indicate a low-energy depositional environment. The Upper Laramie Formation underlies the No. 1 sandstone unit at Trench T-3 as shown on Figures 2.4-5 through 2.4-9.

In OU-2, prominent top of bedrock features include the north and south paleoridges and the west/east-trending medial paleoscour (DOE 1993b). The north and south paleoridges are generally southwest/northeast-trending bedrock high features that are indicated by borehole control, as shown on Figure 2.4-18. Trench T-3 is located above the southern flank of the north paleoridge. The medial paleoscour is a bedrock trough feature that is believed to originate in the 903 Pad Area and trends to the northeast between the paleoridges. This paleoscour takes a northward bend and is truncated along the north-facing hillside of the

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South Walnut Creek drainage. Where the paleoscour intersects the hillside, a well-developed surface drainage gully has developed (Figure 2.4-16).

2.4.2 Geotechnical Testing

To estimate the physical properties of the subsurface soils in the vadose zone around Trench T-3 (IHSS 110), samples were collected for geotechnical testing. The samples were selected from the SVE Site No. 1 cores during a visual inspection on August 12, 1994, and from locations: BH3987, 10191, 21693, and 24093 through 25093. The visual inspection of the core included a review of the stratigraphic logs and the existing core to obtain, at a minimum, a sample for each required analysis from each of the lithological layers in the vadose zone around Trench T-3 (i.e., GC, SC, and the No. 1 Sandstone). The geotechnical analyses performed and American Society of Testing and Materials (ASTM) or other method designations for testing the existing core are presented below:

Geotechnical Analyses and ASTM or other Numbers

- Soil porosity (COEEN 111021906)
- Soil permeability in principle directions (ASTM D2434)
- Relative permeability of soil as a function of liquid saturation (EPA 600/2-91/065)
- Relative permeability of soil as a function of gas saturation (EPA 600/2-92/065)
- Capillary pressure as a function of liquid saturation (ASTM D2325)
- Sieve analyses (ASTM 0422)
- Hydraulic conductivity (ASTM 5084)

Due to the limited quantity of intact core from existing boreholes, it was not possible to select a full suite of geotechnical analyses. Therefore, samples from similar lithological layers at

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the same or different locations were selected for the geotechnical testing. The geotechnical samples were submitted for analyses on August 24, 1994. Table 2.4-2 presents the original sample number, the borehole number, composite sample number, depth interval of the sample, and lithology by USCS or Wentworth as appropriate. The USCS codes and Wentworth scales were determined during logging of the core by the stratigrapher. The samples were combined to obtain enough samples to perform the required geotechnical analysis. Table 2.4-3 lists the geotechnical tests performed on each of the samples submitted. Preliminary laboratory geotechnical results are presented in summary Tables 2.4-4 and 2.4-5 of Appendix A-2.

Table 2.4-4 provides a summarized list of the specific gravity, effective porosity, moisture content, dry density, hydraulic conductivity, and ending with final geotechnical results. The remolding criteria required that the samples be remolded for permeability testing based on target dry densities and moisture contents. These target values were derived from field data obtained during previous investigations, and represent the average dry density and moisture content for a given material type. The remolding procedure was to premoistened each sample to the target moisture content. The mass of material required to fill a 2.5-inch diameter by 3.0-inch high mold at the target density was determined. This mass was placed in the mold in three 1.0-inch lifts. Each lift was compacted by kneading compaction with a tamper, followed by an application of hydraulic pressure to achieve the proper density for that lift. The surfaces of the first two lifts were scarified prior to the addition of the next lift. After compaction, the remolded test specimen was removed from the mold, and its weight and dimensions were measured. The specimen was then mounted in the permeameter.

Vertical hydraulic conductivities for geologic materials in and beneath Trench T-3 ranged from 6.60E-04 cm/sec to 9.40E-08 cm/sec. The sample with the highest hydraulic conductivity was collected from location 12191 at a depth of 15.0 to 15.5 BGS and was described as sandy gravel (GW).

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Table 2.4-5 provides results of the sieve analyses. No Atterberg Limits tests were performed on the samples submitted. Results for "Relative permeability of soil as a function of liquid saturation (EPA 600/2-91/065) and Relative permeability of soil as a function of gas saturation (EPA 600/2-92/065)", have not been provided by the laboratory at the time this report was issued.

2.4.3 Geophysical Borehole Logs

Geophysical borehole logging around Trench T-3 was performed during the 1993 revised bedrock field program on pilot borehole 21693, which is located north of Trench T-3. The following geophysical logs were run:

- Caliper
- Natural Gamma
- Short Normal Resistivity
- Neutron
- Tube Wave Amplitude
- Density

Figure 2.4-17 shows the correlation of the geophysical logs with the core lithology from pilot borehole 21693.

2.5 HYDROGEOLOGY

This section presents a summary of OU-2 hydrogeology, with emphasis on the Northeast Trenches Area and Trench T-3 (IHSS 110). The discussion is based on information presented in the Preliminary Draft Phase II RFI/RI Report for OU-2 (DOE 1993b) and the field investigation conducted in 1994 as part of the SVE Pilot Test Site No. 1.

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Past subsurface investigations in the OU-2 area focused on shallow saturated units within OU-2, including the saturated unconsolidated surficial deposits and the shallow (up to 200 feet deep) saturated bedrock units of the Arapahoe and Upper Laramie Formations.

Hydrogeologic conditions in the shallow units of OU-2 are strongly influenced by local geologic conditions, local areal recharge, and interactions with South Walnut and Woman Creeks. Groundwater flow is controlled to a high degree by the shape of the top of bedrock surface, and the geometry and lithology of geologic units. Groundwater recharge occurs primarily as a result of local infiltration of snowmelt, rainfall, and surface water within the OU-2 area. The majority of OU-2 groundwater discharges to surface seeps within the boundaries of OU-2 because the major shallow water-bearing units are completely truncated on the north, east, and south by South Walnut and Woman Creeks.

The hydrogeologic system at OU-2 is comprised of two distinct water-bearing zones: the Upper Hydrostratigraphic Unit (UHSU) and the Lower Hydrostratigraphic Unit (LHSU). The UHSU within OU-2 consists of saturated portions of unconsolidated surficial deposits, high terrace deposits, colluvium, disturbed ground, Arapahoe Formation No. 1 Sandstone that is in hydraulic communication with the saturated surficial materials, and weathered claystone of the Arapahoe and/or Laramie Formations. In addition, Laramie sandstones were considered part of the UHSU, where they subcrop in isolated areas beneath the No. 1 Sandstone Unit or hillside colluvium. The majority of groundwater flow in the UHSU of OU-2 occurs in saturated Rocky Flats Alluvium and in the Arapahoe No.1 Sandstone. In the Northeast Trenches Area, UHSU groundwater flow occurs primarily in the Arapahoe Formation No. 1 Sandstone, except during high groundwater conditions when the extent of saturated Rocky Flats Alluvium includes much of the Northeast Trenches Area. Beneath IHSS 110, the majority of UHSU groundwater flow occurs in the Arapahoe Formation No. 1 Sandstone. Under low groundwater conditions, UHSU groundwater flows only in the Arapahoe Formation No. 1 Sandstone. The hydrogeologic units of interest in OU-2, and the focus of this discussion, are the saturated surficial deposits in the Rocky Flats Alluvium (Section

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2.5.1.1) and the No. 1 Sandstone Unit of the UHSU (Section 2.5.1.2). The conceptual boundary between the UHSU and LHSU is shown in Figure 2.5-1.

The LHSU is composed of Upper Laramie Formation clayey-silty sandstones, claystones, and siltstones that are not in substantial hydraulic communication with the UHSU. Because the LHSU is not in substantial hydraulic communication with the hydrogeologic units of interest, it is not described further in this document. A discussion of the LHSU can be found in the OU-2 Phase II RFI/RI (DOE 1993b).

2.5.1 Upper Hydrostratigraphic Unit

Groundwater in the UHSU of OU-2 exists under unconfined conditions except where portions of the No.1 Sandstone are overlain by claystone, resulting in confined and unconfined conditions within the sandstone. The hydrogeology of the Rocky Flats Alluvium and the No. 1 Sandstone Unit is discussed in Sections 2.5.1.1 and 2.5.1.2, respectively. The UHSU system interactions are discussed in Section 2.5.1.3. In each of these sections, a general discussion of OU-2 hydrogeologic conditions is followed by information more specific to the Northeast Trenches Area and IHSS 110.

Water level data presented in the following sections were collected as part of the Rocky Flats Site-Wide Groundwater Data Collection Program, with the exception of data from wells installed as part of the SVE Pilot Test Site No. 1. Water levels for the SVE wells were obtained after well development in the fourth quarter 1993. The site-wide water levels were used to construct potentiometric maps for second quarter 1992 and fourth quarter 1993. Water levels from the SVE wells were used in the construction of the fourth quarter 1993 potentiometric maps only, because these wells had not yet been installed during 1992. Fourth quarter 1993 groundwater elevations are presented in Table 2.5-1. Second quarter 1992 groundwater elevations are presented in Appendix B of the OU-2 RFI/RI Report (DOE 1993b).

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2.5.1.1 Rocky Flats Alluvium

Groundwater flow within the Rocky Flats Alluvium is strongly influenced by the top of bedrock features, and by the geometry and lithology of alluvial geologic units (Section 2.4). Saturated alluvial conditions within the Rocky Flats Alluvium occur predominantly within lows and scours in the top of the Arapahoe and/or Laramie Formation bedrock materials. The largest of the scours, the medial paleoscour contains and transmits most of the alluvial groundwater in OU-2. This paleoscour appears to originate in the vicinity of the 903 Pad and trends predominantly from southwest to northeast (Figure 2.4-14). The medial paleoscour is believed to truncate along the South Walnut Creek hillside. Alluvial groundwater flowing within the scour discharges along the head of a well-developed surface drainage gully on the hillside, probably as a result of this truncation of the paleoscour along the hillside. This discharge is indicated by seepage observed along the head of the surface drainage gully (Figure 2.4-14).

The areal extent of the saturated alluvium within the medial paleoscour varies considerably with the season. Alluvial groundwater levels are generally at their lowest level during the first quarter of the year. Figures 2.5-2 and 2.5-3 show the areal extent of the saturated alluvium during second quarter (May) 1992 and fourth quarter (October) 1993, respectively. Second quarter 1992 conditions represent the high groundwater level conditions for that year (DOE 1993b). Fourth quarter 1993 represents lower groundwater level conditions. The width of the saturated alluvial zone within the medial paleoscour, in the vicinity of the Northeast Trenches, ranged from approximately 175 feet to 250 feet during October 1993, while the similar saturated alluvial zones width ranged from approximately 300 feet to 450 feet during May 1992. During May 1992, the zone of saturated alluvium included the area of IHSS 110.

It is important to note that the Rocky Flats Alluvium beneath the IHSS 110 is generally dry. The Rocky Flats Alluvium beneath the site becomes saturated only under high groundwater conditions, such as those which occurred during second quarter 1992.

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The fourth quarter 1993 groundwater levels are significantly lower than the May 1992 conditions. For example, the difference in groundwater elevation between May 1992 and October 1993 was approximately 11 feet at wells 07891 and 4286, both of which are located in the Northeast Trenches area within the medial paleoscour. During second quarter 1992, the groundwater elevation at the west end of Trench T-3 was approximately 5,945 feet mean sea level (ft. MSL) (Figure 2.5-2). During fourth quarter 1993, the alluvium at this location is unsaturated (Figure 2.5-3). The groundwater elevation of the uppermost saturated unit (No. 1 Sandstone Unit) at this location is approximately 5,930 ft. MSL during fourth quarter 1993, indicating a significant drop in hydraulic head.

The approximate depth from the ground surface to the alluvial groundwater surface beneath Trench T-3 ranged from 10 to 15 feet during high groundwater conditions (May 1992). During October 1993, the estimated depth to groundwater in the No. 1 Sandstone Unit ranged from 20 to 30 feet.

In the Northeast Trenches Area, the flow direction of alluvial groundwater in May 1992 was generally to the northeast, following the medial paleoscour, with a hydraulic gradient of about 0.019 feet/foot (Figure 2.5-2). The alluvial groundwater flow direction during October 1993 was also generally to the northeast following the medial paleoscour, with a hydraulic gradient of approximately 0.015 feet/foot (Figure 2.5-3).

Recharge. Groundwater recharge to the Rocky Flats Alluvium within the OU-2 area occurs due to local direct infiltration of precipitation, and due to seepage from surface water features such as ditches. The rate of recharge to the alluvium is generally highest during the spring, when precipitation is high and evapotranspiration is low. The effects of increased temperature and evapotranspiration tend to minimize the recharge rate during summer. Recharge is also minimal during fall and winter months, due to the low precipitation that occurs during those months.

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The dominance of localized areal recharge on the OU-2 UHSU groundwater system is indicated by the large groundwater level fluctuations that occur in response to springtime precipitation events. Alluvial groundwater levels typically rise rapidly in the spring due to recharge and then decrease until spring of the following year when the seasonal cycle begins again, as shown in the hydrographs for wells B218789 and 4286 (Figures 2.5-4 and 2.5-5), located in the Northeast Trenches Area. The period of rapid water level rise in these wells is followed by a period in which water levels fall rapidly, presumably due to discharge from the alluvial system to seeps and to the No. 1 Sandstone Unit. This period is generally followed by a period of slower water level decline (beginning in early summer), during which discharge from alluvium occurs at a lower rate.

Hydraulic Properties and Estimated Flow Velocities. Estimates of hydraulic conductivity for the Rocky Flats Alluvium at OU-2 are based on aquifer testing activities (drawdown-recovery tests) on wells during the 1986 initial Comprehensive Environmental Assessment and Response Program (CEARP) Phase II site characterization, slug tests performed on 1986 and 1987 wells during the 1987 Phase I RFI/RI, and from aquifer pumping tests conducted in 1992 as part of the Phase II RFI/RI. Results of the 1986 and 1987 tests are summarized in Table 2.5-2. The results of the 1992 tests are summarized in Table 2.5-3.

Hydraulic conductivity values estimated for the Rocky Flats Alluvium from the 1986 and 1987 investigations ranged from 4 x 10⁻² cm/s to 6 x 10⁻⁵ cm/s (Rockwell International 1987). Hydraulic conductivity estimates from pumping tests ranged from 4 x 10⁻⁵ cm/s to 9 x 10⁻⁵ cm/s, while those from slug tests ranged from 6 x 10⁻⁵ cm/s to 5 x 10⁻² cm/s. The geometric mean for the 1986 and 1987 investigation results is 4 x 10⁻⁴ cm/s. Hydraulic conductivity values estimated from the 1992 pumping test conducted at the well cluster, located in the Northeast Trenches Area (wells 05691, 11491, 20291, and 20491), range from 8 x 10⁻⁴ cm/s to 4 x 10⁻³ cm/s. Estimated values of hydraulic conductivity from the 1992 pump test at the cluster of wells 1787, 20591, and 20691, ranged from 1 x 10⁻⁴ cm/s to 9 x 10⁻⁴ cm/s. The geometric mean of the estimated values from the 1992 tests is 8 x 10⁻⁴ cm/s.

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Potential average groundwater flow velocity (average linear velocity) was estimated for the Rocky Flats Alluvium based on the estimated mean hydraulic conductivity, estimated hydraulic gradient, and assumed effective porosity. Using the geometric mean value for estimated hydraulic conductivity from the 1986, 1987, and 1992 aquifer tests (6 x 10⁻⁴ cm/s); the estimated average hydraulic gradient for the alluvium from the 1992 water level measurements (about 0.020 feet/foot); and an assumed effective porosity of 10 percent; the estimated potential average linear groundwater flow velocity is about 120 feet/year in the area of Trench T-3.

Greater than expected groundwater yields experienced during bedrock SVE pilot tests in 1994 at Trench T-3 are believed to be due to the highly friable coarse grained sandstone unit of the No. 1 Sandstone. The Test Site No. 1 wells penetrate this unit (see Figures 2.4-5 through 2.4-9), which is believed to transmit the majority of groundwater in the No. 1 Sandstone in the vicinity of Trench T-3. See Section 2.4 for further discussion of lithology location and depth.

Rocky Flats Alluvium Seeps. Because the Rocky Flats Alluvium is completely truncated to the north, east, and south within the OU-2 area, all alluvial groundwater is discharged to surface and subsurface seeps along the slopes of the drainages, with the exception of alluvial groundwater which migrates vertically into the underlying No. 1 Sandstone Unit (Plate 2.5-1). Groundwater seepage from the Rocky Flats Alluvium occurs where saturated alluvium is truncated along the hillsides at the contact between Rocky Flats Alluvium and bedrock. At these locations, discharged seep water infiltrates the colluvium and the high terrace alluvium downslope from the seepage face. The resultant increase in soil moisture in these downslope geologic materials allows characteristic vegetation (typically cattails, baltic rushes, woody bushes, and other phreatophytes) to develop that is distinct from the surrounding tall and short prairie grasses common to RFETS. The locations of these alluvial seeps and associated downslope vegetated areas were mapped by visual field observations during the summers of 1992 and 1993. High terrace alluvium and bedrock seep locations were also mapped.

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An alluvial seep area occurs at the surface drainage gully northeast of the Northeast Trenches Area. This seep area is considered to be large relative to other OU-2 seeps. As discussed earlier, the majority of the alluvial groundwater within OU-2 is contained and transmitted along the medial paleoscour (a top of bedrock feature). This bedrock feature is believed to be truncated along the South Walnut Creek drainage at the head area of the above-mentioned surface drainage gully. This alluvial seep supplies surface water flow to the drainage gully. This surface water in turn flows downslope within the gully and discharges to South Walnut Creek approximately 300 feet west of Pond B-5.

Other alluvial seeps along the South Walnut Creek drainage are thought to occur east of the surface drainage gully. These seeps are considered to be of minor importance because they are not located in areas of known groundwater contamination.

2.5.1.2 Arapahoe Formation No. 1 Sandstone

The Arapahoe Formation No. 1 Sandstone is the uppermost sandstone unit within OU-2. The No. 1 Sandstone Unit is a fluvial sandstone channel which incised into the surrounding claystone bedrock deposits. The saturated No. 1 Sandstone Unit is bounded in areal and vertical extent by the surrounding bedrock deposits, which are mostly claystone, or by the South Walnut Creek drainage, which has eroded away the northern edge of the sandstone channel. Figures 2.5-6 and 2.5-7 show the areal extent of the No. 1 Sandstone Unit in the portion of OU-2 west of the East Spray Fields. East of that area, subsurface control for the No. 1 Sandstone Unit is limited or non-existent.

The No. 1 Sandstone Unit subcrops beneath the Rocky Flats Alluvium in some OU-2 locations and is separated from the alluvium by claystone in others (DOE 1993b, Figure 3.5-22). The No. 1 Sandstone Unit subcrops beneath the Rocky Flats Alluvium in much of the Northeast Trenches Area (Figure 2.4-13). IHSS 110 is located along the edge of such an area. Beneath IHSS 110, the thickness of the claystone layer separating the No.1 Sandstone

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from alluvium ranges from approximately 0 to 10 feet. Thickness of the claystone layer increases to the northwest.

The majority of groundwater in the No. 1 Sandstone Unit in OU-2 occurs under unconfined conditions, but it does occur under confined conditions in limited areas. Where the No. 1 Sandstone Unit subcrops beneath the alluvium, groundwater within the No. 1 Sandstone Unit is unconfined. Where the sandstone is separated from the alluvium by claystone, groundwater may occur under confined or unconfined conditions.

In the Northeast Trenches Area, groundwater within the No. 1 Sandstone Unit is believed to exist under unconfined conditions. As stated above, the No. 1 Sandstone Unit subcrops to alluvium in much of the area, thus providing a direct means for hydraulic communication between the units. In addition, the alluvium is primarily unsaturated beneath the Northeast Trenches Area, during most of the year, and the groundwater level falls below the top of the No.1 Sandstone providing for unconfined groundwater conditions. This condition exists beneath IHSS 110 during most of the year due to its location relative to the saturated alluvium zone.

Groundwater flow direction within the No. 1 Sandstone Unit is controlled by the geometry of the sandstone unit and its interaction with the overlying alluvium and South Walnut and Woman Creek drainages. Potentiometric maps for the No. 1 Sandstone unit for second quarter (May) 1992 and fourth quarter (October) 1993 (Figures 2.5-6 and 2.5-7) indicate that the primary flow direction within the sandstone is to the north-northeast, with some flow to the southeast. The hydraulic gradient in the No. 1 Sandstone Unit varies from approximately 0.028 feet/foot to as much as 0.1 feet/foot.

East of the 903 Pad, the potentiometric surface of the No. 1 Sandstone Unit appears to be see mounded, causing flow in the sandstone to diverge, with most flow moving to the north and northeast and some flow moving to the southeast (Figures 2.5-6 and 2.5-7). Flow is primarily

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to the northeast or north in the area beneath and to the north of the medial paleoscour. Groundwater flowing north and northeast discharges to subsurface sandstone seeps where the sandstone subcrops beneath colluvium along the southern slope of the South Walnut Creek drainage.

Recharge Recharge to the No. 1 Sandstone Unit in OU-2 probably occurs as a result of infiltration of precipitation and surface water through overlying unsaturated deposits, vertical flow from overlying saturated alluvium, and inflow to the area from upgradient portions of the sandstone west of OU-2. The No. 1 Sandstone Unit is believed to receive recharge from downward vertical flow from overlying saturated alluvium in areas where the alluvium and sandstone are in direct contact, or where they are separated by only a few feet of weathered and/or fractured claystone (Figure 2.4-13). Downward vertical flow between the alluvium and No. 1 Sandstone Unit is indicated by downward vertical gradients between the units in areas where the alluvium and No. 1 Sandstone Unit are not in direct contact (DOE 1993b). Evidence for recharge in the contact zone along the medial paleoscour northeast of the 903 Pad is indicated by a potentiometric high within the sandstone in that area and contaminant data that indicate migration of contamination from the alluvium to the sandstone (Section 2.6.2). In addition, evaluation of groundwater geochemical data for wells screened in the Rocky Flats Alluvium and wells screened in the No. 1 Sandstone Unit indicates that the two units have similar groundwater geochemistry (DOE 1993b).

Water level data indicate that recharge to the No. 1 Sandstone Unit within OU-2 also occurs as inflow from the west, where the No. 1 Sandstone Unit crosses the western boundary of OU-2. This groundwater flow is the only apparent source of groundwater recharge into the UHSU within OU-2 that is not directly related to infiltration from precipitation falling on OU-2.

Hydraulic Properties and Estimated Flow Velocities. Estimates of hydraulic conductivity for the No. 1 Sandstone Unit at the OU-2 site are based on aquifer testing activities

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conducted in 1987 and 1992, and on the 1994 pumping test results from Site No. 1 described in Appendix B. The results from the 1987 tests are summarized in Table 2.5-4. The results from the 1992 tests are summarized in Table 2.5-5. The Site No. 1 results are presented in Appendix B and summarized in Table 2.5-6.

Hydraulic conductivity values estimated for the No. 1 Sandstone Unit from the 1987 investigations (slug tests only) ranged from 3 x 10⁻³ cm/s to 2 x 10⁻⁴ cm/s (Rockwell International 1987). The geometric mean of the 1987 investigation results is 1 x 10⁻³ cm/s. Calculated values of hydraulic conductivity for the No. 1 Sandstone Unit, determined from the 1992 pumping test measurements conducted at the Site No. 1 well cluster (wells 3687, 20991, and 21091, and 20891), ranged from 3.7 x 10⁻⁴ to 6.2 x 10⁻⁴ cm/sec. The geometric mean of the 1992 investigation results is 4.8 x 10⁻⁴ cm/s.

Hydraulic conductivity estimates for the No. 1 Sandstone Unit from the 1994 pumping test range from 1×10^{-3} to 4×10^{-3} cm/s (Table 2.5-6). The geometric mean of the 1994 results is 2.3×10^{-3} cm/s.

Potential groundwater flow velocities (average linear velocities) were estimated for the No.1 Sandstone based on the estimated mean hydraulic conductivity, estimated hydraulic gradient range, and assumed effective porosity. Based on the geometric mean value for estimated hydraulic conductivity from the 1987, 1992, and 1994 aquifer tests (1 x 10⁻³ cm/s), the measured hydraulic gradient range from the 1992 water level measurements (0.028 to 0.1 feet/foot; DOE 1993b), and an assumed effective porosity of 10 percent, the estimated potential average linear groundwater flow velocity ranged from 300 ft/year to 1,000 ft/year.

Arapahoe Formation No. 1 Sandstone Seeps. Because the No.1 Sandstone is entirely truncated to the north, east, and south by the South Walnut and Woman Creek drainages, no direct off site groundwater pathway within the sandstone exists from OU-2 to off site

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locations. Therefore, virtually all No. 1 Sandstone Unit groundwater within OU-2 is discharged to seeps along the slopes of the drainages.

It is believed that the No.1 Sandstone subcrops beneath colluvium along the South Walnut Creek hillside north of the Northeast Trenches. This is based on projections of elevations of the No. 1 Sandstone Unit encountered in monitoring wells and boreholes located on the pediment top, close to the hillside. Outcrops in some manmade ditches along the hillside also confirm the subcrop position of the sandstone. The location of the base of the No. 1 Sandstone Unit, projected into the hillside from nearby subsurface control, is shown in Figures 2.5-6 and 2.5-7. Seep areas and associated downslope vegetated areas that occur near this projected base are attributed to groundwater discharge from the sandstone (Plate 2.5-1). In contrast to the localized alluvial seep discharge from the previously discussed medial paleoscour, groundwater subsurface seepage associated with the No.1 Sandstone along the South Walnut Creek hillside tends to be spread over a wide area and discharges at a low flow rate.

2.5.1.3 UHSU System Interaction

Where the No. 1 Sandstone Unit and Rocky Flats Alluvium are in direct contact or are separated by a thin layer of claystone, their water levels are similar, indicating a substantial degree of hydraulic communication. Where the alluvium and sandstone are separated by a substantial thickness of claystone, they become less hydraulically connected and behave as more separate systems with different flow directions and water levels.

Saturated Rocky Flats Alluvium and the No. 1 Sandstone Unit appear to be in hydraulic communication in much of OU-2 where the sandstone and alluvium are in contact or in close vertical proximity. In the subcrop area northeast of the 903 Pad, along the medial paleoscour, paired wells 1991 (sandstone) and 13491 (alluvial) have very similar water levels and appear

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to be in hydraulic communication. Downward vertical gradients between the screened intervals of these two wells in second quarter 1992 were 0.019 feet/foot.

Groundwater elevation observations indicate that the Rocky Flats Alluvium and No. 1 Sandstone Unit are in less hydraulic communication in areas where they are separated by claystone (i.e., in the Northeast Trenches Area, several hundred feet northeast and downgradient of wells 01991 and 13491, along the paleoscour). Water levels in wells 03191 (alluvial) and 12691 (sandstone) differ by 8 to 9 feet in May 1992 observations. At the well (05391 (alluvial) and well 12391 (sandstone) well pair, the observed water levels differed by 14 to 15 feet in May 1992. Several feet of claystone separates the sandstone and alluvium at both of these locations. Downward vertical gradients across these two well pairs in second quarter 1992 were approximately 0.2 feet/foot and 0.4 feet/foot, respectively. The higher vertical gradients for these two pairs, relative to the gradients reported for the pair above (i.e., pair 01991/13491), are also indicative of a lower degree of hydraulic communication. In addition, there appears to be a longer delay at well 12391 in the water level response to recharge events than occurs in well 05391 (see Figures 2.5-8 and 2.5-9, respectively). The response delay may result because well 05391 receives direct recharge from precipitation, while well 12391 receives recharge from upgradient areas of the No. 1 Sandstone Unit. This is further evidence that the sandstone and alluvium have limited vertical hydraulic communication in this area.

Interaction between the colluvium, Rocky Flats Alluvium, and the No. 1 Sandstone Unit occurs where the saturated alluvium is truncated upslope of colluvium and where sandstone subcrops beneath the colluvium. In most cases, flow is from the alluvium and sandstone to the colluvium. In limited areas, however, localized recharge of subcropping sandstones from colluvial water may occur.

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2.6 NATURE AND EXTENT OF CONTAMINATION

The following discussion provides a description of the nature and extent of contamination within subsurface soils, the liquid collected from location 25194, UHSU groundwater, and soil gas in the vicinity of Trench T-3. In general, VOC and semivolatile organic compound (SVOC) analytical results for these media are discussed in greater detail than the remaining chemical groups (i.e., metals, water quality parameters, radionuclides) because the OU-2 Subsurface IM/IRA focuses on the removal of VOC contamination in the subsurface.

The only bedrock well (23293) in the vicinity of Trench T-3 was unable to be developed and, as a result, was not sampled. Therefore, the nature and extent of contamination in the LHSU will not be discussed in this section.

2.6.1 Subsurface Soils.

Nine source boreholes, two plume characterization monitoring wells, one pilot borehole, one abandoned plume characterization monitoring well, and seven SVE boreholes (10191, 02991, 12191, 21693, 22493, BH3987, BH4087, 24093, 24193, 24493, 24593, 24693, 24793, 25093, 25194, 25294, 25394, 25494, 25594, and 25694) were drilled and sampled during Phase I, Phase II, and Site No. 1 investigations to characterize the vertical extent of contamination in Trench T-3. Subsurface soil analytical results for these boreholes and wells are summarized in Table 2.6-1. Table 2.6-1 presents the detection frequency, concentration or activity ranges, and mean concentration or activity, as well as the background mean plus two standard deviations for metals and radionuclides. Analytical results for samples collected from the above boreholes are presented in Appendix C1 of this report.

Detections of VOC, SVOC and pesticide/polychlorinated biphenyl (PCB) are shown on Figure 2.6-2 (Figure 2.6-1 is a legend for analyte abbreviations and laboratory and validation qualifiers). SVOC and pesticide/PCB analyses were performed only on samples collected

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from boreholes 10191, 25294, 25595, BH3987, and BH4087. Cross-sections (Figures 2.6-4 through 2.6-6) were constructed to illustrate the vertical extent of contamination for selected volatiles beneath Trench T-3. The VOCs selected for this evaluation were CCl₄, CHCl₃, PCE, TCE, and total VOCs because of their prevalence in the subsurface soils beneath Trench T-3. The cross-sections were constructed with the following information: the borehole log, generalized lithologic units, Trench T-3 location and approximate depth, initial and high groundwater levels, and analytical results on a logarithmic scale. The generalized lithologic units include the Rocky Flats Alluvium, Arapahoe Formation, No. 1 Sandstone Unit, Laramie Formation, and the approximate contact between these units. Initial groundwater level information was collected in the field at the time of drilling and the high water level was measured in monitoring wells during second quarter 1992. Figure 2.6-3 presents the legend for the source borehole characterization cross-sections.

2.6.1.1 <u>VOCs</u>

Fourteen VOCs were detected in subsurface soil samples collected within Trench T-3 (IHSS 110), as shown on Table 2.6-1. Toluene, a suspected field contaminant (see the OU-2 Phase II RFI/RI report [DOE 1993b] for further discussion), was detected in approximately 72 percent of the subsurface soil samples. Chlorinated hydrocarbons (CHCs), including 1,1,1-trichloroethane (1,1,1-TCA), CCl₄, chloroform (CHCl₃), PCE, TCE, 1,1-dichloroethene (1,1-DCE), 1,2-dichloroethene (1,2-DCE), and 1,2-dichloroethane (1,2-DCA) were detected at concentrations ranging from a few parts per billion to several parts per thousand, as shown on Figure 2.6-2. The vertical extent of selected VOC contaminants is presented on Figures 2.6-4 through 2.6-6. In addition to these chlorinated hydrocarbons (CHCs), five other VOCs (2-butanone, acetone, ethylbenzene, methylene chloride, and total xylenes) were detected in subsurface soil samples. Locations at which elevated levels of VOCs were encountered are described below.

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Apparent NAPL was observed in subsurface materials at several locations in the vicinity of Trench T-3. Free product was observed in borehole 10191 at an approximate depth of 2.8 feet during drilling. Borehole 10191 was drilled in the trench in December of 1991 during the OU-2 Phase II RFI/RI alluvial program. The free product encountered in borehole 10191 was described as a yellowish-brown liquid with a high viscosity (thick consistency). No sample of the free product was collected for analysis. Source borehole 10191 exhibited elevated levels of 1,1,1-TCA, CCl₄, CHCl₃, PCE, and TCE in soil samples collected above the initial water at the time of drilling. In general, the concentrations of the CHCs decreased with depth in the vadose zone in source borehole 10191. Below the water table, concentrations increased again, but to levels significantly lower than those seen in the vadose zone (see Section 2.6.2).

Two samples were collected for VOC analysis based on elevated organic readings in the field (using a photoionization detector [PID]) and the observation of discolored soil (black, tar-like) in the core from borehole 24793, at an approximate depth of 6.5 to 10 feet. The discolored core was described as a black, sticky substance that is coating the gravel surfaces, has impregnated the matrix, and occurs as dry asphaltic-like lumps. Elevated PCE (1,090,000 μ g/kg) and TCE (8,100 μ g/kg) concentrations were detected in the sample collected from borehole 24793 at depths of 7.2 to 7.5 feet and 7.5 to 7.8 feet.

A clear liquid was encountered during the installation of three pressure monitoring probe locations inside the trench. These three probe locations were APM20, APM24, and APM25, as shown on Figure 2.6-7. The clear liquid was encountered at an approximate depth of 2.5 feet at these locations. The clear liquid was dripping from the downhole equipment when removed at location APM24, and appeared as a sheen on the downhole equipment at locations APM24 and APM20. Probes APM20 and APM25 were installed to a total depth of 7 feet, while APM20 was installed to a total depth of 12 feet. A maximum PID field reading of 177 parts per million (ppm) was observed on the downhole equipment from location APM24.

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Three VOC samples were collected from boreholes 25594 and 25694 based on elevated organic readings in the field (using a PID) and the observation of discolored soil (black, tar-like). Two of the three VOC samples were collected from borehole 25594 at approximate depths of 9.8 to 10 feet and 15.3 to 16 feet BGS, with resulting PCE concentrations of 510,000 μ g/kg and 730,000 μ g/kg, respectively. Total xylenes were also detected at a concentration of 95,000 μ g/kg at a depth of 9.8 to 10 feet in borehole 25594. TCE and PCE were detected in the sample collected from borehole 25694 at concentrations of 280 μ g/kg and 38,000 μ g/kg, respectively.

The analytical results for the stratified liquid collected from borehole 25194 in November and December 1994 are discussed in Sections 2.6.4 and 2.6.5 of this report.

Review of the soil gas analytical data collected from the SVE pilot tests (DOE 1994) indicate that approximately 90 percent of the VOCs detected were CHCl₃, CCl₄, PCE, and TCE. These four VOCs are the primary contaminants that were observed in the subsurface soil samples collected in and around Trench T-3. The following is a summary of the average concentration of extracted soil gas for CHCl₃, CCl₄, PCE, and TCE, and total VOCs observed during the SVE pilot test (DOE 1994):

	Average Concentration Range (ppm)	
Analyte	in Extracted Soil Gas	
CHCl ₃	Non-detected (ND) to 23	
CCl ₄	12 to 941	
PCE	ND to 1,379	
TCE	ND to 30	
Total VOCs	207 to 1,947	

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2.6.1.2 **SVOCs**

Fourteen SVOCs were detected in subsurface soil samples collected within Trench T-3, as shown on Table 2.6-1. Three were phthalates - bis(2-ethylhexyl)phthalate, butyl benzyl phthalate, and di-n-butyl phthalate; and four were polyaromatic hydrocarbons (PAHs), 2-methylnaphthalene, naphthalene, phenanthrene and pyrene. The SVOCs detected, except for phthalates, are illustrated on Figures 2.6-2 and 2.6-3 (see the Preliminary Draft Phase II RFI/RI Report for OU-2 [DOE 1993b] for further discussion on phthalates). Of the 21 samples analyzed, phenanthrene was detected in one sample from source borehole 10191, at a depth of 4.2 to 8 feet. Of 21 samples analyzed, 2-methylnaphthalene, 2-methylphenol, and 4-methylphenol were each detected once in a sample from source borehole 10191, at a depth of 4.2 to 8 feet. Of 21 samples analyzed, hexachlorobutadiene was detected once in a sample from borehole 10191 at a depth of 8 to 14.1 feet. Of 21 samples analyzed, hexachloroethane was detected twice in samples from borehole 10191 at two depths: 8 to 14.1 feet and 14.1 to 20.1 feet.

Five SVOCs were detected in soil samples collected at locations 25294 and 25594, none of which was detected in prior work. Butyl benzyl phthalate, detected in both boreholes at depths of 6 to 8 feet and 9 to 10 feet, respectively, ranged in concentrations from 1.1 to 3 mg/kg. The remaining four SVOCs, with one detection each, had lower concentrations, from 0.051 to 1.2 mg/kg.

2.6.1.3 Pesticides/PCBs

Aroclor-1254, a PCB, was detected at the depth of 4.2 to 8 feet at an estimated concentration of 6,900D μ g/kg in borehole 10191 in 1 of 19 samples analyzed, as shown on Table 2.6-1 and Figure 2.6-2.

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2.6.1.4 **Metals**

Table 2.6-1 indicates that seven metals (arsenic, barium, cadmium, calcium, lead, manganese, silver) were detected at concentrations above the background mean plus two standard deviations (background) in subsurface soil samples from Trench T-3. Arsenic was detected above background in 4 out of 23 samples analyzed. All concentrations of arsenic above background were collected from boreholes BH3987 and BH4087. Barium exceeded the background in only one sample, collected from borehole BH3987 at a depth of 15 to 17 feet with a concentration of 413 mg/kg. Cadmium exceeded the background in 6 out of 23 samples analyzed. All concentrations above background were obtained from boreholes BH3987 and BH4087 at concentrations within the same order of magnitude as the background. Calcium was detected above background in one sample collected at a depth of 7.2 to 7.5 feet from borehole 24793. The concentration of calcium above background is likely related to the presence of caliche, a calcium carbonate, in borehole 24793. Lead and silver were detected above background in one sample, collected from borehole 10191 at a depth of 4.2 to 8 feet. Manganese was detected in two samples, from boreholes BH3987 and 10191, at depths of 15 to 17 feet and 20 to 26 feet, respectively.

2.6.1.5 Radionuclides

Nine radionuclides (americium-241 [Am-241], plutonium-238 [Pu-238], plutonium-239/240 [Pu-239/240], Radium-226 [Ra-226], strontium-89,90 [Sr-89,90], tritium, uranium-233,234 [U-233,234], uranium-235 [U-235], and uranium-238 [U-238]), and gross beta were detected at activities above the background (see Table 2.6-1). Am-241 was detected at activities above background in 56 percent of the samples analyzed. Pu-239/240 was detected above background in 19 of 25 samples. Elevated activities of Am-241, gross beta, Pu-239/240, U-233,234, U-235, and U-238 were found in a sample collected at a depth of 4.2 to 8 feet from borehole 10191. The maximum activities of Am-241, Pu-238, and Pu-239/240 occurred in a sample collected at 0 to 4 feet in depth from borehole 25194. The maximum activity

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of Pu-239/240 (8.495 pCi/g) is nearly 500 times higher than the background. Elevated levels of radionuclides occurred in the 4.2 to 8-foot interval of borehole 10191 and generally decreased with depth, indicating the source of radionuclides to be within Trench T-3. Trench T-3 is estimated to be between 5 and 10 feet deep.

Ra-226 was detected above background in two samples collected at depths greater than 44 feet from borehole 10191. Sr-89,90 was detected above the background in 3 of 19 samples analyzed from boreholes BH3987 and BH4087. Tritium was detected above background in one sample collected from borehole BH3987 at a depth of 17 to 20 feet.

All samples analyzed from the latest drilling operations in Trench T-3 in 1994 had Am-241 and Pu-239/240 results higher than background. No background level for Pu-238 has been established and Pu-238 activities for all samples analyzed ranged from 0.006 to 0.1229 pCi/g.

2.6.1.6 Other Analytes and Parameters

The pH of subsurface soils in Trench T-3 ranged from 6.23 to 9.17. Ammonia concentrations ranged from 0.48 to 8.38 μ g/g, and nitrate/nitrite ranged in concentration from 0.27 to 7.18 μ g/g. Total organic carbon content ranged from 167 to 19,200 μ g/g; the maximum concentration was found in a sample collected at a depth of 4.2 to 8 feet from borehole 10191. The maximum total organic carbon result may be associated with NAPL contamination in borehole 10191.

2.6.1.7 **Summary**

The subsurface soil analytical data collected from Trench T-3 indicate that it is a source of VOC contamination (1,1,1-TCA, CCl₄, CHCl₃, PCE, TCE, 1,1-DCE, 1,2-DCE, and 1,2-DCA) to the subsurface soil and potentially to UHSU groundwater. The concentrations of CHCs decrease with depth down to the water table. There is minor PCBs, PAHs, and SVOCs

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contamination. Arsenic, lead, and silver occur above background in Trench T-3. Activities of Am-241, gross beta, Pu-239/240, U-233,234, U-235, and U-238 are also above background. Apparent non-aqueous phase liquid (NAPL) was observed in subsurface materials at several locations in the vicinity of Trench T-3. A yellowish-brown liquid suspected to consist of one or more free-phase CHCs was observed n borehole 10191 at an approximate depth of 2.8 feet. NAPL was observed in borehole 24793 at an approximate depth of 6.5 to 10 feet. NAPL was also observed in borehole 25594 at approximate depths from 7 to 16 feet BGS. NAPL was also observed in borehole 25694 at an approximate depth of 11.8 to 12 feet BGS. This NAPL appeared as black asphalt-like lump that impregnated the soil matrix and coated the gravels. A clear liquid was encountered on the downhole equipment during the installation of three pressure monitoring probes (locations APM20, APM24, and APM25) at an approximate depth of 2.5 feet. A stratified liquid sample with three distinct layers was extracted from borehole 25194 at an approximate depth of 4 to 5 feet BGS.

2.6.2 Groundwater

This section presents information on the nature and extent of VOC contamination in UHSU groundwater in the OU-2 area, specifically the Northeast Trenches Area, including IHSS 110. Other chemical concentrations were determined from samples collected in the Northeast Trenches Area during fourth quarter 1993. However, only VOCs are presented here, because VOCs are expected to be the only groundwater contaminants with the potential to significantly impact vadose zone chemical processes. To characterize VOC contamination in the area, fourth quarter 1993 analytical data from wells screened in RFA colluvium, Arapahoe Formation No. 1 Sandstone, and subcropping Laramie Formation sandstone were evaluated. Analytical results from groundwater sampling performed during SVE pilot tests (March 1994) are presented in Section 2.6.2.6. Analytical results from groundwater sampling performed prior to the abandonment of the Arapahoe Formation No. No. 1 Sandstone wells (24193, 24393, 24993, and 25093) in September, 1994 are presented in Section 2.6.2.7.

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Isoconcentration maps for fourth quarter 1993 were prepared for the alluvial/colluvial and No.1 Sandstone components of the UHSU. Isoconcentration maps were prepared for several analytes and total volatile organics. Concentrations shown on isoconcentration maps include results from 'real' and 'field duplicate' analyses. Real sample results are presented in all cases, except where the field duplicate concentrations for specific analytes are greater, in which case the field duplicate results are shown.

The lateral extent of the saturated zones for the alluvial/colluvial isoconcentration maps were established during the development of the alluvial/colluvial potentiometric map for fourth quarter 1993. Available data for wells sampled during fourth quarter 1993 are presented in Figures 2.6-8 to 2.6-17. Analytical results for UHSU groundwater sample are presented in Appendix C2. Detected concentrations and laboratory or validation qualifiers are indicated in Appendix C2. Non-detected chemicals are indicated by the 'U' qualifier.

The occurrence of CCl₄, CHCl₃, PCE, TCE, and total VOCs in alluvial/colluvial and No. 1 Sandstone Unit groundwater is discussed in the following sections.

2.6.2.1 <u>Carbon Tetrachloride</u>

The highest concentrations of carbon tetrachloride (CCl₄) in OU-2 alluvial/colluvial groundwater during fourth quarter 1993 were detected at the 903 Pad (Figure 2.6-8). The maximum observed concentration during this period was 26,000 µg/l at well 06691. CCl₄ is also present in colluvial groundwater to the south and southeast of the 903 Pad.

The alluvial/colluvial contaminant plume originating in the 903 Pad Area extends to the northeast along the medial paleoscour and toward the Northeast Trenches Area. In the vicinity of the Northeast Trenches, the concentration of CCl₄ ranges from less than 50 µg/l to 360 µg/l. The zone of saturated alluvium does not extend to IHSS 110 during fourth quarter 1993; therefore, no CCl₄ contamination is indicated for the alluvium at that location.

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Based on the areal extent of the contaminant plume, the primary sources of CCl₄ to the saturated alluvial groundwater appear to be the 903 Pad and Trench T-2.

The isoconcentration map of CCl₄ for the No. 1 Sandstone Unit shows high concentrations west of the 903 Pad, in the Northeast Trenches Area, and in the area east of the 903 Pad (Figure 2.6-9). Migration of contaminated groundwater from the alluvium/colluvium to the No. 1 Sandstone Unit appears to have occurred in these areas west of the 903 Pad where the alluvium and No. 1 Sandstone Unit exhibit a high degree of hydraulic communication (Figures 2.5-1 and 2.5-5). Some migration of contaminated groundwater may have occurred from the saturated alluvium in the medial paleoscour to the No. 1 Sandstone Unit in the vicinity of wells 01991 (sandstone) and 13491 (alluvium), east of the 903 Pad where the sandstone subcrops to the alluvium. The primary source of contamination in the No. 1 Sandstone Unit in the Northeast Trenches Area is likely the trenches in that area. Hydraulically upgradient (south) of the trenches, the concentrations are significantly lower than observed concentrations in the vicinity and downgradient (north) of the trenches.

2.6.2.2 <u>Chloroform</u>

The highest concentrations of chloroform (CHCl₃) in OU-2 alluvial/colluvial groundwater during fourth quarter 1993 were detected at the 903 Pad (Figure 2.6-10). The maximum observed concentration during this period was 24,000 µg/l at well 06691. CHCl₃ is also present in colluvial groundwater to the south (Trench T-2 area) and southeast of the 903 Pad.

It is believed that the contaminant plume originating at the 903 Pad is transported in the alluvium through the medial paleoscour to the northeast. However, the observed concentrations of CHCl₃ decrease dramatically just east of the 903 Pad. In the vicinity of the Northeast Trenches, the highest observed concentration during fourth quarter 1993 was 28 ug/l.

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The highest CHCl₃ concentrations in the No. 1 Sandstone Unit (Figure 2.6-11) were detected in the areas west of the 903 Pad and the Northeast Trenches, particularly at IHSS 110. At well 24193, near the center of IHSS 110, the concentration of CHCl₃ was observed to be 220 µg/l during October 1993. The 903 Pad and IHSS 110 are considered to be source areas for CHCl₃.

2.6.2.3 <u>Tetrachloroethene</u>

The highest concentrations of tetrachlorethene (PCE) in OU-2 alluvial/colluvial groundwater during fourth quarter 1993 were detected at the 903 Pad (Figure 2.6-12). The maximum observed concentration during this period was 12,000 µg/l at well 08891. PCE is also present in colluvial groundwater to the south (Trench T-2 Area) and southeast of the 903 Pad.

The contaminant plume originating at the 903 Pad is transported in alluvium through the medial paleoscour to the northeast. This is indicated by the concentration of PCE at well 00191 (1,200 μ g/l) northeast of the 903 Pad. The medial paleoscour plume appears to extend to the Northeast Trenches Area where the concentrations range from less than 50 μ g/l to 71 μ g/l (wells 507891 and 4286, respectively).

The highest PCE concentrations in the No. 1 Sandstone Unit (Figure 2.6-13) were detected in the Mound Area, and in the Northeast Trenches, particularly IHSS 110. At well 02291, the concentration during fourth quarter 1993 was 2,400 µg/l. At well 24193, in the Northeast Trenches Area, the concentration of PCE was observed to be 880 µg/l during October 1993. IHSS 110 is considered to be a source area for PCE. Concentrations of PCE north of the trenches indicate that contaminants migrate to the north in the No. 1 Sandstone Unit.

The contaminants shown east of the 903 Pad in the No. 1 Sandstone Unit may have been transported to that area within alluvial/colluvial groundwater originating at the pad. The 903

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Pad is considered to be a source of PCE contamination to both alluvium/colluvium and the No. 1 Sandstone Unit.

2.6.2.4 <u>Trichloroethene</u>

The highest concentrations of trichloroethene (TCE) in OU-2 alluvial/colluvial groundwater during fourth quarter 1993 were detected at Trench T-2 (Figure 2.6-14). The maximum observed concentration during this period was 58,000 µg/l at well 07391. TCE is also present in the 903 Pad Area, where the maximum observed concentration was 2,200 µg/l (well 08891), and in the Northeast Trenches Area, where the maximum concentration was 37 µg/l (well 4286).

The contaminant plume originating at Trench T-2 is transported in colluvium down the hillside to the south toward Woman Creek. The plume originating at the 903 Pad appears to migrate to the northeast in the paleoscour, as indicated by the concentration of TCE at well 00191 (210 μ g/l), east of the 903 Pad. The medial paleoscour plume appears to extend to the Northeast Trenches Area where TCE concentrations range from less than 5 μ g/l to 370 μ g/l (well 4286).

The highest TCE concentrations in the No. 1 Sandstone Unit (Figure 2.6-15) were detected in the Northeast Trenches, particularly north of Trench T-4. At well 3687, the concentration of TCE was observed to be 47,000 µg/l during October 1993. Trench T-4 is considered to be a source area for TCE groundwater contamination.

Concentrations of TCE from No. 1 Sandstone Unit wells in the vicinity of Trench T-3 ranged from 40 to 72 μ g/l during fourth quarter 1993. This range is similar to the concentrations observed in samples from the period beginning first quarter 1992 through third quarter 1992, when concentrations ranged from 53 to 95 μ g/l (DOE 1993b).

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2.6.2.5 Total Volatile Organics

The highest concentrations of total VOCs in alluvial/colluvial groundwater are present in the 903 Pad Area and in the Trench T-2 Area (Figure 2.6-16). The maximum observed concentrations of total VOCs were approximately 60,000 µg/l at both well 07391, located in the Trench T-2 Area, and well 06691, located at the 903 Pad.

Contamination in alluvial groundwater at the 903 Pad is believed to migrate in the medial paleoscour to the northeast toward the southern edge of the Northeast Trenches. Concentrations decrease in the northeasterly direction. Contamination in the Trench T-2 Area migrates to the south in colluvium, as shown by decreasing concentrations in that direction.

The highest concentrations of total VOCs in the No. 1 Sandstone Unit were observed in the Northeast Trenches Area (Figure 2.6-17). Contaminants migrate to the north along the direction of groundwater flow in this unit. The highest concentrations have been observed at well 3687, where the concentration was approximately 50,000 µg/l in fourth quarter 1993. Total VOC concentrations of approximately 5,000 µg/l were also observed at IHSS 110.

2.6.2.6 Groundwater Sampling Results from SVE Pilot Tests

Groundwater was extracted from the No. 1 Sandstone Unit at extraction well 24913, as part of SVE Pilot Tests 3 and 4 (Figure 2.4-1). Samples of the extracted groundwater were collected from a sample port on the transfer line that carried discharges from well 24193 to storage tanks. Fourth quarter 1993 samples were collected in accordance with Rocky Flats Standard Operating Procedures (SOPs), a process that involves purging wells by bailing, followed by sampling by bailer. The pilot test groundwater sampling was performed in conjunction with the pumping of thousands of gallons of water from the extraction well to the storage tanks. A total of four groundwater samples were collected in March 1994.

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Groundwater concentrations for the VOCs described in Sections 2.6.2.1 to 2.6.2.4 were also evaluated for the pilot tests samples. These samples were analyzed by two methods, VOACLP and VOA524.2. The concentration ranges for the VOCs are described below. Analytical results are also presented in Appendix C3.

Carbon Tetrachloride

The concentrations for CCl₄ ranged from 290 to 1,800 µg/l for Method VOA524.2 for the March 1994 samples. The range for Method VOACLP was 390 to 170 µg/l. During fourth quarter 1993, the concentration of CCl₄ from well 24193 was 3,800 µg/l.

Chloroform

The concentration range for Method VOA524.2 detections of CHCl₃ was 14 to 160 μ g/l during the March 1994 sampling. VOACLP results ranged from 15 to 140 μ g/l during this period. The concentration of CHCl₃ at well 24193 during fourth quarter 1993 was 220 μ g/l.

Tetrachloroethene

The concentration range for Method VOA524.2 analysis of PCE during March 1994 was 410 to 3,800 μ g/l. The VOACLP analysis results indicated a concentration range from 670 to 2,400 μ g/l. The fourth quarter well 24193 concentration of PCE was 880 μ g/l.

Trichloroethene

The range for TCE detections was 45 to 140 μ g/l for VOA524.2 analysis of March 1994 samples. The VOACLP analysis results indicate a range from 46 to 110 μ g/l. The fourth quarter 1993 concentration of TCE was 72 μ g/l at well 24193.

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2.6.2.7 Groundwater Sampling Results from WARP Wells

Prior to abandonment during the well abandonment and replacement program (WARP), Arapahoe Formation No. 1 Sandstone wells 24193, 24393, 24993, and 25093, groundwater samples were collected as shown on Figure 2.4-1. The collection of the samples was in accordance with RFETS SOPs. The collection method and sampling intervals are discussed in Section 2.2.2 and are presented on Table 2.6-2. The analytical data are also presented in Appendix C3.

Eight VOCs (1,1,1-TCA, 1,1-DCE, CCl₄, CHCl₃, cis-1,2-DCE, methylene chloride, PCE, and TCE) were detected in the groundwater samples collected from Arapahoe Formation No. 1 Sandstone wells (24193, 24393, 24993, and 25093). Table 2.6-2 shows the number of detections, the minimum and maximum concentration, and the average concentration for each detected VOCs and depth of sample collection (i.e., top of groundwater or bottom of well). Concentration ranges for these VOCs are described below:

1,1,1-Trichloroethane

The concentrations for 1,1,1-TCA ranged from 14-140 μ g/l in the samples collected prior to abandonment of these wells. The maximum concentration of 1,1,1-TCA was detected in a sample collected from the top of groundwater in well 24193.

1,1-Dichloroethene

The concentrations for 1,1-DCE ranged from 9 to 180 μ g/l in the samples collected prior to abandonment of these wells. The maximum concentration of 1,1-DCE was detected in a sample collected from the bottom of well 24193.

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Carbon Tetrachloride

The concentrations for CCl₄ ranged from 490 to 5,200 µg/l in the samples collected prior to abandonment of these wells. The maximum concentration of CCl₄ was detected in a sample collected from the top of groundwater in well 24193.

Chloroform

Chloroform was detected in all samples collected from these wells prior to their abandonment and ranged in concentrations from 22 to 340 µg/l. The maximum concentration occurred in a sample collected from the top of groundwater in well 24193.

cis-1,2-Dichloroethene

cis-1,2-Dichloroethene was detected in 50% of the groundwater samples collected from these wells prior to their abandonment and ranged in concentrations from 8 to 11 μ g/l. The maximum concentration occurred in the groundwater sample collected from the top of groundwater in well 24393.

Methylene Chloride

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Methylene chloride was detected in approximately 63% of the groundwater samples analyzed from these wells prior to their abandonment and ranged in concentrations from 8 to 47 μ g/l. The maximum concentration was occurred in the groundwater sample collected from the bottom of well 24193.

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Tetrachloroethene

Tetrachloroethene was detected in all the groundwater samples collected from these wells prior to their abandonment and ranged from 250 to 1,600 µg/l. The maximum concentration occurred in the groundwater sample collected from the top of groundwater in well 24193.

Trichloroethene

Trichloroethene was detected in all the groundwater samples collected from these wells prior to their abandonment and ranged in concentration from 40 to 110 µg/l. The maximum concentration occurred in the groundwater sample collected from the top of groundwater in well 24193.

2.6.2.8 **Summary**

Isoconcentration contour maps were prepared for UHSU groundwater VOCs (1,1-DCE, CCl₄, CHCl₃, methylene chloride, PCE, and TCE). The isoconcentration maps show that the major areas of VOC (CCl₄, CHCl₃, 1,1-DCE, PCE, and TCE) occurrence in the alluvium/colluvium are beneath and east of the 903 Pad; in the vicinity of Trench T-2, south of the 903 Pad (CCl₄, CHCl₃, 1,1-DCE, PCE, and TCE); in the Mound Area at the Mound Site (PCE and TCE); in the vicinity and north of the Northeast Trenches (PCE and TCE); and to a lesser extent, the Southeast Trenches (PCE and TCE).

The major areas of VOC occurrence in the No.1 Sandstone are east and west of the 903 Pad (CCl₄, CHCl₃, 1,1-DCE, PCE, and TCE); two areas in the Mound Area (PCE and TCE); and the Northeast Trenches Area (CCl₄, CHCl₃, 1,1-DCE, PCE, and TCE).

The highest VOC concentrations detected in the UHSU groundwater were 140,000 μ g/l (TCE, well 07391 in the colluvium south of Trench T-2); 39,000 μ g/l (CHCl₃, well 06691 in the

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alluvium beneath the 903 Pad); 17,000 μ g/l (CCl₄, well 08891 in the alluvium beneath the 903 Pad); and 14,000 μ g/l (PCE, well 08891 in the alluvium beneath the 903 Pad).

The potential for the occurrence of VOC dense nonaqueous phase liquids (DNAPLs) in groundwater appear to be greatest for CCl₄, PCE, and TCE, based on the observation of groundwater concentrations that exceed 1 percent of the chemical solubility. Potential DNAPLs in groundwater could exist beneath the 903 Pad (CCl₄, PCE, and TCE), in the vicinity of Trench T-2 (PCE and TCE), north and northeast of the Mound Site (PCE), and north of Trench T-4 in the Northeast Trenches (TCE). Direct evidence of DNAPLs in groundwater was not observed during the Phase II RFI/RI programs.

VOCs are widely distributed across the portion of OU-2 between the western boundary and the East Spray Fields and are closely associated with identified IHSS areas. In particular, VOCs are prevalent in the 903 Pad Area (beneath and around Trench T-2 and the 903 Pad), in the Mound Area, and in the Northeast Trenches Area. The most prevalent VOCs appear to be 1,1,1-TCA, 1,1-DCA, and 1,2-DCE.

Detections of SVOCs in UHSU groundwater are limited to a few compounds: benzoic acid, bis(2-ethylhexyl)phthalate, diethyl phthalate, di-n-butyl phthalate, and heptachlorepoxide. Those compounds are detected infrequently in a few wells generally at concentrations less than about 20 μ g/l.

No pesticides or PCBs were detected in UHSU groundwater during the Phase II RFI/RI investigations.

Am-241, Pu-239/240, and U-238 are potential waste-related contaminants in UHSU groundwater. Am-241 and Pu-239/240 occurred in filtered and unfiltered UHSU groundwater samples collected in the vicinity of the 903 Pad. U-238 occurred in groundwater primarily

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in the vicinity of Trench T-2. Radionuclide contamination could be associated with high concentrations of VOCs observed in the UHSU in the 903 Pad Source Area.

2.6.3 Soil Gas

Two Soil Gas Surveys (SGSs) were performed in and around Trench T-3 (IHSS 110). Both a shallow (near surface, less than 5 feet deep) and a deeper (5 and 10 feet below grade) survey were performed in 1993, as discussed in the Soil Vapor Survey Report (DOE 1994b). Figures 2.6-18 through 2.6-23 illustrate the results for CCl₄, PCE and TCE from the deeper SGS. Findings of the SGSs are summarized below.

The shallow SGS survey included analyses for the following VOCs:

- 1,1-DCE
- trans-1,2-dichloroethene (trans-1,2-DCE)
- cis-1,2-dichloroethene (cis-1,2-DCE)
- 1,1-DCA
- 1,2-DCA
- CCl₄
- PCE
- TCE
- vinyl chloride
- Total VOCs

1,1-DCE, trans-1,2-DCE, cis-1,2-DCE, and 1,2-DCA were not detected in the soil vapor. 1,1-DCA was detected at 16 of 35 sampling locations, and concentrations ranged from 40 to 1,900 μ g/l. CCl₄ was detected at 18 of the 35 sampling locations with concentrations ranging from 0.36 to 111 μ g/l. TCE was detected at 14 of the 35 sampling locations with concentrations ranging from 1.2 to 21 μ g/l. PCE was detected at 22 of the 35 sampling

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locations with concentrations ranging from 0.11 to 410 μ g/l. Vinyl chloride was detected at two sampling locations at concentrations less than 23 μ g/l.

Review of the spatial distribution of the soil gas data in Trench T-3 indicates that CCl₄ was found only in the west end of the trench (west of borehole 10191). PCE in soil gas is located in the west central part of Trench T-3 (located east of borehole 10191 and around the SVE wells and boreholes). TCE in soil gas is similar in location to the PCE plume. Two elevated total VOC concentration areas were observed in and around Trench T-3. One area is located in the west central part of Trench T-3 (near the SVE wells and boreholes) and the second is located in the western end of Trench T-3 (west of borehole 10191).

The two deeper SGSs (depths of 5 and 10 feet) included analyses for the following VOCs:

- 1,1-DCA
- CCI₄
- PCE
- TCE
- Total VOCs

Based on the evaluation of soil gas results obtained from the 5-foot sampling interval, total VOCs appear to be prevalent in the western portion of Trench T-3 (around borehole 10191) (Figure 2.6-21). However, the CCl₄ soil vapor plume extends west of the Trench T-3 boundary, while 1,1-DCA, PCE, and TCE soil vapor plumes are located in the western portion of Trench T-3 (Figure 2.6-18 through 2.6-22).

Review of the soil gas data obtained from the of 10 foot depth interval indicates that total VOCs, CCl₄, and PCE were observed at higher concentrations than at the 5-foot depth and higher concentrations were generally located near sampling location 110-29. 1,1-DCA was

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not detected at the 10-foot depth interval sample, and TCE was detected at relatively low concentrations (Figures 2.6-22 through 2.6-25).

2.6.4 NAPL

The constituents detected in the liquid collected from location 25194 in November and December of 1994 are discussed in this section. The field sampling techniques and analytical methods and procedures are discussed in Section 2.2.1 and the analytical data is presented in Appendix C5-1 through C5-3. The constituents detected are discussed by analytical method for each layer analyzed. Figures 2.6-28 and 2.6-29 present a summary of the constituents detected. Analytical results for each distillation sample and review of the distillation test results are discussed in Section 2.6.5.

2.6.4.1 **VOCs**

The grab liquid samples for analytical testing collected from borehole 25194 in November, 1994, were submitted for analysis by EPA Methods 8260 (VOA), 8270 (SVOA), modified 8015 (TPH) and a radionuclide screen. The two distinct layers (the floating phase and the aqueous phase) were analyzed separately by each method except for the radionuclide screen. Figure 2.6-26 presents the detected constituents for each layer (i.e., floating and aqueous) collected from borehole 25194.

Nine VOCs (1,1,1-TCA, 1,1-DCA, acetone, CHC1₃, ethylbenzene, m,p-xylene, o-xylene, PCE and TCE) were detected in the floating layer.

Ten VOCs (1,1,1-TCA, 1,1-DCA, 2-butanone, acetone, CHCl₃ m,p-xylene, methylene chloride, o-xylene, PCE and TCE) were detected in the aqueous layer of the grab sample collected from borehole 25194, as shown on Figure 2.6-26.

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Two VOCs (PCE and TCE) were detected in the floating layer (1) from the liquid samples collected in December, 1994, as shown on Figure 2.6-27.

Two VOCs (PCE and TCE) were detected in the floating layer (2) from the liquid samples collected in December, 1994, as shown on Figure 2.6-27.

Two VOCs (TCE and PCE) were detected in the VOA sample prepared from the aqueous layer of the December, 1994 samples, as shown on Figure 2.6-27.

2.6.4.2 **TPH**

The floating layers (1 and 2) and the aqueous layer (3) of the December NAPL were submitted for analysis by modified Method 8015 (8015m). Although the TPH results were reported back as Gasoline Range Organics (GRO) (C_6 through C_{12}) and Diesel Range Organics (DRO) (C_{12} - C_{24}), gasoline and diesel were not implicitly identified; this was evident by the data qualifiers and the report narrative submitted by the laboratory. Each of the GRO and DRO results for these samples were qualified with a G or X to indicate that the sample peak patterns did not match the peak patterns of the gasoline or diesel standards. See Section 2.5.6.3 for further details regarding the identification and quantification of GRO and DRO components.

A report narrative was not available for the two layers of the November NAPL sample; however, the data qualifier assigned to the gasoline result was identical to that of the December sample (the data qualifier was G), indicating that although hydrocarbons were found in the same hydrocarbon range as gasoline, the peak pattern did not match the gasoline standard. The diesel result was not qualified. The data received for the November NAPL were preliminary (i.e., draft).

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Hydrocarbons were detected in the C_6 through C_{12} (C_6 - C_{12}) range and C_{12} through C_{24} (C_{12} - C_{24}) range in the floating phase of the November sample. The gasoline result was qualified with a G, indicating that the peak pattern did not match the peak pattern of the gasoline standard.

Hydrocarbons were detected in the C_6 - C_{12} and the C_{12} - C_{24} range in the floating layer (1) from the December, 1994 sample. Hydrocarbons were also detected in the C_6 - C_{12} and the C_{12} - C_{24} range in the floating layer (2). Hydrocarbons in the C_6 - C_{12} and C_{12} - C_{24} ranges were also detected in the aqueous layer. Each of these results was qualified with a G or X; these are discussed in more detail in Section 2.5.6.3.

2.6.4.3 **SVOCs**

Nine SVOCs (2,4-dimethylphenol, 2-methylnaphthalene, 2-methylphenol, 4-methylphenol, bis[2-ethylhexyl]phthalate, di-n-butyl phthalate, fluorene, naphthalene, and phenanthrene) were detected in the floating layer (sample number 95N0058, November 1994). Two of the nine SVOCs detected were phthalates: bis[2-ethylhexyl]phthalate and di-n-butyl phthalate. Four of the nine SVOCs detected were PAHs: 2-methylnaphthalene, fluorene, naphthalene, and phenanthrene. The remaining three SVOCs detected were phenols: 2,4-dimethylphenol, 2-methylphenol, and 4-methylphenol.

Five SVOCs (2-methylphenol, 4-methylphenol, bis[2-ethylhexyl]phthalate, di-n-butyl phthalate, and phenanthrene) were detected in the aqueous layer sample (sample number 95N0058, November 1994).

Seven SVOCs (naphthalene, 2-methylnaphthalene, phenanthrene, di-n-butylphthalate, pyrene, chrysene, and bis[2-ethylhexyl]phthalate) were detected in the floating layer (1) from the December sampling event.

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Six SVOCs (naphthalene, 2-methylnaphthalene, fluorene, phenanthrene, di-n-butylphthalate, bis[2-ethylhexyl]phthalate) were detected in the floating layer (2) from the December sampling event.

Eleven SVOCs (phenol, 2-methylphenol, 4-methylphenol, 2,4-dimethylphenol, naphthalene, 2-methylnaphthalene, fluorene, phenanthrene, di-n-butyl phthalate, chrysene, and bis[2-ethylhexyl]phthalate) were detected in the aqueous layer from the December sampling event.

Semivolatile TICs were detected in the floating layer (1) (sample number C0639-03), the floating layer (2) (sample number C0640-05), and the aqueous layer (sample number C0670-05) from the December sampling event. See Section 2.6.5.2 for a discussion of the TICs.

2.6.4.4 Radionuclides

The radionuclide screen performed on the sample collected from borehole 25194 in November 1994 prior to shipment indicated a gross alpha activity of 749,000 pCi/L and a gross beta activity of 803,000 pCi/L.

The radionuclide screen performed on the floating layer (1) from the sample collected from extraction well 25194 in December, 1994 indicated a gross alpha activity of 19,400 pCi/L and gross beta activity of 42,000 pCi/L. Radionuclide analysis for Am-241, Pu-239/240, U-233/234, U-235, and U-238 were performed on the floating layer (1).

One radionuclide screen was performed on the floating (2) and aqueous layers. The gross alpha and gross beta activities were 22,600 and 39,400 pCi/L, respectively. Separate select radionuclide analyses were performed on the floating (2) (sample number C0640) and aqueous layers (sample number C0670) for Am-241, Pu-239/240, U-233/234, U-235, and U-238. Am-241 was detected at an activity of 0.008 pCi/g in the floating layer (2) and at an activity of

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1.62 pCi/g in the aqueous layer. Pu-239/240 was detected at an activity of 0.029 pCi/g in the floating layer (2) and at an activity of 1.16 pCi/g in the aqueous layer. U-233/234 was detected at an activity of 1.96 pCi/g in the floating layer (2) and at an activity of 398 pCi/g in the aqueous layer. U-235 was detected at an activity of 0.35 pCi/g in the floating layer (2) and at an activity of 101 pCi/g in the aqueous layer. U-238 was detected at an activity of 15.5 pCi/g in the floating layer (2) and at an activity of 3,240 pCi/g in the aqueous layer. In general, the activities in the aqueous layer were two orders of magnitude higher than the floating layer (2).

2.6.5 Sample Collection for Distillate Test and Numbering Overview

The NAPL sample collected in the field on December 20, 1994, was biphasic. Each phase was bottled (4 liters of each phase was collected), labeled, and recorded on the chain of custody as separate sample numbers. The floating phase was labeled CO639 (1), and the bottom water phase was labeled CO640 (2).

While inroad to the laboratory, sample number CO640 separated again, into a top and bottom phase. The laboratory separated the two phases (using 1 or 2 liters, and the VOC vials for CO640) and created a third sample, CO670. Sample CO640 was the top floating, and CO670 the bottom phase. However, the sample aliquot contained in the VOC vial for CO640 was not biphasic, and the laboratory used that vial (not realizing it was one phase because the vial was amber) to create the third volatile sample (number CO670-04). The results for the volatile analysis on samples CO640-04 and CO670-04 are, therefore, nearly identical. Table 2.2-2 summarizes how these samples were numbered, and the analytical testing that was performed for each sample. A description of the original sample and the phases is also provided in Section 2.2.1.

The remaining 2 liters of CO640 was used for the distillation analysis. Each liter contained approximately 50% upper phase (floating) and 50% lower phase (bottom water phase). The

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distillation was performed on the combined phases, and resulted in 16 fractions, each of which, were analyzed by Methods 8260, 8270, and 8015M. Table 2.2-3 summarizes how the distillate fractions were numbered, and the analytical testing that was performed for each fraction. A brief description of the distillation procedure is also provided in Section 2.2.1.

In general, each phase of the original sample (samples CO639, CO640, and CO670), and the distillate fractions originating from the original sample CO640, were analyzed by Methods 8260, 8270, and 8015M. Radionuclides were also analyzed for samples CO640 and CO670. The following sections address the organic analyses only.

Tables 2.6-3 through 2.6-10 tabulates the target analytes that were detected in each of the distillate fractions. The following sections (2.6.5.1 through 2.6.5.4) provide a discussion of those results. Figure 2.6-30 depicts the sample numbering scheme for the original December NAPL sample, the top floating, the bottom water phase, and the distillate fractions from the combined phases of C640.

2.6.5.1 Analytical Data Review

The objective of this data review was to identify the major chemical components present in the December NAPL sample. This was accomplished by performing a cursory review of the data; it did not entail a full data validation. Data validation was still pending when this report was prepared. The review of the data included looking at the target compounds detected in each fraction, the tentatively identified compounds (TICs) from Methods 8260 and 8270, and the chromatograms from the modified Method 8015 analysis. (Radionuclide data are not addressed in this discussion)

The data reviewed were from the original NAPL collected on December 20, 1994 (sample numbers CO639, CO640 - top floating, and CO670 - bottom water phase) and the distillate fractions that were generated from the combined phases of sample CO640.

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Electronic Data

Electronic data for Methods 8015M, 8260, and 8270 were received for the NAPL sample fractions collected on December 20, 1994, and the subsequent distillate samples. Due to dilutions performed for Methods 8260 and 8270, duplicate analytical records were present in the electronic deliverable. The duplicate records were eliminated, thus creating a working dataset, using the following selection criteria:

- Chemicals that were not detected in the undiluted analysis were retained in the working dataset. There were some exceptions of target analytes that were not detected in the undiluted run, but had a reported concentration in the diluted analysis. In these cases, the result in the diluted analysis was retained.
- Chemicals that exceeded calibration range (E qualified data) in the undiluted analysis were eliminated. The reported concentration from the diluted analysis was retained. There was one exception of 4-methylphenol that was E qualified in both the undiluted and diluted analysis. In this case, the highest reported concentration was retained.
- Chemicals that did not exceed the calibration range in the undiluted analysis, but had reported concentrations in both runs, were selected based on the highest concentration reported.

Hardcopy Data

Raw data (i.e., extraction logs, chromatograms, and mass spectra) for Methods 8015M, 8260, and 8270 were obtained for the NAPL sample collected on December 20, 1994, and the subsequent distillate samples. The raw data were primarily used to evaluate tentatively identified compounds (TICs) for Methods 8260 and 8270. The chromatograms generated by

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Method 8015M were also looked at in an effort to obtain additional information regarding the types of hydrocarbons potentially present in the NAPL sample. The raw data were not used to validate the data.

2.6.5.2 <u>Methods 8260 and 8270 Overview</u>

Target Compounds and Tentatively Identified Compounds (TIC)

Target compounds refer to a specific list of analytes to be quantified in an environmental sample. Analytical standards for target compounds are contained in the calibration standard for the method being performed. These standards are also measured in laboratory control samples and matrix spike samples. Therefore, it is possible to accurately quantitate target compounds in environmental samples (barring matrix interference or other anomalous analytical conditions). Similarly, the analytical standards provide mass spectral information which facilitates accurate identification of target compounds in environmental samples.

Tentatively identified compounds (TICs) apply to methods (i.e., Methods 8260 and 8270) which use gas chromatography/mass spectrometry (GCMS) instrumentation. TICs are non target compounds that can be detected in an environmental sample but do not meet the identification criteria of target compounds, internal standards, or surrogates. For each environmental sample, a mass spectral library search can be conducted to tentatively identify non target compounds. Contract Laboratory Program (CLP) protocol states that a mass spectral library search will be made for up to 20 extraneous compounds of the greatest apparent concentration. The mass spectral library is a compilation of spectra for 50,000 (or more) compounds. Tentative identification is based on an electronic library search and/or a visual comparison of the TIC spectra in the environmental sample against a similar spectra found in the mass spectra library, and is not absolute. TIC quantitation is estimated because the mass spectra and reported concentration are not compared to a standard.

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Target Compounds - Distillate Samples

The target compounds identified for this project included the CLP Target Compound List (TCL) for volatiles and semivolatiles; pesticides/PCBs were not included. TCL analytes that were frequently detected in the distillate fractions included tetrachloroethene (PCE), trichloroethene (TCE), acetone, phenol, 2,4-dimethylphenol, ortho and meta cresol, naphthalene, phenanthrene, and 2-methylnaphthalene. TCL analytes that were infrequently detected included bis(2-ethylhexyl)phthalate, di-n-butylphthalate, and methylene chloride; although these are common laboratory contaminants, the reported concentrations were not B qualified by the laboratory. That is, the associated method blanks did not have reported concentrations of these common laboratory contaminants. There was one occurrence of benzyl alcohol (160 ppb at a reporting limit of 250 ppb) in sample CO643.

Acetone was B qualified in two instances, however, the amount detected in the associated method blank was negligible (9.2 ppb with reporting limit of 10 ppb) by comparison to the concentration found in the samples (i.e., 22,000,000 ppb with a reporting limit of 12,000,000 ppb). Other samples showed similarly high concentrations of acetone that were not B qualified.

There were four instances of PCE sample results that were B qualified. The concentration in the associated liquid waste method blanks were 530 ppb and 560 ppb, both at a reporting limit of 635 ppb. The concentrations of PCE detected in three of the samples (CO644, CO647, and CO704) exceeded the amounts detected in the method blank by factors of 1000 or more. Sample CO703 had less than 5 times (1,700 ppb at a reporting limit of 620 ppb) the amount of PCE detected in the associated method blank. The PCE detected in CO703, therefore, may be considered suspect according to the Environmental Protection Agency (EPA) National Functional Guidelines for Organic Data Review.

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Distillate sample CO647 had m,p-Xylenes below the reporting limit (e.g., J qualified). Sample CO648 reported all of the xylene isomers (o,m, and p) above the reporting limit, but at relatively low concentrations compared to the amounts of PCE and semivolatiles present. CO648 also had ethylbenzene below the reporting limit (e.g., J qualified). Sample CO703 was the only sample that had benzene, toluene, and ethylbenzene concentrations above the reporting limit; m,p-Xylenes were also present, but J qualified. Sample CO703 also had carbon disulfide detected at 9,400 ppb with a reporting limit of 620 ppb. These samples also showed significantly decreased concentrations of PCE, TCE, and the semivolatiles. Sample CO703, in particular, did not have any PCE detected and the TCE was J qualified. The traces of BTEX detected in these samples may not have been detected in other samples because of significant dilutions and/or matrix interferences. The BTEX components may also be breakdown products from the distillation process.

TICs - Distillate Samples

The total concentrations of volatile TICs ranged in concentration from 18,000 ppb in sample CO698 to 16,600,000 ppb in sample CO647. Volatile TICs were reported for samples CO645, CO647, CO648, CO649, CO698, CO703, CO704, and CO705. TICs were not detected in CO641, CO642, CO643, CO644, and CO646. The occurrence of TIC detections and reported concentrations (or lack of) for each of the samples appeared to be directly proportional to the amount of PCE and TCE present in the samples (i.e., higher concentrations of PCE and TCE resulted in lower concentrations and fewer detections of TICs). Samples containing high concentrations of PCE and/or TCE were probably diluted to the extent that the TICs were not measurable. Most of the volatile TICs were reported as unknown hydrocarbons (alkanes and alkenes). Some volatile TICs were identified as substituted benzenes.

Semivolatile TICs were detected in all of the distillate samples. PCE was tentatively identified in concentrations ranging from 46,000 ppb in sample CO643 to 1,000,000,000 ppb

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in sample CO644. Samples CO641, CO642, CO643, CO644, CO645, CO646, and CO647 had PCE tentatively identified in the semivolatile fractions. Most of the semivolatile TICs were reported as unknown hydrocarbons (alkanes, alkenes, and cyclo alkanes). There were some TICs that looked like remnants of target compounds; these included substituted benzenes, substituted naphthalenes, alcohols, and glycol. A small percentage of semivolatile TICs were tentatively identified as camphene and limonene (i.e., terpines).

As mentioned in the Method 8260 and 8270 overview, the reported concentrations for all TICs are estimated values, and do not reflect an exact quantitation.

December NAPL before Distillation

Volatile TICs were not detected in CO639-02, CO640-04, and CO670-04; however, due to extremely high concentrations of PCE and TCE, these samples were significantly diluted (i.e., dilution factors of 10,000). The samples were probably diluted to the extent that the TICs were not measurable. PCE and TCE were the only target compounds detected.

Semivolatile TICs were detected in CO639-03, CO640-05, and CO670-05. The TICs reported were similar to those found in the distillate samples, except that PCE was not identified and there were fewer instances of specific compound groups reported (i.e., most of the TICs were reported as unknown hydrocarbons).

Target compounds that were detected in samples CO639-03, CO640-05, and CO670-05 by Method 8270 included 2-Methylnaphthalene, Phenanthrene, bis(2-Ethylhexyl)phthalate, and di-n-Butylphthalate. Concentrations of Naphthalene and 2-Methylnaphthalene were greatest in CO640-05 and CO639-03 respectively; however, none was detected in CO670-05. Phenol, 2-Methylphenol, 4-Methylphenol, and 2,4-Dimethylphenol were detected only in sample CO670-05. However, these compounds were detected in some of the distillate fractions originating from CO640. It is presumed that the original sample, before distillation, was

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diluted to the extent that these compounds (Phenol, 2-Methylphenol, 4-Methylphenol, and 2,4-Dimethylphenol) could not be measured.

2.6.5.3 Modified Method 8015 Overview

Modified Method 8015 is a gas chromatography (GC) method that was used to identify and quantitate gasoline range organics (GRO) (C_6 - C_{12}) and diesel range organics (DRO) (C_{12} - C_{24}). Simply stated, any hydrocarbon configuration, that fell within these ranges (C_6 - C_{24}) may have been detected. However, the hydrocarbon peak patterns must match the peak patterns of the gasoline or diesel calibration standard before it can be identified as gasoline or diesel.

The December NAPL samples contained C_6 - C_{24} hydrocarbons, but the hydrocarbon peak patterns did not match the peak patterns of the gasoline or diesel calibration standards. This was indicated by the qualifiers (X, Y, or G) that were added to each of the GRO and DRO results. As stated in the report from the laboratory, these qualifiers were included to indicate that although hydrocarbons were detected in the gasoline and diesel hydrocarbon ranges, the chromatograms did not match the gasoline or diesel calibration standards. A more reliable identification may be made by examining the results from the Methods 8260 and 8270.

The reported concentrations of the hydrocarbons that were present in these samples were based on the quantitation of those hydrocarbons that eluted within the C_6 - C_{12} and C_{12} - C_{24} range. Therefore, this method would not have necessarily detected, or reported, other hydrocarbons that were not within the C_6 - C_{24} range. However, based on sample chromatograms received from the laboratory, and conversations held with the laboratory's coordinator of petroleum analyses, it was possible to determine that some hydrocarbons heavier than diesel may be present in some of the fractions. This observation is based on hydrocarbon retention time markers (i.e., elution times for specific hydrocarbons) that have been established by the laboratory. These retention time markers (below) are based on gasoline and diesel calibration standards:

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- C₆ hydrocarbons elute at 2 minutes and 47 seconds
- C₁₂ hydrocarbons elute at 12 minutes and 52 seconds
- C₂₄ hydrocarbons elute at 23 minutes and 40 seconds

For example, calibration standards for diesel do not elute after 23 minutes and 40 seconds. For this project, the laboratory performed the method allowing 29 minutes elution time for each sample. The chromatograms for samples CO639-04, CO670-06, and in particular CO640-06, show a definite broad based peak at 25 minutes which tapers off at 29 minutes. This peak, although less pronounced, is also present in some of the distillate fractions originating from CO640-06. The distillate fractions represent the top and bottom layers collected from 106 to 120 degrees centigrade (CO704, CO705, CO649 and CO698), and the residue (CO703). (Method 8015 data are not available for distillate samples collected after 120 degrees centigrade). The presence of a motor oil or industrial lubricant is indicated by these observations.

2.6.5.5 <u>Summary of Analytical Results</u>

This section summarizes the results of Methods 8260, 8270, and 8015M for the December NAPL sample and distillate fractions originating from the oil phase of the NAPL.

The predominant component of the December NAPL sample appears to be PCE, followed by TCE, naphthalene, 2-methylnaphthalene, and the cresols.

PCE and TCE are known for their uses as industrial solvents. PCE can also be used as a drying agent for metals and certain other solids (The Condensed Chemical Dictionary, Tenth Edition, Hawley 1981a).

Naphthalenes and cresols are commonly associated with petroleum products or coal tar. Cresols may also originate from toluene by sulfonation or oxidation. Some uses for cresols

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include disinfectants, ore flotation, textile scouring agent, and surfactants. Uses for naphthalene include cutting fluid and lubricants (Hawley 1981b).

The results of the GRO analysis do not indicate the presence of gasoline. However, the presence of BTEX components in some of the distillate fractions may be indicative of gasoline. It is important to note that the concentrations of BTEX were negligible by comparison to the PCE and TCE, which appear to be the primary components of the NAPL. It is also possible that the occurrence of BTEX components originated from break down products during the distillation process. For instance, although xylenes are commonly related to fuel products, they may be derived from fractional distillation of petroleum (Hawley 1981c).

The results of the DRO analysis do not indicate the presence of diesel, and the discussion included in the report from the laboratory indicated that the hydrocarbon pattern did not look like diesel. As discussed in the overview for Modified Method 8015, the presence of hydrocarbons heavier than diesel are indicated.

2.7 GEOPHYSICAL SURVEY OF TRENCH T-3

2.7.1 Introduction

Surface geophysical survey methods were used as part of the investigation of Trench T-3 within IHSS 110 at the SVE Test Site No. 1 (shown in Figure 1.1-1). The primary objective of the geophysics survey was to obtain subsurface information to help delineate the areal extent of Trench T-3 excavation and the trench edges if possible. An additional objective of the geophysics was to identify the potential existence of metallic debris within the trench. The geophysical methods used were electromagnetics (EM) and ground penetrating radar (GPR).

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2.7.2 Description of Geophysical Methods

2.7.2.1 <u>Electromagnetics</u>

EM methods provide a rapid means of measuring the electrical conductivity of subsurface soil, rock, and groundwater. EM can be useful for assessing subsurface conditions such as depth and orientation of bedrock, presence of ferrous and nonferrous materials, thickness and lateral variations of subsurface units or lateral extent of paleochannels. Specifically at the SVE Test Site, EM was used to assess the variation of conductivity across the site; to obtain information on the potential area of excavation associated with the construction of Trench T-3; and to delineate potential areas of buried metallic debris.

The EM method involves the induction of electrical current into the subsurface. A small alternating current passing through a transmitter coil produces a primary, time-varying magnetic field into the ground. Through inductive coupling, the primary magnetic field produces small eddy currents in the subsurface which, in turn, create their own secondary magnetic field. The receiver coil senses both the primary and secondary fields. Changes in magnitude and phase of the individual currents are converted to voltages and output as ground conductivity values in millimhos (mmhos)/meter on the instrument and recorded manually or by a digital data logger.

The selection of EM instrumentation is dependent on the desired penetration depth. For all available EM instruments, the depth of investigation is related to the separation between the transmitter and receiver coils and the mode of coil orientation (horizontal or vertical). By using multiple coil spacings or orientations, several penetration depths can be achieved, allowing vertical variations of conductivity to be assessed. For shallow less than 15 feet investigations, EM data can be collected with a Geonics EM-31 terrain conductivity meter. The EM-31, which has a fixed spacing of 12 feet, has an effective penetration depth of approximately 15 feet using the vertical dipole mode.

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The EM-31 measures both the quadrature phase component and the inphase component of the induced magnetic field. The quadrature phase is linearly related to the ground conductivity and thus interpretable in terms of subsurface geology, and more specifically in terms of disturbed versus non-disturbed soil. The inphase measurement is the ratio of the induced secondary magnetic field to the primary magnetic field, and is more sensitive to metallic objects than the quadrature phase measurement.

Individual conductivity values are not necessarily diagnostic in themselves. However, the variations in conductivity can indicate changes in subsurface conditions. As an example, trench materials can sometimes produce a conductivity low (depending on the trench fill properties). However, in trenches that contain metallic objects such as drums, a conductivity high might be observed. In some trenches, where significant constituent inhomogeneity exists, the associated EM anomaly can appear as a dipole characterized by both high and low values in close proximity to each other. This is because the EM response can be affected by the interaction between the anomaly-producing body in the subsurface and the orientation of the instrument. Although dipoles can be observed with quadrature data, they are more common with inphase data.

Conductivity values can be plotted and contoured to estimate lateral conductivity variations. Variations in the subsurface conductivity due to buried metallic trench materials generally produce relatively large (greater than 20 mmhos/meter) anomalies (areas where the measured conductivity varies significantly from some background level). However, these anomalies or smaller ones can be masked by the interfering effects of surface debris, buried utilities, overhead utilities and communications apparatus, or any large metal structures close to the survey area.

Interpretation of an EM contour map requires that the basic characteristics and causes of conductivity anomalies be kept in mind. Most types of soil and rock are electrical insulators of high resistivity. The electrical conduction that takes place in the subsurface is primarily

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electrolytic and occurs through the moisture-filled pores and fracture contained in the matrix. If a conductive body such as a metal drum is placed in the matrix, ion flow and conduction occurs preferentially through the metal, thus increasing the bulk conductivity. Conversely, if non-conductive materials such as unreinforced concrete are placed in the matrix, ion flow and conduction occur around the resistor, thus reducing the bulk conductivity. Therefore, landfill areas, which may have buried metallic objects, sludge, or leachate, are generally revealed as conductivity highs, while landfill or hardfill areas, which may have buried concrete, asphalt, wood, or dry backfill soil materials, are generally revealed as conductivity lows. All these facets are superimposed on the geologic framework of the site. Variability of clay and sand layers will produce small conductivity anomalies due to the variable ion flow between the two rock types.

2.7.2.2 Ground Penetrating Radar

GPR using impulse radar technology has been applied for the non-intrusive investigation of shallow subsurface materials. The method has been used for locating voids in concrete or limestone, finding buried pipelines or reinforcement bars, mapping shallow geologic interfaces, and delineating near-surface soil layering. GPR has been shown to be a successful tool for resolving soil stratigraphy, thus allowing the potential delineation of excavation areas associated with buried trenches.

GPR involves transmitting a relatively high-frequency electromagnetic pulse using a transducer antenna into the medium, and recording reflected electromagnetic energy with a receiving antenna. Electromagnetic reflections occur whenever the dielectric constant of the material(s) changes (i.e., metal versus soil). As the antenna is towed along a survey line, the reflected electromagnetic signals are converted to analog (or with some instrumentation digital) signals, processed, and displayed as travel times on a graphic recorder as output. As the transducer is pulled along a transect line, the graphic recorder prints an approximation of

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the interfaces one would see in cross-section. The display is similar to a geologic section, except that the record is a time section rather than a depth section.

An important step in a successful GPR survey is to clearly define the objective target(s) to the degree possible. Fundamental questions must be answered before implementing GPR. Approximate target depths must be evaluated, because at most soil sites typically encountered, GPR is a very shallow investigation tool. Approximate target geometry must also be evaluated to aid in the selection of appropriate data collection density and proper antennas. Electrical properties of the medium must be evaluated to estimate how well the radar signals will penetrate, and to judge whether a sufficient dielectric contrast exists for the target to be detected. And finally, the site environment must be evaluated, such as the presence of metal structures or utility wires, accessibility, the amount of surface vegetation, and the site topography, all of which can contribute to the success or failure of a GPR survey.

The ultimate effectiveness of GPR at a given site is directly proportional to the dielectric properties of the medium through which the signal is transmitted. GPR allows the greatest resolution of subsurface features when favorable conditions exist. However, properties of the medium can effect penetration depths. These depths are primarily controlled by the electrical conductivity of the surveyed medium because the electromagnetic pulses lose energy in the form of heat when transmitted through electrically conductive units. Conductivity of a particular medium is predominantly governed by the water content, amount of salt in solution, and the percentage of conductive clay. Typical penetration depths of GPR are:

- Less than 4 feet through clay
- Over 75 feet through freshwater saturated sands
- Over 30 feet in clean limestone
- Over 230 feet through ice
- Less than 1 foot in seawater

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Thus, the depth of penetration and ultimate effectiveness of GPR is highly site specific. As a result, a feasibility or test study is often conducted to identify the usefulness of GPR on a project-by-project basis.

2.7.3 Field Testing of GPR

An initial test for conducting GPR at the Trench T-3 site was conducted prior to full implementation over the entire site. The study was conducted to test the applicability of GPR specifically to delineate trench edges. Prior to conducting the GPR field test, several questions were answered to aid in the selection of appropriate survey design. The depth of penetration desired was estimated to be 6 to 9 feet, which was the approximate depth of the excavated trenches. Penetration of 3 to 6 feet was thought to be sufficient however, to detect trench edges.

GPR data were collected with a Geophysical Survey Systems, Inc. (GSSI) Subsurface Interface Radar (SIR) System-3. The system included a profiling recorder, control cable, and transmitting and receiving antenna. This system provided instantaneous and continuous profile records of the radar response.

Testing of various GPR data acquisition parameters was conducted as part of the test study. Two antenna frequencies were available for testing, the 300 Mhz and 500 Mhz. During testing, it was concluded that the 300 Mhz would not provide the resolution required for discerning the targets of interest, so the 500 Mhz antenna was used for the rest of the survey. Other data acquisition parameters were tested for optimum data resolution given survey objectives. The following recording parameters were tested:

- Time range for recording
- Signal range gain
- High and low pass filter settings (given time range for recording)

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- Printer speed
- Antenna towing speed

These recording parameters were tested on multiple lines over the western part of Trench T-3. Final data acquisition parameters allowed GPR penetration depths of approximately 4 feet. This minimal penetration was likely due to the significant amount of clay and clayey fill in the upper several feet. However, this penetration was sufficient to detect potential targets associated with the sides of the excavated trench.

After optimization of the data parameters, several test lines with a five foot separation were conducted to determine potential correlation from line to line. Several potentially anomalous areas were observed in the upper 3 to 4 feet of soil material and could be correlated over several lines. Based on the results of the feasibility study, the decision was made to implement GPR data collection over the entire Trench T-3 area.

2.7.4 Field Operations

Subsurface conductivities were measured using the Geonics EM-31 with a data logger over a grid pattern. EM data were collected using a nominal 5-foot station spacing, with a 10-foot separation between transects. Labeling of the lines was from -30 feet to 140 feet. Line 0 was conducted just east of Boring 10191. Transects were conducted in a general north-south direction, perpendicular to the suspected east-west orientation of the trench. Data were collected in the vertical dipole mode (0 to 15 feet penetration) for both the quadrature and inphase data. Readings were collected in a general east-west orientation (parallel to the suspected trench orientation) and north-south (perpendicular to the suspected trench orientation). EM data were input to the computer software GEOSOFT, which was used to grid and contour the data.

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GPR data were collected along north-south trending transects separated by a distance of 10 feet. The GPR lines were conducted along the same transects as the EM. Additionally, a cross line was conducted for correlation purposes. The GPR data acquisition parameters used were derived from the field test, and remained the same for the entire implementation phase. Along each GPR transect, a marker signal was used at each survey flag (nominally 5 feet) during antenna towing to aid correlation of printed records with actual location in the field. Each printed GPR record was annotated with line number, and footage marker (shown by vertical dashed line) along each completed transect. Also shown on the GPR records are horizontal lines for time scaling. Using the time range setting used during data collection, each division between scaling lines is approximately 6 nanoseconds. Based on the approximate velocity of the medium each scaling division would represent an approximate thickness of 3/4 to 1-1/4 feet.

2.7.5 Results

Results of the EM survey are shown in the contour maps of Figures 2.7-1 through 2.7-4. Figures 2.7-1 and 2.7-2 depict results for the quadrature and inphase data for the east-west orientation, respectively. Figures 2.7-3 and 2.7-4 depict the results for the quadrature and inphase data for the north-south orientation, respectively. Also shown on the figures are the interpreted trench edges based on the GPR data (discussed below).

Quadrature values for both orientations varied from 15 to 69 mmhos/meter. Inphase values for both orientations varied from 32 to 33 parts/thousand. The highest quadrature values are observed from Line 10 to Line 30 (Figure 2.7.1). This zone also displays the most widely fluctuating inphase values. This combination of observations is likely indicative of buried metallic objects. There are also isolated anomalies further east (see Figure 2.7-3) along Line $50 \ (x = 50 \ \text{and} \ y = 20)$ and along line $80 \ (x = 80 \ \text{and} \ y = 15)$. These shallower anomalies could be due to localized areas of buried metallic debris. Anomalies that are associated with surface metals include those in Figure 2.7-3 at coordinate (30,0) and (120,30).

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Variations in conductivity due solely to trench excavation and emplacement of fill are not readily apparent on the EM plots. The conductivity variations and associated anomalies indicative of metallic objects appear to supersede any variations due to excavation.

Sample copies of a portion of the GPR raw data are shown in Figures 2.7-5 through 2.7-12. Figures 2.7-5 and 2.7-6 are selected GPR record sections in which evidence of a buried trench is not apparent. Reflections are relatively continuous, except for areas where surface cobbles were encountered beneath the GPR antenna. Figures 2.7-7 through 2.7-12 depict GPR transects in which the edges of a potential buried trench were interpreted. An interpretation for the trench was made from the GPR data for one or more of several observed anomalies. These were:

- A disruption in the continuity of near-surface layering, with the disruption usually offsetting the layering downward near the suspected location of the trench (e.g., Figures 2.7-7, 2.7-9, 2.7-10, 2.7-11, and 2.7-12)
- An increase in GPR reflection energy relative to surrounding areas (e.g., Figures 2.7-8 and 2.7-9)
- An absorption of GPR energy relative to surrounding areas (e.g., Figures 2.7-11 and 2.7-12)

The edges of both the north side and the south side of the trench were estimated from interpretation of each GPR transect. Those interpreted locations were then marked in the field for later surveying. The surveyed position of the interpreted trench edges along each transect were connected together to allow inclusion on the EM contour maps.

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2.8 THREE-DIMENSIONAL SITE VISUALIZATION

A series of three-dimensional geologic and contaminant concentration models (Figures 2.8-1 through 2.8-3) were constructed for the area around IHSS 110 (Trench T-3). The purpose of the models was to integrate existing geologic data and provide an evaluation tool for assessing contamination in and around IHSS 110. The models present a three-dimensional visualization of the geology and the contaminant distributions for total VOCs beneath the area. The geologic model consists of four layers representing the Rocky Flats Alluvium, the No. 1 Sandstone Unit, and claystone overlying and underlying the No. 1 Sandstone Unit. The total VOC contamination is presented in several views that are color coded to represent total VOC concentration ranges.

Software Selection

The software products used in the construction of the IHSS 110 area geologic and contaminant distribution models was geologic visualization software, Earth Vision (produced by Dynamic Graphics, Inc.). The visualization software provides two and three-dimensional modeling capabilities for geologic media. Two-dimensional grids from XYZ data were constructed and then used to produce solid graphical bodies. These solid bodies were then merged into the geologic model.

Earth Vision uses a minimum tension gridding technique to construct grids from scattered data sets. Gridding is necessary to estimate values of a property surface (usually elevation or concentrations) at regularly spaced locations (Davis 1986). Minimum tension gridding uses a spline function to connect the irregularly spaced data with a smooth continuous surface (Davis 1986). The values at the regular space points comprising the grid are taken from this splined surface. The particular function used in Earth Vision is known as Brigg's Bicubic spline function.

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Model Construction

The geologic model was constructed using grids of the surfaces of each of the following four geologic units: the Rocky Flats Alluvium, No. 1 Sandstone Unit, and claystones overlying and underlying the No. 1 Sandstone Unit. Topography forms the top surface of the model, with the bottom of the model formed arbitrarily at 5,700 feet in elevation for the area modeled and 5,850 feet for the IHSS 110-specific model. In addition, a surface was included in the model to represent the groundwater level in the No. 1 Sandstone Unit during March 1992. This period was chosen because it represents a relatively high groundwater level.

The major source of data to delineate the top and bottom surfaces of these geologic units was contained in the Preliminary Draft Phase II RFI/RI Report for OU-2 (DOE 1993b). These data consisted of digitized contour maps constructed by Woodward-Clyde Federal Services (WCFS) for the RFI/RI report. The following figures were delivered to EG&G in July 1994 during preparation of this report:

- Top of Bedrock Map
- Top of No. 1 Sandstone Unit Map
- Base of No. 1 Sandstone Unit Map
- First Quarter of 1992 Alluvial/Colluvial Potentiometric Map
- First Quarter of 1992 No. 1 Sandstone Unit Potentiometric Map
- Second Quarter of 1992 Alluvial/Colluvial Potentiometric Map
- Second Quarter of 1992 No. 1 Sandstone Unit Potentiometric Map

XYZ coordinate files corresponding to the location of contours on maps for the top of each of the respective units were then used to construct surface grids for each of these units.

When the grids were calculated by the software, they were extrapolated over the entire study area. The grids were then edited to represent the actual extent of the geologic units.

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Furthermore, the spatial limits of the sandstone were used to constrain the extent of this geologic unit in the model. All gridded values outside the spatial limits of the No. 1 Sandstone Unit were set to a null value. Grid cells with this value were considered to be blank, accounting for the absence of the geologic units in these areas.

Analytical results for VOCs (CCl₄, CHCl₃, PCE, TCE, Total VOCs) for subsurface soil collected from locations in the Northeast Trenches Area of OU-2 were provided for the three-dimensional visualization model.

Only total VOCs, however, were used to produce the visualizations presented in Figures 2.8-1 through 2.8-3.

Spreadsheets were prepared and included the northing, easting, elevation of the midpoint of the sampling interval, analyte, results in µg/kg, and the sample location. Using the results, a three-dimensional grid of total VOC concentrations was constructed, representing concentrations of various VOCs present in the soil in the area around IHSS 110. These data were obtained from analytical results for soil borings conducted for the OU-2 RFI/RI and SVE studies. In order to limit interpolation error due to the large spread of data values over several orders of magnitude, the initial data files were converted to logarithmic values. Limiting the spread of data values reduced error in the model resulting from the interpolation of a value from adjacent values that exhibited large numerical differences. Three-dimensional grids were then constructed from these three-dimensional data files. The resulting logarithmic three-dimensional grids were then converted back to the actual values.

Solid geologic bodies were constructed from these contaminant concentration threedimensional grids, using the surfaces constructed previously. The Rocky Flats Alluvium was constructed from the topography grid and the base of bedrock grid; the overlying claystone was constructed from the base of bedrock grid and the top of No. 1 Sandstone Unit grid, and the underlying claystone was constructed from the base of the No. 1 Sandstone Unit grid and

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the model base grid (set arbitrarily at 5,700 or 5,850 feet). These bodies represent three-dimensional visualizations of the geologic units in the model. The base of the model is well below the zone of interest (with respect to contaminant distribution) and does not interfere with the visualization. These bodies were then merged to produce complete geologic/contaminant distribution models of the area around IHSS 110 which display not only the geology, but also contamination concentrations of the selected VOCs in soil.

Model Results

The resulting diagrams illustrate the geology and contaminant distribution beneath the area around IHSS 110. Visualizations for total VOC concentrations are shown on Figures 2.8-1 through 2.8-3. These figures present various views of the contaminant distributions (for total VOC concentrations) and the geology. It is apparent from the model results that elevated total VOC concentrations are present in the west end of Trench T-3. The models also indicate that the elevated concentrations most likely do not extend below the potentiometric surface or are limited to just below the high water table. Downward migration of the contaminants is apparently restricted by the bedrock claystones underlying the alluvium beneath Trench T-3.

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3.0 OVERVIEW OF POTENTIAL CONTAMINANT MIGRATION PATHWAYS

Contaminant fate and transport through groundwater, surface water, and air pathways at OU-2 have been evaluated in the Preliminary Draft Phase II RFI/RI Report for OU-2 (DOE 1993b) to assess the potential for on-site and off-site migration of selected contaminants. The transport of contaminants in various environmental media including surface soils, groundwater, surface water, air, and biota was also evaluated for the 903 Pad, Mound, and East Trenches Areas of OU-2 in the Preliminary Draft Phase II RFI/RI Report for OU-2.

This section will limit the discussion of fate and transport to an overview of the potential migration pathways of contaminants found at IHSS 110 (Trench T-3). The Preliminary Draft Phase II RFI/RI Report for OU-2 presents a thorough discussion of fate and transport of selected chemicals throughout OU-2. A summary of contaminants found at Trench T-3 is provided on Figure 3.0-1. Contaminant migration pathways for Trench T-3 are shown schematically on Figure 3.0-2.

The primary pathway for contamination originating in the trench occurs through vertical migration through the vadose zone beneath the trench to groundwater and then laterally within the saturated alluvium, when present, and within the No. 1 Sandstone Unit.

VOCs (CCl₄, CHCl₃, 1,1-DCE, PCE, and TCE) have the potential to be released to the subsurface from Trench T-3 as dissolved constituents or as NAPLs. Pooled NAPL was encountered in borehole 10191 in Trench T-3 during the OU-2 Phase II alluvial field investigation. NAPL-saturated soil was also encountered in borehole 24793 (near Trench T-3) during the ongoing SVE Pilot Test Program. Most recently, NAPL was observed during installation of subsurface pressure monitoring probes inside the trench in August of 1994. Dissolved VOCs and possibly NAPLs have the potential to migrate vertically through the vadose to contaminate groundwater. Subsequently, leaching of residual contamination

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(adsorbed and possibly NAPL) from the vadose zone could continue to contaminate groundwater.

High concentrations of VOCs have been detected in groundwater in well 3687, which is screened in the No. 1 Sandstone Unit, located hydraulically downgradient (north) of Trench T-4. VOCs appear to have migrated in groundwater from source areas by advection and dispersion processes to form contaminant plumes within the No. 1 Sandstone Unit, and to a lesser extent, within the alluvium. Groundwater contaminant plumes in the sandstone migrate toward the north-northeast, and appear to discharge at seeps on the hillside of the South Walnut Creek drainage. Contaminated groundwater in the alluvium flows along the medial paleoscour, northeastward toward the surface drainage gully. To date, discharge of contaminants at the surface drainage gully appears to be minimal, based on groundwater concentrations that are at or below the method detection limits.

Volatilization to form soil gas potentially occurs beneath Trench T-3, due to the presence of residual contamination in vadose zone soils. Volatilization from groundwater to form soil gas may also occur in association with groundwater contaminant plumes in the No. 1 Sandstone Unit and Rocky Flats Alluvium. The resulting soil gas may reach the atmosphere, depending on the depth of the residual contamination or water table.

Volatilization may also occur from seeps and surface water directly to the atmosphere. A portion of the contaminants not volatilized at seeps migrate downslope with water in the colluvium and potentially discharge to South Walnut Creek. Once in the creek, a portion of the VOCs are volatilized to the atmosphere or transported by streamflow advection/dispersion/sediment transport processes.

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Elevated activities of radionuclides (Am-241, Pu-239/240) have been observed in source boreholes drilled in Trench T-3. Activity levels decrease rapidly below the trenches, indicating that these species are relatively immobile in the vadose zone in this area. These contaminants have not been observed at high activities in groundwater in these areas, and are not expected to be discharged with the groundwater at seeps.

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4.0 SUMMARY

The thickness of the RFA in the vicinity of Trench T-3 is approximately 15 feet. The RFA consists of primarily sandy and clayey gravels with some clay layers. In general, caliche layers have been identified on the north side of Trench T-3. The caliche layers may retard infiltration of precipitation to the vadose zone around Trench T-3. Where the caliche layers have been disturbed due to excavation of Trench T-3, infiltration of precipitation may be enhanced relative to surrounding areas. The thickness of the No. 1 Sandstone Unit beneath Trench T-3 ranges from 20 to 35 feet. The No. 1 Sandstone Unit is separated from the bottom of the trench by approximately 10 feet of claystone on the western end of Trench T-3 and is in direct contact on the eastern end. The approximate depth to the high groundwater was 15 feet BGS (May 1992). The primary flow direction of the groundwater in the No. 1 Sandstone Unit is to north-northeast. The majority of groundwater is believed to flow in the highly friable, coarse-grained sandstone unit of the No. 1 Sandstone Unit.

The evaluation of the geological and geophysical data indicated that Trench T-3 is approximately 5 to 10 feet in depth, ranges from 19 to 23 feet wide, and 135 to 140 feet long. Borehole 25394, which is located on the eastern end of Trench T-3, encountered a caliche layer at an approximate depth of 6 feet BGS. The caliche layer indicates that the base of the trench in the vicinity of borehole 25394 is less than 6 feet.

The Historical Release Report (DOE 1992a) indicated that sanitary sewage sludge contaminated with uranium and plutonium and flattened drums with uranium were reportedly buried in this trench. During drilling of boreholes in and around Trench T-3 void spaces, flattened drums, NAPL, and residual NAPL have been encountered. Void spaces were encountered in boreholes 25194, 25294, and 25494 at depths generally above 6 feet. The void space in borehole 25194 was encountered at an approximate depth from 4 to 5.3 feet and was filled with a stratified liquid. The stratified liquid was observed to have three distinct layers (a black floating layer on top, a yellowish brown layer in the middle, and a black

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sinking layer on the bottom) from a sample collected before grouting the borehole. Flattened drums were observed in boreholes 25294, 25494, 25594, and 25694 at approximate depths from 3 to 7 feet BGS. NAPL was encountered in boreholes 10191 and 25194 at approximate depth from 2 to 5 feet BGS. Residual NAPL was observed in boreholes 24793, 25594, and 25694 at approximate depths from 7 to 14 feet BGS. In general, void spaces and flattened drums are located in the western and central portions, NAPL is located in the western portion, and residual NAPL is located in the central portion of Trench T-3.

The primary contaminants groups detected in samples collected from Trench T-3 include CHCs, BTEX constituents, TPHs described as gasoline and diesel, PAHs, phenols, phthalates, actinides (Am-241, Pu-239/240, U-233,-234, U-235, and U-238). Subsurface soil samples collected from Trench T-3 indicated the presence of CHCs (primarily CCl₄, CHCl₃, PCE, and TCE) at concentrations ranging from parts per million to parts per thousands. In general, the elevated concentrations of CHCs were observed in samples collected from the residual or NAPL saturated soils. PAHs and phthalates were detected in the subsurface soil samples collected from Trench T-3 at concentrations up to parts per million. Actinides (Am-241, Pu-239/240, U-233,-234, U-235, and U-238) were detected at activities at approximately 1 pCi/g in the subsurface soil samples. Soil gas surveys indicate that the CHCs (CCl₄, PCE, and TCE) were the most frequently detected and the total VOCs concentration ranged from 50 to 600 μg/L.

Analysis of the liquid samples collected from location 25194 indicated the presence of CHCs, BTEX constituents, TPHs described as gasoline and diesel, PAHs, phthalates, phenols, and the U-isotopes. CHCs detected in the liquid sample were 1,1-DCA, CHCl₃, 1,1,1-TCA, TCE, and PCE. The four BTEX constituents detected were toluene, ethylbenzene, m,p-xylene, and o-xylene. PAHs detected were naphthalene, 2-methylnapthalene, phenanthrene, anthracene, pyrene, chrysens, and fluorene. Phthalates detected were di-n-butylphthalate and bis[2-ethylhexyl]phthalate. Phenols detected were phenol, 2-methylphenol, and 4-methylphenol. TPHs described as having carbons in the gasoline and diesel ranges were also detected. Am-

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241 and Pu-239/240 were detected at activities up to 1 pCi/g and U-233,-234, U-235, and U-238 were detected at activities up to 398 pCi/g, 101 pCi/g, and 3240 pCi/g, respectively,

Review of the groundwater isoconcentration maps (Figures 2.6-8 through 2.6-17) indicated that Trench T-3 is a likely source of contamination to groundwater within the No. 1 Sandstone. The upgradient wells (i.e., 2587 and 01991) from Trench T-3 in the No. 1 Sandstone had total VOCs concentration of 259 ug/l and 273 ug/l, respectively, as measured in fourth quarter of 1993. While the downgradient wells in the No. 1 Sandstone (i.e., 24193, 03391, and 03691) from Trench T-3 had total VOCs concentration of 5,174 ug/l, 1,041 ug/l, and 1,021 ug/l, respectively, as measured in fourth quarter of 1993.

Potential contaminant migration paths from Trench T-3 are summarized in the following:

- Leakage into subsoil from buried waste materials and possibly by direct discharge of waste into the trench.
- NAPL and aqueous liquids in the western portion of Trench T-3 are believed to be perched. Possible reasons for this could be the presence of an impermeable layer within the trench or beneath the trench. The claystone bedrock beneath the western portion and above the No. 1 Sandstone could retard vertical migration of the NAPL and aqueous liquids in this area of the trench.
- Residual NAPL observed in the boreholes in the central portion of the trench
 and presence of void spaces combined with the subcropping No. 1 Sandstone
 provides a contaminant pathway to groundwater.
- Contaminants entering the groundwater in the No. 1 Sandstone are then controlled by the groundwater flow direction (north and northeast).

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Contaminated groundwater in the No. 1 Sandstone is believed to extend to the north facing slope of the South Walnut Creek Drainage and then seeps directly into Ponds B-1 and B-2 or into the colluvium above the ponds then flow downhill to the ponds.

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TABLE 2.2-1

TRENCH T-3 (IHSS110)

DRILLING AND SOIL SAMPLE COLLECTION AND ANALYSIS SUMMARY

November 1994

		St. id	F. 1	Total	Т	RFEDS	Waste	Sample	Sample		
	Location	Start	End	Depth	Top of	Sample	Sample	Start Depth	End Depth		
Number	Type	Date	Date	(ft)(BGS)	Bedrock	Number	Number	(ft)BGS)	(ft)(BGS)	Analysis Requested	Comment
25194	BH/EW	11/2/94	11/10/94	5.3	NE	BH20665WC	95N0058	3.6	5.3	VBR, BDR, WW, RH	Liquid Sample
						DR00010WC		0	4	RH, V, B, M, RA, RB, RC	Drum Composite
						DR00016WC		0	4	RH, V, B, M, RA, RB, RC	Drum Composite
25294	BH	11/2/94	11/4/94	8	NE	BH20654WC		6.75	7	RH, VBR	Discrete VOA
						BH20655WC		6	8	RH, BDR	Compositee
	,					_DR00011WC		0	. 8	RH, V, B, M, RA, RB, RC	Drum Composite
25394	BH	11/4/94	11/4/94	9	NE	BH20651WC		4	6	RH, WH, VBR	Compositee
						BH20650WC		5.75	6	RH, VBR	Discrete VOA
						BH20653WC		6	8	RH, GQB	Composite
						DR00012WC		0	8	RH. V. B. M. RA. RB. RC	Drum Composite
25494	BH	11/7/94	11/7/94	3.5	NE	DR00013WC		. 0	3.5	RH, V, B, M, RA, RB, RC	Drum Composite
25594	BH	11/7/94	11/8/94	16	15.5	BH20658WC		15.75	16 .	RH, VBR	Discrete VOA
						BH20659WC		9	10	RH, BDR, WW	Composite
						BH20660WC		9.8	10	RH, VBR	Discrete VOA
						DR00014WC		0	16	RH. V. B. M. RA. RB. RC	Drum Composite
25694	BH	11/8/94	11/9/94	14	NE	BH20652WC		10		RH, GQB	Composite
						BH20656WC		11.8	12	RH, VBR	Discrete VOA
						BH20657WC		4	- 6	RH, GQB	Composite
						DR00015WC		0	14	RH. V. B. M. RA. RB. RC	Drum Composite

Explanations:

BH - Borehole

V - VOA-CLP

EW - Extraction well

VBR - VOA (8240)

NE -Not encountered

B - BNA-CLP

BGS - Below ground surface

BDR - BNA (8270)

RH - Radionuclide screen

M - Total Metals-CLP

RA - Gross alpha and beta

GQB - Soil moisture content

RB - Plutonium-239/240, Americium-241

WH - Total organic carbon

RC - Uranium-233,234, Uranium-235, Uranium-238

WW - Total petroleum hydrocarbons (8015 modified)

TABLE 2.2-2
SUMMARY OF REQUESTED ANALYSIS

EG&G Sample Number	Laboratory Sample Number	- 		VOA Method (8260)	SVOA Method (8270)	Modified Method (8015)	Select Radionuclide	Special Sample Prep
C0639	C0639-02	12-20-94	Floating Layer (1)	X				
C0639	C0639-03	12-20-94	Floating Layer (1)		х			
C0639	C0639-04	12-20-94	Floating Layer (1)			X		
C0639	C0639-05	12-20-94	Floating Layer (1)			ν		х
C0640	C0640-04	12-20-94	Top Floating Layer (2)	Х	·			
C0640	C0640-05	12-20-94	Top Floating Layer (2)		- X			
C0640	C0640-06	12-20-94	Top Floating Layer (2)			X		
C0640	C0640-07	12-20-94	Top Floating Layer (2)					Х
C0640	C0640-08	12-20-94	Top Floating Layer (2)				Х	
C0640	C0670-04	12-20-94	Bottom Water	X				
C0640	C0670-05	12-20-94	Bottom Water		х			
C0640	C0670-06	12-20-94	Bottom Water			х		
C0640	C0670-07	12-20-94	Bottom Water					Х
C0640	C0670-08	12-20-94	Bottom Water				Х	

TABLE 2.2-3

SUMMARY OF DISTILLATION ANALYSIS CONDUCTED ON LIQUID SAMPLE C0640 COLLECTED IN DECEMBER 1994

Sample Fraction After Distillation	Miscible with water?	Miscible with methylene chloride?	Distillation Temperature Range (°C)	Distillate Sample Number	Volume (mL)	Density (g/mL)	Analyses Requested
А-Тор	Yes	No	97-98	C0641-01	13	0.967	Volatiles Semivolatiles TPH
A-Bottom	No-heavier	Yes	97-98	C0642-01	27	1.539	Volatiles Sémivolatile TPH
В-Тор	Yes	No	98-100	C0643-01	200	0.966	Volatiles Semivolatiles TPH
B-Bottom	No-heavier	Yes	98-100	CO644.01	100	1.475	Volatiles Semivolatiles TPH
С-Тор	Yes	No	100-105	C0645-01	156	0.960	Volatiles Semivolatiles TPH

TABLE 2.2-3
SUMMARY OF DISTILLATION ANALYSIS
(continued)

Sample Fraction After Distillation	Miscible with water?	Miscible with methylene chloride?	Distillation Temperature Range (°C)	Distillate Sample Number	Volume (mL)	Density (g/mL)	Analyses Requested
C-Bottom	No-heavier	Yes	100-105	C0645-01	39	1.270	Volatiles Semivolatiles TPH
D-Top	No-lighter	Yes	100-106	C0647-01	48	0.835	Volatiles Semivolatiles TPH
D-Bottom	Yes	No	100-106	C0648-01	437	1.004	Volatiles Semivolatiles TPH
Е-Тор	No-lighter	Yes	106-109	C0704-01	4	0.888	Volatiles Semivolatiles TPH
E-Bottom	Yes	No	106-109	C0649-01	100		Volatiles Semivolatiles TPH
F-Тор	No-lighter	Yes	109-120	C0705-01	2	0.865	Volatiles Semivolatiles TPH

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TABLE 2.2-3
SUMMARY OF DISTILLATION ANALYSIS
(continued)

Sample Fraction After Distillation	Miscible with water?	Miscible with methylene chloride?	Distillation Temperature Range (°C)	Distillate Sample Number	Volume (mL)	Density (g/mL)	Analyses Requested
F-Bottom	Yes	No	109-120	C0698-01	50	0.965	Volatiles Semivolatiles TPH
G	Yes -	No	120-140	C0699-01	9		Volatiles Semivolatiles TPH
Н	Yes	No	140-160	C0700-01	3.5		Volatiles Semivolatiles TPH
I	Yes	No	160-180	C0701-01	2		Volatiles Semivolatiles TPH
J	No-lighter	Yes	180-205	C0702-01	0.5	1.020	Volatiles Semivolatiles TPH
К	No-lighter	Yes	N/A (Residue)	C0703-01	785	0.875	Volatiles Semivolatiles TPH

TABLE 2.2-4
UHSU GROUNDWATER SAMPLES COLLECTED FROM SVE ARAPAHOE NO. 1 SANDSTONE WELLS PRIOR TO WARP
(September 1994)

			Depth to Top of Groundwater	
Well Number	Sample Number	Collection	(ft BTC)	Sample Collection Interval
24193	GW01389GA	9/6/94	26.6	Bottom of casing sample
24193	GW01431GA	9/6/94	26.6	Top of groundwater sample
24393	GW01390GA	9/6/94	26.79	Top of groundwater sample
24993	GW01391GA	9/7/94	26.79	Bottom of casing sample
24993	GW01392GA	9/6/94	26.91	Top of groundwater sample
24993	GW01393GA	9/7/94	26.91	Bottom of casing sample
25093	GW01394GA	9/6/74	26.75	Top of groundwater sample
25093	GW01395GA	9/7/94	26.75	Bottom of casing sample

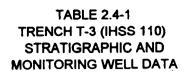
Explanation:

BTC = Below top of casing

UHSU = upper hydrostratigraphic unit

SVE = soil vapor extraction

WARP = Well Abandonment and Replacement Program



			Ground	· ·		Borehole	Elevation	Depth to	Elevation	Depth to	Elevation	Depth to	Elevation	Top of		Screen	Interval	
			Surface	1	Stratigraphy	Total	of Total	Top of	Top of	Top of	Top of	Base of	Base of	Well Casing	Depth	Depth	Elevation	Elevation
Location	Northina	Easting	Elevation	Location	of Screened	Depth	Depth	Bedrock	Bedrock	Ka (No.1)	Ka (No.1)	Ka (No.1)	Ka (No.1)	Elevation	to Top	to Base	of Top	of Base
Number	(ft)	(ft)	(ft)	Туре	Interval	(R BGS)	(ft BGS)	(ft BGS)	(ft)	(ft BGS)	(ft) i	(ft BGS)	(ft)	(ft)	(ft BGS)	(ft BGS)	(ft)	(ft)
2487	749751	2086746	5958.0	MW	Qrf	18.5	5939.5	15.1	5942.9	NE	NE	NE	NE	5959.6	3.5	13.6	5954.8	5944.7
2587	749719	2086748	5960.0	MW	Ka (No.1)	47.0	5913.0	16.5	5943.5	17.5	5942.5	44.7	5915.3	5961.0	17.5	43.5	5942.0	5916.0
BH3987	749760	2089605	5957.0	BH	NA	22.0	5935.0	14.5	5942.5	NE	NE	NE	NE	NA	NA	NA	NA	NA
BH4087	749850	2087026	5954.0	ВН	. NA	14.5	5939.5	8.0	5946.0	NE	NE	NE	NE	NA	NA	NA	NA	NA
02991	749777	2086970	5956.0	MW	Ka (No.1)	57.9	5898.1	15.8	5940.2	15.8	5940.2	50.1	5905.9	5957.9	42.0	52.0	5914.3	5904.3
10191	749789	2086868	5958.0	ВН	NA	54.0	5904.0	14.5	5943.5	24.6	5933.4	48.0	5910.0	NA	NA	NA	NA	NA
12191	749774	2086949	5957.0	MW	Ka (No.1)	36.9	5920.1	15.7	5941.3	15.7	5941.3	NE	NE	5958.2	18.0	33.0	5938.5	5923.5
21693	749826	2086867	5955.0	ВН	NA NA	163.0	5792.0	15.6	5939.4	19.4	5935.6	48.1	5906.9	NA	NA	NA	NA	NA
22493	749825	2086857	5955.0	ВН	NA NA	52.3	5902.7	15.6	5939.4	19.8	5935.2	44.1	5910.9	NA	NA	NA	NA	NA
23293	749823	2086846	5956.0	MW	KI (sist,cs)	89.5	5866.5	15.5	5940.5	24.0	5932.0	44.5	5911.5	5958.0	77.9	88.0	5877.8	5867.6
24093	749808	2086899	5956.0	AV1	Qrf	18.3	5937.7	13.4	5942.6	NE	NE	NE	NE	5957.9	5.4	15.4	5950.6	5940.6
24193	749808	2086905	5956.0	SV1	Ka (No.1)	75.0	5881.0	13.0	5943.0	13.0	5943.0	NA	NA	5959.0	22.0	72.0	5934.0	5884.0
24293	749786	2086903	5957.0	Al1	Qrf	17.6	5939.4	15.1	5941.9	15.1	5941.9	NE	NE	5957.3	5.0	15.0	5952.0	5942.0
24393	749789	2086907	5957.0	SI1	Ka (No.1)	74.5	5882.5	15.1	5941.9	15.1	5941.9	NA	NA	5959.1	22.0 ·	72.0	5935.0	5885.0
24493	749807	2086895	5956.0	APM1	Qrf	15.2	5940.8	13.0	5943.0	NE	NE	NE	NE	5958.0	8.1	11.1	5947.9	5944.9
24593	749781	2086904	5956.0	APM2	Qrf	14.2	5941.8	13.4	5942.6	NE	NE	NE	NE	5957.7	8.3	11.3	5947.7	5944.7
24693	749787	2086918	5956.0	APM3	Qrf	16.4	5939.6	13.7	5942.3	13.7	5942.3	NE	NE	5957.0	9.0	12.0	5947.0	5944.0
24793	749803	2086910	5956.0	BH	NA NA	10.0	5946.0	NE	NE	NE	NE	NE	NE	NA	NA	NA_	NA	NA
24893	749784	2086908	5957.0	ВН	NA	17.1	5939.9	13.5	5943.5	13.5	5943.5	NE	NE	NA NA	NA	NA	NA .	NA NA
24993	749809	2086910	5956.0	SPM1	Ka (No.1)	76.0	5880.0	14.2	5941.8	16.7	5939.3	49.3	5906.7	5958.0	23.0	68.0	5933.0	5888.0
25093	749787	2086912	5957.0	SPM2	Ka (No.1)	71.0	5885.0	15.1	5941.9	NA	NA	NA	NA	5957.9	23.0	68.0	5934.0	5889.0
25194	749789	2086874	5958.1	EW	Qrf	5.3	5952.8	NE	NE	NE	NE	NE	NE	NA	2.5	4.5	5955.6	5953.6
25294	749797	2086911	5957.5	ВН	NA	9.0	5948.5	NE	NE	NE	NE	NE	NE	NA	NA	NA	NA	NA
25394	749805	2086950	5956.7	BH	NA	16.0	5940.7	15.5	5941.2	15.5	5941.2	NE	NE	NA	NA	NA	NA	NA
25494	749803	2086914	5956.9	ВН	NA	8.0	5948.9	NE	NE	NE	NE	NE	NE	NA	NA	NA	NA	NA NA
25594	749792	2086917	5957.2	ВН	NA NA	14.0	5943.2	NE	NE	NE	NE.	NE	NE	NA	NA_	NA	NA	NA
25694	749803	2086929	5956.7	ВН	NA	4.0	5952.7	NE	NE	NE	NE	NE	NE	NA	NA	NA	NA	NA

EXPLANATION:

Al1	Altuvial injection well	KI (sist,cs)	Laramie Formation siltsone and claystone
APM1	Alluvial pressure monitor	MW	Monitoring well
APM2	Altuvial pressure monitor	NA	Not available
APM3	Altuvial pressure monitor	NE	Not encountered
AV1	Alluvial extraction well	Qrf	Rocky Flats Alluvium
BGS	Depth below ground surface	SI1	Sandstone injection well
ВН	Borehole	SPM1	Sandstone pressure monitor
EW	Extraction well	SPM2	Sandstone pressure monitor
Ka (No.1) Arapahoe Formation No.1 Sandstone	SV1	Sandstone extraction well

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TABLE 2.4-2
SUMMARY OF SAMPLES COMBINED FOR LABORATORY GEOTECHNICAL ANALYSIS
RFETS, TRENCH T-3 (IHSS110)
MARCH, 1995

					- Lit	hology -
Sample	Borehole	Composite	Sample Depth	Sample Depth	USCS	Wentworth
Number	Number	Sample	From	to	Code (2)	Scale (3)
		Number	Ft. (BGS)	Ft. (BGS)		
BH00001EG	10191	BH00014EG	17.6	18.1	N/A	Silty Claystone
BH00002EG	10191	BH00014EG	18.7	19.3	N/A	Silty Claystone
BH00003EG	12191	(1)	15.0	15.5	GW	N/A
BH00004EG	24193	BH00015EG	2.9	3.5	Caliche	N/A
BH00005EG	24193	BH00016EG	13.3	13.6	N/A	Sandstone
BH00006EG	24193	(1)	13.0	13.4	N/A	Siltstone
BH00007EG	24593	BH00015EG	1.2	1.5	Caliche	N/A
BH00008EG	24593	BH00017EG	11.6	12.4	GM	N/A
BH00009EG	24693	BH00017EG	10.5	11.6	CL/GM	N/A
BH00010EG	24893	(1)	4.0	4.5	CL	N/A
BH00011EG	24893	BH00016EG	14.7	15.2	N/A	Sandstone
BH00012EG	24993	BH00018EG	10.2	10.8	SC	N/A
BH00013EG	24993	BH00018EG	12.7	13.6	SM	N/A

- (1) This sample was not combined with any other samples and retained the same sample number for geotechnical analysis.
- (2) Uniform Soil Classification System
- (3) A logarithmic grade scale for size classification of sediment particles. Applies to detrital sediments.

TABLE 2.4-3 SUMMARY OF GEOTECHNICAL ANALYTICAL TESTS CONDUCTED RFETS, TRENCH T-3 (IHSS110) MARCH, 1995

			GEOTECHNICAL TESTS PERFORMED								
Sample Number	Borehole Number	Depth BGS (Ft.)	Permeability Back pressure, Constant Head	Permeability Back pressure Saturated, Flow Pump Method	Capillary Moisture Retention Tests	Mechanical Analysis - Sieve - Tests	Specific Gravity Tests				
BH00003EG	12191	15.0 - 15.5	X			x	x				
BH00006EG	24493	13.0 - 13.4		X		X	X				
BH00010EG	24893	4.0 - 4.5		X		X	X				
BH00014EG	10191	Composite (2)		X	X	X	X				
BH00015EG	Composite (1)	Composite (2)		X	X	X	X				
BH00016EG	Composite (1)	Composite (2)		X .	X `	X	X				
BH00017EG	Composite (1)	Composite (2)	X		X	X	X				
BH00018EG	Composite (1)	Composite (2)		X	X	X	X				

- (1) Multiple boring location samples of the same lithology combined.
- (2) Multiple depth samples of the same lithology combined.



TABLE 2.4-4

SUMMARY OF GEOTECHNICAL TESTING RFETS, TRENCH T-3 (IHSS110) MARCH 1995

Sample Number	Boring Numb e r	Depth BGS (2) (Ft.)	Specific Gravity (Unitless)	Effective Porosity, n (3) (%)	Dry Density (4) (pcf)	Moisture Content (4) (%)	Initial Void Ratio, e (5) (Unitless)	Initial Saturation (%)	Coefficient of Permeability, k (6) (cm/sec)	Confining Pressure (psi)	Maximum Hydraulic Gradient (Unitless)	Final Moisture Content (%)	Final Dry Density (pcf) (7)	Final Void Ratio, e (Unitless)	Final Saturation (%)
BH00003EG(1)	12191	15.0 - 15.5	2.66	26.18	110.0	8.0	0.46	26.0	6.60E-04	5.000	18.510	13.9	117.6	0.43	89.7
BH00006EG(1)	24493	13.0 - 13.4	2.71	39.08	120.0	11.5	0.44	84.0	1.40E-08	3.865	21.029	22.7	107.3	0.60	8.601
BH00010EG (1)	24893	4.0 - 4.5	2.65	27.39	122.0	13.0	0.35	91.6	9.40E-08	4.795	3.805	13.6	125.4	0.34	113.0
BH00014EG	10191	Composite	2.63	32.84	118.0	13.0	0.38	84.5	2.10E-06	4.991	0.166	17.3	118.3	0.40	117.2
BH00015EG	Composite	Composite	2.53	37.55	107.0	16.0	0.48	82.3	1.70E-07	4.894	2.005	21.9	106.9	0.49	115.9
BH00016EG	Composite	Composite	2.68	29.88	121.0	15.0	0.40	93.9	4.70E-08	4.593	7.397	15.8	117.7	0.44	100.6
BH00017EG	Composite	Composite	2.67	35.65	122.0	10.0	0.31	79.8	2.30E-07	5.000	18.380	17.3	128.7	0.31	156.0
BH00018EG	Composite	Composite	2.62	34.04	118.0	13.0	0.37	84.4	9.40E-08	4.809	3.556	18.6	114.2	0.45	112.7

- (1) Composite samples BH00003EG, BH00006EG & BH00010EG were analyzed for soil porosity, hydraulic concuctivity and sieve analysis.
- (2) Below Ground Surface
- (3) Ratio of the volume of voids to the total volume of the mass.
- (4) Target densities & moisture contents were derived from field data obtained during previous investigations. Remolding was based on these target values.
- (5) e: Ratio of the volume of voids to the volume of solid particles.
- (6) k: Coefficient of permeability where permeability is that property of a solid allowing it to transmit water.
- (7) pcf is "Pounds per cubic feet".
- (8) Target densities and moisture contents where derived from field data obtained during previous investigations.

TABLE 2.4-5 SUMMARY OF MECHANICAL TESTING - SIEVE TEST DATA RFETS, TRENCH T-3 (IHSS110) MARCH, 1995

Sample Number	Boring Number	Depth BGS (Ft.)	Lithology	Gravel (1) (%)	Sand (2) (%)	Silt (3) (%)	Clay (4),(5)
BH00003EG	12191	15.0 - 15.5	GW	17	46	25	13
BH00006EG	24493	13.0 - 13.4	Siltstone	0	8	45	47
BH00010EG	24893	4.0 - 4.5	CL	0	45	32	23
BH00014EG	10191	Composite	Silty Claystone	. 0	38	44	18
BH00015EG	Composite	Composite	Caliche	28	32	24	16
BH00016EG	Composite	Composite	Sandstone	0	40	42	18
BH00017EG	Composite	Composite	CL/GM	24	46	16	14
BH00018EG	Composite	Composite	SC/SM	27	43	13	17

- (1) Partical sizes of sieve number 4 and larger are identified as gravel.
- (2) Partical sizes less than sieve number 4 and larger than sieve size number 200 are identified as sand.
- (3) Partical sizes less than sieve number 200 and larger than 0.002mm are identified as silt.
- (4) Partical sizes less than 0.002mm are identified as clay.
- (5) Atterbery limits were not run.

TABLE 2.5-1
OU2 GROUNDWATER ELEVATIONS
FOURTH QUARTER 1993

Well Number	Lithologic Unit	Measurement Date	Depth to Water (ft)	Ground Surface Elevation	Top of Casing Elevation	Groundwater Elevation
191	Qrf	7-Oct-93	21.3	5968.9	5970.44	5949.14
291	Ka (No.1)	7-Oct-93	29.95	5966.2	5967.57	5937.62
386	Kl(ss)	5-Oct-93	16.41	5676.2	5677.86	5661.45
391	KI(ss)	6-Oct-93	9,43	5920.8	5922.4	5912.97
491	Qc/Ka(cs)	6-Oct-93	19.38	5903.5	5904.97	5885.59
691	Qc	8-Oct-93	-1	5894.5	5896.13	dry
791	Qc	8-Oct-93	21.59	5907.1	5908.27	5886.68
891	Qc	8-Oct-93	21.77	5868.4	5869.95	5848.18
987	Ka(No.1)	5-Oct-93	20.38	5980,2	5981.7	5961.32
991	KI(cs)	8-Oct-93	-1	5867	5868.56	dry
1087	Qrf	5-Oct-93	13	5982	5983.52	5970.52
1187	KI(ss)	8-Oct-93	20.12	5913,6	5915.12	5895
1287	Ka(no.1)	5-Oct-93	-1	5934.8	5936.3	dry
1291	Qc	8-Oct-93	17.4	5851,2	5852.85	5835.45
1391	Qrf	5-Oct-93	13.49	5973.7	5975.3	5961.81
1487	Kl(ss,cs)	8-Oct-93	15.77	5855	5856.56	5840.79
1491	Ka (No.1)	5-Oct-93	16.24	5970.4	5972.03	5955.79
1587	Qrf	7-Oct-93	22.54	5971.3	5972.79	5950.25
1791	Ka (No.1)	1-Oct-93	14.89	5965.8	5967.41	5952.52
1891	Ka (No.1)	1-Oct-93	18.8	5971.8	5973.37	5954.57
. 1987	Qrf	1-Oct-93	13.75	5968.4	5969.91	5956.16
1991	Ka?(cs)	5-Oct-93	25.74	5962.2	5963.61	5937.87
2091	Qrf/Ka(No.1)	1-Oct-93	22.94	5965.2	5966.65	5943.71
2187	Qvf	4-Oct-93	8.44	5928.4	5929.69	5921.25
2191	Qrf	1-Oct-93	-1	5965.8	5967.51	dry
2291	Ka(No.1)	1-Oct-93	15.05	5936.7	5938.26	5923.21
2387	Ka(No.1)	1-Oct-93	18.76	5972.8	5974.49	5955.73
2391	Qп	5-Oct-93	-1	5956.8	5958.43	dry
2487	. Qrf	5-Oct-93	15.7	5958.3	5959.69	5943.99
2491	Ka(No.1)	1-Oct-93	17.68	5944.5	5946.21	5928.53
2587	Ka(No.1)	5-Oct-93	28.59	5959.5	5960.98	5932.39
2591	Ka (No. 1?)	5-Oct-93	40.81	5923.6	5925.34	5884.53
2687	Qrf	7-Oct-93	15.38	5954.3	5955.9	5940.52
2787	Qтſ	7-Oct-93	-1	5947.8	5949.65	dry
2791	Qrf	5-Oct-93	-1	5954.3	5955.79	dry

TABLE 2.5-1
OU2 GROUNDWATER ELEVATIONS
FOURTH QUARTER 1993

	TOWN QUARTER 1775										
Well Number	Lithologic Unit	Measurement Date	Depth to Water (ft)	Ground Surface Elevation	Top of Casing Elevation	Groundwater Elevation					
2891	Qrf	5-Oct-93	12.84	5953.1	5954.61	5941.77					
2987	Qc	8-Oct-93	17.6	5812.6	5814.29	5796.69					
2991	Ka (No.1)	6-Oct-93	27.91	5956.3	5957.9	5929.99					
3091	Ka (No.1)	5-Oct-93	37.15	5952.9	5954.23	5917.08					
3191	Qrf	6-Oct-93	25.24	5950.4	5952.02	5926.78					
3287	Qrf	7-Oct-93	47.97	5946.4	5947.97	5900					
3387	Qrf	7-Oct-93	-1	5945.8	5947.22	dry					
3391	Ka (No.1)	5-Oct-93	26.95	5944.5	5946.22	5919.27					
3586	Qvf	1-Oct-93	9.51	5910.8	5912.76	5903.25					
3587	Qrf	6-Oct-93	-1	5950	5951.39	dry					
3591	Qrf	6-Oct-93	33.8	5949	5950.8	5917					
3686	Qvf	5-Oct-93	-1	5883.7	5885.22	dry					
3687	Ka(No.1)	6-Oct-93	37.14	5949.7	5951.11	5913.97					
3691	Ka (No.1)	5-Oct-93	34.05	5932.6	5934.43	5900.38					
3786	Qvf	5-Oct-93	8.27	5796.6	5798.26	5789.99					
3791	Ka (No.1)	5-Oct-93	39.38	5936.8	5938.24	5898.86					
3891	Qrf	5-Oct-93	-1	5940.9	5942.95	dry					
3986	Qrf	5-Oct-93	28.88	5908.2	5909.41	5880.53					
3991	Qrf	6-Oct-93	35.79	5935.2	5936.87	5901.08					
4091	Qrf	6-Oct-93	37.44	5928.5	5930.14	5892.7					
4186	Qrf	7-Oct-93	46.65	5942.6	5944.36	5897.71					
4191	Qrf	7-Oct-93	20.2	5955.6	5956.99	5936.79					
4286	Qrf	5-Oct-93	25.6	5956.3	5957.87	5932.27					
4291	Ka?(cs)	7-Oct-93	-1	5952.5	5953.9	dry					
4386	Qrf	1-Oct-93	-1	5972.9	5974.46	dry					
4487	Qc	4-Oct-93	-1	5949.6	5951.1	dry					
4491	Qrf	7-Oct-93	31.24	5949.5	5951.15	5919.91					
4591	Qrf	7-Oct-93	45.28	5948.7	5950.25	5904.97					
4691	Qrf	7-Oct-93	47.75	5944.7	5946.43	5898.68					
4891	Qrf	8-Oct-93	· -1 *	5939.2	5940.76	dry					
4991	Qrf	8-Oct-93	41.82	5936.9	5938.63	5896.81					
5091	Qrf	8-Oct-93	44.05	5937.6	5939.24	5895.19					
5191	Qrf	8-Oct-93	44.72	5938.4	5939.85	5895.13					
5291	Qrf	7-Oct-93	37.18	5941.2	5943	5905.82					
5391	Qrf	6-Oct-93	36.24	5940.2	5941.67	5905.43					

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TABLE 2.5-1
OU2 GROUNDWATER ELEVATIONS
FOURTH QUARTER 1993

Well Number	Lithologic Unit	Measurement Date	Depth to Water (ft)	Ground Surface Elevation	Top of Casing Elevation	Groundwater Elevation			
5691	Qrf	6-Oct-93	31.69	5947.6	5948.99	5917.3			
5991	, Óc	8-Oct-93	25.48	5908.3	5909.91	5884.43			
6091	Qrf	6-Oct-93	37.67	5930.1	5931.6	5893.93			
6191	Qrf	5-Oct-93	35.76	5919.2	5920.72	5884.96			
6286	Kl(ss)	4-Oct-93	28.9	5902	5903.18	5874.28			
6291	Ka?(cs)	5-Oct-93	34.05	5897.9	5899.28	5865.23			
6386	Qc ·	4-Oct-93	16.96	5901.1	5902.01	5885.05			
6391	Qrf	5-Oct-93	26.33	5903.6	5905.17	5878.84			
6486	Qvf	7-Oct-93	11.36	5839.1	5841.05	5829.69			
6491	Kl (ss)	5-Oct-93	17.7	5671.5	5673.25	5655.55			
6586	Qvf	6-Oct-93	6.28	5786.7	5788.27	5781.99			
6591	Ka (No.1)	7-Oct-93	20.61	5978.3	5979.78	5959.17			
6691	Qrf	7-Oct-93	22.03	5978.3	5979.94	5957.91			
6786	Qc	6-Oct-93	16.72	5802.3	5803.97	5787.25			
6791	Qrf	, 7-Oct-93	, -1,	5978.9	5980.38	dry			
6891	Qrf	7-Oct-93	13.1	5974.1	5975.62	5962.52			
6991	Qrf	7-Oct-93	20.94	5972.9	5974.57	5953.63			
7191	Qrf	7-Oct-93	22.46	5974.8	5976.34	5953.88			
7291	Qrf	7-Oct-93	22.62	5977.3	5978.8	5956.18			
7391	Qc	5-Oct-93	9.82	5949.1	5950.61	5940.79			
7891.	Qrf	6-Oct-93	29.5	5957.8	5959.45	5929.95			
7991	Qrf	7-Oct-93	27.75	5954.9	5956.78	5929.03			
8091	Qrf	7-Oct-93	-1	5947.9	5949.51	dry			
8291	· Qrf	7-Oct-93	16.46	5950.2	5951.94	5935.48			
8391	Qrf	7-Oct-93	41.9	5947.2	5948.65	5906,75			
8491	Qrf	7-Oct-93	18.28	5950,6	5952.16	5933.88			
8591	Qrf	7-Oct-93	46.08	5948.6	5950.12	5904.04			
8891	Qrf	7-Oct-93	23.73	5976.4	5978.06	5954.33			
9091	Qrf	7-Oct-93	23.54	5975.2	5976.79	5953.25			
9691	Ka(No. 1)	5-Oct-93	13.4	5935.6	5937.05	5923.65			
10991	Ka(No.1)	8-Oct-93	44.75	5940	5941.64	5896.89			
11291	Qrf	6-Oct-93	-1	5930.6	5932.12	dry			
11491	Qrf	6-Oct-93	-1	5948.2	5949.76	dry			
11691	Ka (No.1)	5-Oct-93	34.73	5938.6	5939.91	5905.18			
11791	KI(cs)	6-Oct-93	9.13	.5923.3	5925.03	5915.9			

TABLE 2.5-1
OU2 GROUNDWATER ELEVATIONS
FOURTH QUARTER 1993

Well Number	Lithologic Unit	Measurement Date	Depth to Water (ft) ¹	Ground Surface Elevation	Top of Casing Elevation	Groundwater Elevation
11891	Ka (No.1)	5-Oct-93	26.23	5945.5	5947.44	5921.21
12091	Ka (No.1)	1-Oct-93	19.03	5971.6	5973.27	5954.24
12191	Ka (No.1)	6-Oct-93	28.26	5956.5	5958.19	5929.93
12291	Ka (No.1)	5-Oct-93	16.27	5971	5972.73	5956.46
12391	Ka (No.1) & Kl(ss)	6-Oct-93	50.1	5940.1	5941.7	5891.6
12491	Ka (No.1)	6-Oct-93	31.54	5946.8	5948.35	5916.81
12691	Ka (No.1)	6-Oct-93	35.8	5949.7	5951.08	5915.28
12891	Qrf	7-Oct-93	38.12	5946.8	5948.35	5910.23
12991	Ka (No.1)	7-Oct-93	24.52	5965.7	5967.22	5942.7
13091	Qrf	7-Oct-93	21.47	5973.7	5975.2	5953.73
13191	Ka (No.1)	7-Oct-93	20.24	5978.3	5979.9	5959.66
13291	Qrf	8-Oct-93	-1	5978.5	5979.97	dry
13391	Qrf	5-Oct-93	38.47	5923.8	5925.35	5886.88
13491	Qrf	5-Oct-93	25.43	5961.9	5963.42	5937.99
13591	Qrf	7-Oct-93	-1	5965.9	5967.55	dry
20191	Ka (No.1)	6-Oct-93	32.52	5946.9	5948.49	5915.97
20291	Qrf	6-Oct-93	31.66	5947.2	5948.58	5916.92
20491	Qrf	6-Oct-93	31.74	5947.2	5948.71	5916.97
20591	Qrf	7-Oct-93	22.4	5968	5969.61	5947.21
20691	Ka (No.1)	7-Oct-93	22.52	5968.1	5969.63	5947.11
20791	Ka?(cs)	7-Oct-93	32.35	5967.9	5969.49	5937.14
21091	Qrf	6-Oct-93	36.18	5948.6	5950.12	5913.94
21191	Ka (No.1)	6-Oct-93	31.6	5946.9	5948.52	5916.92
23193	Kl(ss, cs)	6-Oct-93	37.69	5948.2	5950.46	5912.77
24093	Qrf	30-Sep-93	-1	5956	5957.4	dry
24193	Ka (No.1)	22-Oct-93	29.02	5956	5959.	5929.98
24293	Qrf		-i	. 5957	5957.3	dry
24393	Ka (No.1)	26-Oct-93	29.44	5957	5959.1	5929.66
24493	Qrf	30-Sep-93	-1	5956	5957.95	dry
24593	Qrf	30-Sep-93	-1	5956	5957.7	dry
24693	Qrf	30-Sep-93	-1	5956	5957	dry
24993	Ka (No.1)	30-Sep-93	27.58	5956	5958	5930.42
25093	Ka (No.1)	30-Sep-93	27.42	5957	5957.9	5930.48
34591	Qc	5-Oct-93	-1	5952.2	5954.63	dry
34791	Qc	5-Oct-93	7.76	5951.4	5953.91	5946.15

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TABLE 2.5-1
OU2 GROUNDWATER ELEVATIONS
FOURTH QUARTER 1993

Well Number	Lithologic Unit	Measurement Date	Depth to Water (ft) ¹	Ground Surface Elevation	Top of Casing Elevation	Groundwater Elevation
40491	Qvf	5-Oct-93	-1	5677.3	5678.66	dry
40791	Qvf	5-Oct-93	-1	5688.5	5690.24	dry
41591	Qvf	5-Oct-93	11.91	5725.5	5727.27	5715.36
41691	Qvf	5-Oct-93	10.51	5644	5645.88	5635.37
B218789	Qrf	5-Oct-93	26.34	5962.8	5964.52	5938.18

Note: -1 indicates dry well.

TABLE 2.5-2 ESTIMATED HYDRAULIC CONDUCTIVITY OF ROCKY FLATS ALLUVIUM BASED ON RESULTS OF 1986 AND 1987 AQUIFER TESTS

Site/Well Number	Hydraulic Conductivity from 1986 Pump Tests (cm/sec)	Hydraulic Conductivity from 1987 Slug Tests (cm/sec)
3986	4E-05	
4186	9E-05	
4286	•	5E-02
1787		6E-05
3287		1E-03

Source: Rockwell International 1987. Draft Remedial Investigation Report for 903 Pad, Mound, and East Trenches Areas.

TABLE 2.5-3 ESTIMATED HYDRAULIC CONDUCTIVITY OF ROCKY FLATS ALLUVIUM BASED ON RESULTS OF 1992 AQUIFER TESTS

	Hydraulic Conductivity from Pump Test
Site/Well Number	(cm/sec)
Site 2	
11491 (Alluvial)	1.6E-3 to 1.8E-3
05691 (Alluvial)	1.8E-03
20491 (Alluvial)	3.1E-3 to 3.6E-3
20291 (Alluvial)	8.1E-4 to 8.8E-4
Site 3	
1787 (Alluvial)	1.6E-4 to 9.2E-4
20591 (Alluvial)	1.4E-4 to 8.6E-4
20691 (Alluvial)	1.2E-4 to 4.4E-4

Source: DOE 1992. Phase II RFI/RI Aquifer Test Report.

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TABLE 2.5-4 ESTIMATED HYDRAULIC CONDUCTIVITY OF ARAPAHOE NO. 1 SANDSTONE BASED ON RESULTS OF 1987 AQUIFER TESTS

Hydraulic Conductivity from Slug Tests

Well Number	(cm/s)
987	3E-03
2387	2E-04
2587	2E-03
3687	1E-03

Source: Rockwell International 1987. Draft Remedial Investigation Report for 903 Pad, Mound, and East Trenches Areas.

TABLE 2.5-5 ESTIMATED HYDRAULIC CONDUCTIVITY OF ARAPAHOE NO. 1 SANDSTONE BASED ON RESULTS OF 1992 AOUIFER TESTS

SITE/WELL NUMBER	HYDRAULIC CONDUCTIVITY FROM PUMP TEST (cm/s)
Site 1	
3687 (Bedrock)	4.2E-04 to 4.8E-04
20991 (Bedrock)	3.7E-04 to 6.2E-04
21091 (Bedrock)	4.1E-04 to 5.1E-04
20891 (Bedrock)	4.7E-04 to 6.0E-04

Source: DOE 1992. Phase II RFI/FI Aquifer Test Report.

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TABLE 2.5-6
PUMPING TEST RESULTS
1994

	DISTANCE FROM PUMPING	TRANSMISSIVITY	SATURATED	HYDRAULIC CONDUCTIVITY	Storativity
WELL/METHOD	WELL (ft)	(ft²/min)	THICKNESS (ft.)	(ft/min) (cm/sec)	(S)
24193 (Pumping Well)					
Theis (Unconfined)	0.17*	6.7×10^{-2}	23	2.9×10^{-3} 1.5×10^{-3}	6.6×10^{-3}
Cooper-Jacob (Unconfined)	·	7.5 x 10 ⁻²		3.3×10^{-3} 1.7×10^{-3}	1.2 x 10 ⁻³
24993					
Theis (Unconfined)	5.1	1.0×10^{-1}	23.9	4.2×10^{-3} 2.1×10^{-3}	2.4×10^{-3}
Cooper-Jacob (Unconfined)		1.3×10^{-1}	ł	5.4×10^{-3} 2.7×10^{-3}	5.2 x 10 ⁻⁴
25093					
Theis (Unconfined)	22.1	1.2×10^{-1}	28.5	4.2×10^{-3} 2.1×10^{-3}	9.1 x 10 ⁻⁴
Cooper-Jacob (Unconfined)		1.2 x 10 ⁻¹		4.2×10^{-3} 2.1×10^{-3}	7.6 x 10 ⁻⁴
12191					
Theis (Unconfined)	55.6	1.6×10^{-1}	23.5	6.8×10^{-3} 3.5×10^{-3}	3.1×10^{-3}
Cooper-Jacob (Unconfined)		1.7 x 10 ⁻¹		7.2×10^{-3} 3.7×10^{-3}	2.4×10^{-3}

TABLE 2.6-1
ANALYTES DETECTED IN SUBSURFACE SOILS AT IHSS 110 (Trench T-3)

A nalyte	Background Mean plus two standard deviations	Number of Samples	Number of Detections(5)	Percent Detections	Concentration or Activity Range(1)	Mean Concentration o Activity(2)
Volatile Organic Compounds (μg/kg) -						•
1,1,1,-Trichloroethane	NA	57	9 .	15.8%	6-27,000J	8,046
1,1-Dichloroethene	NA	57	1	1.8%	9	9
1,2-Dichloroethane	NA	57	2	3.5%	6J-14J	10
1.2-Dichloroethene	NA	45	i	2.2%	1Ј	1
2-Butanone	NA	53	7	13.2%	40J-88	60
Acetone	NA	57	15	26.3%	36-86,000	10,233
Carbon tetrachloride	· NA	57	19	33.3%	3J-700,000	62,964
Chloroform	NA	57	17	29.8%	1J-8,800	534
Ethylbenzene	NA	57	1	1.8%	2J	2
Methylene chloride	NA	57	21	36.8%	4J-55,000B-RV	5,792
etrachloroethene	NA	57	28	49.1%	1J-13,000,000D	543,280
Coluene	NA	57	41	71.9%	5J-7,600J	484
Trichloroethene	NA	57)	7	12.3%	1J-120,000	18,302
Semivolatile Organic Compounds (µg/kg)(6)					-	
2-Methylnaphthalene	NA	19	1	5.3%	8,100D	8,100
-Methylphenol	NA ·	19	1	5.3%	450	450
-Methylphenol	NA	19	1 .	5.3%	2,900	2,900
Bis(2-ethylhexyl)phthalate	NA	18	18	100.0%	51J-5,500	523
Di-n-butyl phthalate	NA	19	I	5.3%	1,300	1,300
Hexachlorobutadiene	NA	19	1	5.3%	170J	170
Hexachloroethane	NA	19	2 .	10.5%	370-1,100	735
Naphthalene	NA	19	1	5.3%	2,000	2,000
Phenanthrene	NA	19	1	5.3%	2,700	2,700
Pesticides/PCBs (μg/kg)	•					
Aroclor-1254	NA	19	1	5.3%	6,900J	6,900

TABLE 2.6-1
ANALYTES DETECTED IN SUBSURFACE SOILS AT IHSS 110 (Trench T-3)

Analyte	Background Mean plus two standard deviations	Number of Samples	Number of Detections(5)	Percent Detections	Concentration or Activity Range(1)	Mean Concentration or Activity(2)
PCOC Metals above background (mg/kg)(3)						
Arsenic	13.2	23	4	17.4%	15-26	20.75
Barium	289	23	1	4.3%	413	413
Cadmium	1.7	23	6	26.1%	2.1-6.2	3.48
Calcium	39,393.6	23	. 1	4.3%	67,300	67,300
Lead	24.9	23	1	4.3%	86.4	86.4
Manganese	901.6	23	2	8.7%	1,440B-3,090	2,265
Silver	24.6	23	. 1	4.3%	96.5	96.5
PCOC Radionuclides above background (pCi/g)(3)(4)						
Americium-241	0.012	19	8	42.1%	0.01523J-0.5983	0.124
Gross beta	36.839	19	1	5.3%	56.74	56.74
Plutonium-239/240	0.018	19	13	68.4%	0.02-3.12	0.31
Radium-226	1.208	5	2	40.0%	1.226-1.275	1.251
Strontium-89,90	0.747	19	3	15.8%	0.8-1.1	0.97
Fritium (pCi/l)	395.211	19	1	5.3%	400	400
Uranium-233,-234	2.643	9	1	11.1%	14.35	14.35
Jranium-235	0.114	9	1	11.1%	0.7509	0.7509
Uranium-238	1.485	19	3	15.8%	1.611-26.37	9.93

Locations: 02991, 10191, 12191, 21693, 22493, 24093, 24193, 24493-24793, 24993, 25093, BH3987, BH4087

NA - Not Applicable

- (1) J qualifier represents estimated result, D qualifier represents dilution result, B qualifier for organics indicates analyte was detected in blank sample, and B qualifier for metals represents estimated result.
- (2) The calculation for the mean concentration includes all J, D, and B qualified data.
- (3) For metals and radionuclides, only potential chemicals of concern (PCOCs) have been reviewed and are presented on this table. (See Background discussion in Section 4.0 for list of PCOCs.)

TABLE 2.6-1 ANALYTES DETECTED IN SUBSURFACE SOILS AT IHSS 110 (Trench T-3)

	Background					
	Mean plus two				Concentration	Mean
·	standard	Number of	Number of	Percent	or Activity	Concentration or
Analyte	deviations	Samples	Detections(5)	Detections	Range(1)	Activity(2)

- (4) Radionuclide activities less than or equal to zero are considered to be non-detections.
- (5) Radionuclide and metal results less than the background mean plus 2 standard deviations are considered to be non-detections.
- (6) Background concentrations do not exist and are not applicable for organic compounds.

TABLE 2.6-2
ANALYTES DETECTED IN UHSU GROUNDWATER SAMPLES COLLECTED PRIOR TO ABANDONMENT
OF WELLS DURING WARP
(September 1994)

Analyte	Number of Samples	Number of Detections	Percent Detections	Concentration Range (µg/l)	Mean Concentration (μg/l)
Volatile Organic			,		
Top of Groundwater Sampling	Interval ⁽¹⁾	•			
1,1,1-Trichloroethane	4	4	100%	53 - 190	126
1,1-Dichloroethene	. 4	4 .	100%	35 -76	59
Carbon tetrachloride	4	4	100%	1500 - 5200	3350
Chloroform	4	4	100%	82 - 340	216
cis-1,2-Dichloroethene	4	2	50%	9 - 11	10
Tetrachloroethene	4	4	100%	780 - 1600	1395
Trichloroethene	. 4	4	100%	64 - 110	94
Methylene chloride	4	2	50%	29 - 36	33
Bottom of Well Sampling Interv	al ⁽¹⁾				
1,1,1-Trichloroethane	. 4	4	100%	14 - 180	76
1,1-Dichloroethene	4	4	100%	9 - 180	35
Carbon tetrachloride	4	4	100%	490 - 4500	2020
Chloroform	4	4	100%	22 - 310	131
cis-1,2-Dichloroethene	4	2	50%	8 - 9	8.5
Methylene Chloride	4	3	75%	8 - 47	22
Tetrachloroethene	4	4	. 100%	250 - 1500	748
Trichloroethene	4	4	100%	40 - 100	69

⁽¹⁾ See text for discussion on sample collection.

TABLE 2.6-3
SUMMARY OF ANALYTICAL RESULTS FOR DISTILLATION SAMPLE (97 to 98 Degrees Celsius)

Phase	Temperature Range	Sample ID	Analyte	Less Than	Result	Detection Limit	Lab Qualifier	Units	Distilled Volume (mL)	Method Number
Top Layer	97-98	C0641	Acetone		230,000	50,000		ug/L	13	8260
Water		C0641	Tetrachloroethene		120,000	25,000		ug/L		8260
]	C0641	Trichloroethene	ĺ.	120,000	25,000		ug/L		8260
]	C0641	2,4-Dimethylphenol		4,000	2,700		ug/L		8270
}	,	C0641	2-Methylnaphthalene		1,400	2,700	J	ug/L		8270
	į	C0641	2-Methylphenol		5,000	2,700		ug/L		8270
1		C0641	4-Methylphenol		33,000	2,700		ug/L		8270
!		C0641	Di-n-butylphthalate		350	2,700	J	ug/L		8270
		C0641	Naphthalene	,	1,200	2,700	J	ug/L		8270
İ		C0641	Phenol		2,200	2,700	J	ug/L		8270
		C0641	Diesel Range Organics	<	270	270		mg/Kg		8015M
		C0641 ·	Gasoline Range Organics		400	.270	X	mg/Kg		8015M
Bottom Layer	97-98	C0642	1,1,1-Trichloroethane		2,200,000	6,000,000	J	ug/L	27	8260
DNAPL		C0642	Acetone		22,000,000	12,000,000	В	ug/L		8260
		C0642	Tetrachloroethene		660,000,000	24,000,000		ug/L		8260
ì		C0642	Trichloroethene		120,000,000	6,000,000		ug/L		8260
		C0642	2,4-Dimethylphenol		57,000	152,400	J	ug/L		8270
	٠.	C0642	2-Methylnaphthalene		170,000	76,200		ug/L		8270
		C0642	2-Methylphenol		26,000	76,200	. J	ug/L		8270
1		C0642	4-Methylphenol		130,000	76,200		ug/L		8270
	,	C0642	Naphthalene	í	110,000	76,200		ug/L		8270
		C0642	Diesel Range Organics		11000	3600	Y	mg/Kg		8015M
		C0642	Gasoline Range Organics		170000	9000	X	mg/Kg		8015M

LNAPL - light non-aqueous phase liquid

NA - not applicable

X - the data does not match the gasoline peak pattern as seen in the standard

Y - the data does not match the diesel peak pattern as seen in the standard

J - estimated value

B - associated method blank contains this compound

E - exceeds calibration range

• - same phase - not biphasic

X assigned to diesel - sample contained HC throughout the range - result may be biased high

G assigned to gasoline - the sample is not gasoline or diesel, but believed to be some other HC

TABLE 2.6-4
SUMMARY OF ANALYTICAL RESULTS FOR DISTILLATION SAMPLE (98 to 100 Degrees Celsius)

Phase	Temperature Range	Sample ID	Analyte	Less Than	Result	Detection Limit	Lab Qualifier	Units	Distilled Volume (mL)	Method Number
Top Layer	98-100	C0643	Acetone		9,800	10,000	J	ug/L	200	8260
Water	, , , , ,	C0643	Tetrachloroethene		130,000	5,000	1	ug/L	į	8260
	į	C0643	Trichloroethene		65,000	5,000		ug/L		8260
	İ	C0643	2,4-Dimethylphenol		9,900	6,250		ug/L		8270
	1	C0643	2-Methylphenol		10,000	6,250		ug/L		8270
	ł	C0643	4-Methylphenol	. 1	64,000	6,250		ug/L		8270
		C0643	Benzyl alcohol		160	250	J	ug/L		8270
		C0643	Phenol	1	4,400	6,250	J	ug/L		8270
	i	C0643	Diesel Range Organics	<	26	26		mg/Kg	} 	8015M
		C0643	Gasoline Range Organics		470	26	Х	mg/Kg		8015M
Bottom Layer	98-100	C0644	Acetone		34,000,000	11,750,000	В	ug/L	100	8260
DNAPL		C0644	Tetrachloroethene		640,000,000	23,500,000	l F	ug/L		8260
	i	C0644	Trichloroethene		49,000,000	23,500,000		ug/L		8260
		C0644	2,4-Dimethylphenol		120,000	72,500		ug/L	ļ	8270
		C0644	2-Methylnaphthalene		370,000	72,500		ug/L	Ì	8270
		C0644	2-Methylphenol		48,000	72,500	J	ug/L		8270
	1	C0644	4-Methylphenol	1	250,000	72,500	ĺ	ug/L		8270
		C0644	Naphthalene		240,000	145,000		ug/L		8270
		C0644	Diesel Range Organics		29000	3600	I -	mg/Kg		8015M
		C0644	Gasoline Range Organics		250000	18000	Х	mg/Kg		8015M

LNAPL - light non-aqueous phase liquid

NA - not applicable

X - the data does not match the gasoline peak pattern as seen in the standard

Y - the data does not match the diesel peak pattern as seen in the standard

J - estimated value

B - associated method blank contains this compound

E - exceeds calibration range

* - same phase - not biphasic

X assigned to diesel - sample contained HC throughout the range - result may be biased high

G assigned to gasoline - the sample is not gasoline or diesel, but believed to be some other HC

TABLE 2.6-5
SUMMARY OF ANALYTICAL RESULTS FOR DISTILLATION SAMPLE (100 to 105 Degrees Celsius)

Phase	Temperature Range	Sample ID	Analyte	Less Than	Result	Detection Limit	Lab Qualifier	Units	Distilled Volume (mL)	Method Number
Top Layer	100-105	C0645	Acetone		6,000	10,000	J	ug/L	156	8260
Water		C0645	Tetrachloroethene		150,000	5,000		ug/L		8260
		C0645	Trichloroethene		3,600	2,500		ug/L		8260
		C0645	2,4-Dimethylphenol		20,000	6,800		ug/L		8270
1 .		C0645	2-Methylnaphthalene		3,600	6,800	J	ug/L		8270
	•	C0645	2-Methylphenol		13,000	6,800		ug/L		8270
		C0645	4-Methylphenol		84,000	6,800		ug/L		8270
		C0645	Di-n-butylphthalate		27	137	J	ug/L		8270
	•	C0645	Naphthalene		2,700	6,800	J	ug/L		8270
		C0645	Phenanthrene		. 30	137	J	ug/L		8270
		C0645	Phenol		4,700	6,800	J	ug/L		8270
		C0645	Diesel Range Organics		330	70	Y	mg/Kg		8015M
		C0645	Gasoline Range Organics		1700	70	X	mg/Kg		8015M
Bottom Layer	100-105	C0646	Tetrachloroethene		320,000,000	10,500,000		ug/L	39	8260
DNAPL	:	C0646	Trichloroethene		3,500,000	5,250,000	J	ug/L		8260
. '		C0646	2,4-Dimethylphenol		410,000	320,000		ug/L	f 	8270
		C0646	2-Methylnaphthalene		1,200,000	320,000		ug/L		8270
		C0646	2-Methylphenol		100,000	64,000	ì	ug/L		8270
		C0646	4-Methylphenol		470,000	320,000		ug/L		8270
		C0646	Naphthalene		890,000	320,000		ug/L	İ	8270
		C0646	Phenanthrene		14,000	64,000	J	ug/L		8270
		C0646	Diesel Range Organics		150000	45000	Y	mg/Kg		8015M
		C0646	Gasoline Range Organics		600000	45000	X	mg/Kg		8015M

LNAPL - light non-aqueous phase liquid

NA - not applicable

- X the data does not match the gasoline peak pattern as seen in the standard
- Y the data does not match the diesel peak pattern as seen in the standard
- J estimated value
- B associated method blank contains this compound
- E exceeds calibration range
- - same phase not biphasic
- X assigned to diesel sample contained HC throughout the range result may be biased high
- G assigned to gasoline the sample is not gasoline or diesel, but believed to be some other HC

TABLE 2.6-6
SUMMARY OF ANALYTICAL RESULTS FOR DISTILLATION SAMPLE (100 to 106 Degrees Celsius)

Phase	Temperature Range	Sample ID	Analyte	Less Than	Result	Detection Limit	Lab Qualifier	Units	Distilled Volume (mL)	Method Number
Top Layer	100-106	C0647	m,p-Xylene		28,000	125,000	J	ug/L	48	8260
LNAPL		C0647	Tetrachloroethene		5,300,000	500,000	В	ug/L		8260
		C0647	2,4-Dimethylphenol		710,000	415,000		ug/L		8270
		C0647	2-Methylnaphthalene		3,500,000	415,000		ug/L		8270
		C0647	2-Methylphenol		97,000	415,000	J	ug/L		8270
		C0647	4-Methylphenol		560,000	415,000		ug/L		8270
	ļ	C0647	Di-n-butylphthalate		20,000	41,500	j	ug/L		8270
	ŀ	C0647	Naphthalene		2,400,000	415,000		ug/L		8270
		C0647	Phenanthrene		74,000	415,000	J.	ug/L		8270
		C0647	Diesel Range Organics		980000	90000	Y	mg/Kg		8015M
		C0647	Gasoline Range Organics		1000000	90000	X	mg/Kg		8015M
Bottom Layer	100-106	C0648	Acetone		4,400	2,000	•	ug/L	437	8260
Water	-	C0648	Ethylbenzene	ļ	200	1,000	J	ug/L		8260
		C0648	m,p-Xylene	İ	2,600	1,000		ug/L		8260
		C0648	o-Xylene		1,700	1,000		ug/L		8260
		C0648	Tetrachloroethene		42,000	2,500		ug/L		8260
		C0648	Trichloroethene	1	220	1,000	J	ug/L		8260
		C0648	2,4-Dimethylphenol		24,000	8,700		ug/L	•	8270
		C0648	2-Methylnaphthalene		3,700	8,700	J	ug/L		8270
	ŀ	C0648	2-Methylphenol		10,000	8,700		ug/L		8270
		C0648	4-Methylphenol	ŀ	81,000	8,700		ug/L		8270
		C0648	Di-n-butylphthalate	}	270	43		ug/L		8270
		C0648	Naphthalene	1	2,400	8,700	. J	ug/L		8270
		C0648	Phenanthrene		610	43		ug/L		8270
		C0648	Phenol		3,600	. 8,700	J	ug/L .		8270
		C0648	Diesel Range Organics	'	8800	860	Y	mg/Kg		8015M
		C0648	Gasoline Range Organics	L	10000	860	X	mg/Kg		8015M

LNAPL - light non-aqueous phase liquid

NA - not applicable

- X the data does not match the gasoline peak pattern as seen in the standard
- Y the data does not match the diesel peak pattern as seen in the standard
- J estimated value
- B associated method blank contains this compound
- E exceeds calibration range
- - same phase not biphasic
- X assigned to diesel sample contained HC throughout the range result may be biased high
- G assigned to gasoline the sample is not gasoline or diesel, but believed to be some other HC

TABLE 2.6-7
SUMMARY OF ANALYTICAL RESULTS FOR DISTILLATION SAMPLE (106 to 109 Degrees Celsius)

Phase	Temperature Range	Sample ID	Analyte	Less Than	Result	Detection Limit	Lab Qualifier	Units	Distilled Volume (mL)	Method Number
Top Loves	106-109	C0704	Acetone		140,000	100,000		ug/L	4	8260
Top Layer	100-109	C0704 C0704			1,200,000			ug/L		8260
LNAPL			Methylene Chloride Tetrachloroethene		490,000	•	В	ug/L ug/L		8260
		C0704 C0704			3,300,000	•	Ь	ug/L ug/L		8270
		C0704 C0704	2-Methylnaphthalene 4-Methylphenol		320,000		J	ug/L	ĺ	8270
		C0704 C0704	· -		59,000	1	J	ug/L ug/L		8270
		C0704 C0704	bis(2-Ethylhexyl)phthalate		40,000		J	ug/L ug/L	·	8270
=			Di-n-butylphthalate		2,100,000	· 1	,	ug/L ug/L		8270
		C0704	Naphthalene Phenanthrene		100,000	· I	ī	ug/L ug/L	j	8270
		C0704			100,000	· ·	Y	mg/Kg	ļ	8015M
		C0704 C0704	Diesel Range Organics Gasoline Range Organics		650000		X	mg/Kg	•	8015M
		C0704	Casonnic Range Organics		030000	100000	**		l t	
Bottom Layer	106-109	C0649	Naphthalene		2,000	2,440	J	ug/L	100	8270
Water		C0649	Phenanthrene		69	. 244	J	ug/L		8270
		C0649	Phenol		860	2,440	. J	ug/L	<u> </u>	8270
		C0649	Diesel Range Organics		1800	1	Y	mg/Kg		8015M
		C0649	Gasoline Range Organics		1500	96	X	mg/Kg		8015M

LNAPL - light non-aqueous phase liquid

NA - not applicable

X - the data does not match the gasoline peak pattern as seen in the standard

Y - the data does not match the diesel peak pattern as seen in the standard

J - estimated value

B - associated method blank contains this compound

E - exceeds calibration range

• - same phase - not biphasic

X assigned to diesel - sample contained HC throughout the range - result may be biased high

G assigned to gasoline - the sample is not gasoline or diesel, but believed to be some other HC

TABLE 2.6-8
SUMMARY OF ANALYTICAL RESULTS FOR DISTILLATION SAMPLE (109 to 120 Degrees Celsius)

Phase	Temperature Range	Sample ID	Analyte	Less Than	Result	Detection Limit	Lab Qualifier	Units	Distilled Volume (mL)	Method Number
Top Layer	109-120	C0705	Methylene Chloride		430,000	25,000		ug/L	50	8260
LNAPL		C0705	Tetrachloroethene		97,000	25,000	В	ug/L		8260
		C0705	2-Methylnaphthalene		3,600,000	500,000		ug/L		8270
		C0705	4-Methylphenol		380,000	500,000	J	ug/L		8270
		C0705	bis(2-Ethylhexyl)phthalate		49,000	50,000	J	ug/L		8270
		C0705	Di-n-butylphthalate		38,000	50,000	J	ug/L		8270
		C0705	Naphthalene		2,200,000	500,000		ug/L		8270
		C0705	Phenanthrene		110,000	500,000	J	ug/L		8270
		C0705	Diesel Range Organics		1100000	108000	Y	mg/Kg		8015M
		C0705	Gasoline Range Organics		700000	108000	X	mg/Kg		8015M
Bottom Layer	109-120	C0698	2-Butanone		290	200		ug/L	50	8260
Water		C0698	Acetone		2,800	200		ug/L		8260
		C0698	Tetrachloroethene	!	63	100		ug/L		8260
		C0698	2,4-Dimethylphenol		18,000	4,500	•	ug/L		8270
		C0698	2-Methylnaphthalene		7,900	4,500		ug/L		8270
		C0698	2-Methylphenol		4,400	4,500	J	ug/L		8270
		C0698	4-Methylphenol		52,000	4,500	,	ug/L		8270
		C0698	bis(2-Ethylhexyl)phthalate		96	454	J	ug/L	-	8270
		C0698	Di-n-butylphthalate		100	454	J	ug/L		8270
		C0698	Naphthalene		4400	4,500	J	ug/L		8270
		C0698	Phenanthrene		170	454	J	ug/L		8270
		C0698	Phenol		1,800	4,500	J	ug/L		8270
		C0698	Diesel Range Organics		1700	180	Y	mg/Kg		8015M
		C0698	Gasoline Range Organics		2200	180	X	mg/Kg		8015M

LNAPL - light non-aqueous phase liquid

NA - not applicable

X - the data does not match the gasoline peak pattern as seen in the standard

Y - the data does not match the diesel peak pattern as seen in the standard

J - estimated value

B - associated method blank contains this compound

E - exceeds calibration range

• - same phase - not biphasic

X assigned to diesel - sample contained HC throughout the range - result may be biased high

G assigned to gasoline - the sample is not gasoline or diesel, but believed to be some other HC

(4045-150-0228-581)(TM4-T26X.XLS)(3/8/95 1:15 AM)

TABLE 2.6-9
SUMMARY OF ANALYTICAL RESULTS FOR DISTILLATION SAMPLE (180 to 205 Degrees Celsius)

Phase	Temperature Range	Sample ID	Analyte	Less Than	Result	Detection Limit	Lab Qualifier	Units	Distilled Volume (mL)	Method Number
NA ·	180-205	C0702 C0702 C0702 C0702 C0702 C0702	2,4-Dimethylphenol 2-Methylnaphthalene 2-Methylphenol 4-Methylphenol Naphthalene Phenol		66,000 160,000 16,000 210,000 94,000 56,000	100,000 50,000 100,000 100,000	1	ug/L ug/L ug/L ug/L ug/L ug/L	0.5	8270 8270 8270 8270 8270 8270

LNAPL - light non-aqueous phase liquid

NA - not applicable

X - the data does not match the gasoline peak pattern as seen in the standard

Y - the data does not match the diesel peak pattern as seen in the standard

J - estimated value

B - associated method blank contains this compound

E - exceeds calibration range

• - same phase - not biphasic

X assigned to diesel - sample contained HC throughout the range - result may be biased high

G assigned to gasoline - the sample is not gasoline or diesel, but believed to be some other HC

TABLE 2.6-10
SUMMARY OF ANALYTICAL RESULTS FOR DISTILLATION SAMPLE RESIDUE

Phase	Temperature Range	Sample ID	Analyte	Less Than	Result	Detection Limit	Lab Qualifier	Units	Distilled Volume (mL)	Method Number
NA	RESIDUE	C0703	2-Butanone		1,700	1,240		ug/L	785	8260
	100000	C0703	Acetone		9,600	1,240		ug/L		8260
		C0703	Benzene		830	620		ug/L		8260
		C0703	Carbon Disulfide		9,400	620		ug/L		8260
		C0703	Ethylbenzene		1,300	620		ug/L		8260
		C0703	m,p-Xylenes		230	620	J	ug/L		8260
		C0703	Tetrachloroethene		1,700	620	В	ug/L		8260
	-	C0703	Toluene		4,100	620		ug/L		8260
]	C0703	Trichloroethene		470	620	J	ug/L		8260
		C0703	2,4-Dimethylphenol		23,000	85,600	J	ug/L		8270
		C0703	2-Methylnaphthalene		380,000	85,600		ug/L	·	8270
	1	C0703	4-Methylphenol		28,000	85,600	J	ug/L		8270
ŀ		C0703	bis(2-Ethylhexyl)phthalate		350,000	- 85,600		ug/L		8270
		C0703	Di-n-butylphthalate		100,000	85,600		` ug/L		8270
		C0703	Naphthalene		97,000	428,000	J	· ug/L		8270
,	ĺ	C0703	Phenanthrene		180,000	428,000	J	ug/L		8270
		C0703	Diesel Range Organics		660000	180000	Y	mg/Kg		8015M
	<u> </u>	C0703	Gasoline Range Organics	<	180000	180000	X	mg/Kg		8015M

LNAPL - light non-aqueous phase liquid

NA - not applicable

X - the data does not match the gasoline peak pattern as seen in the standard

Y - the data does not match the diesel peak pattern as seen in the standard

J - estimated value

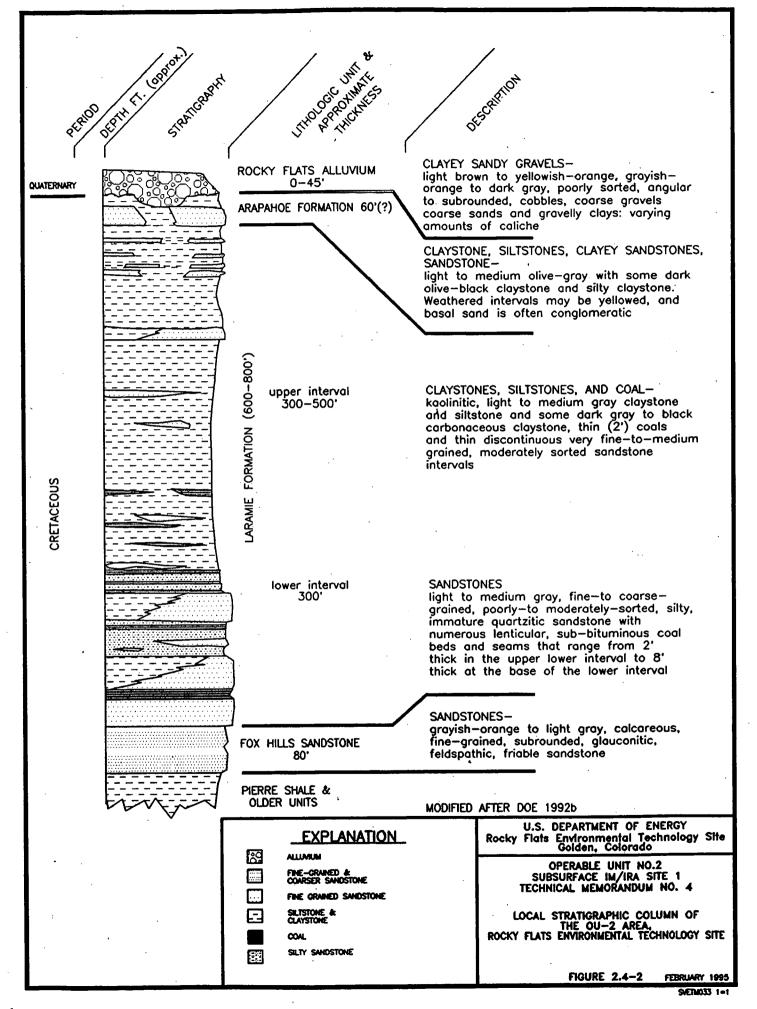
B - associated method blank contains this compound

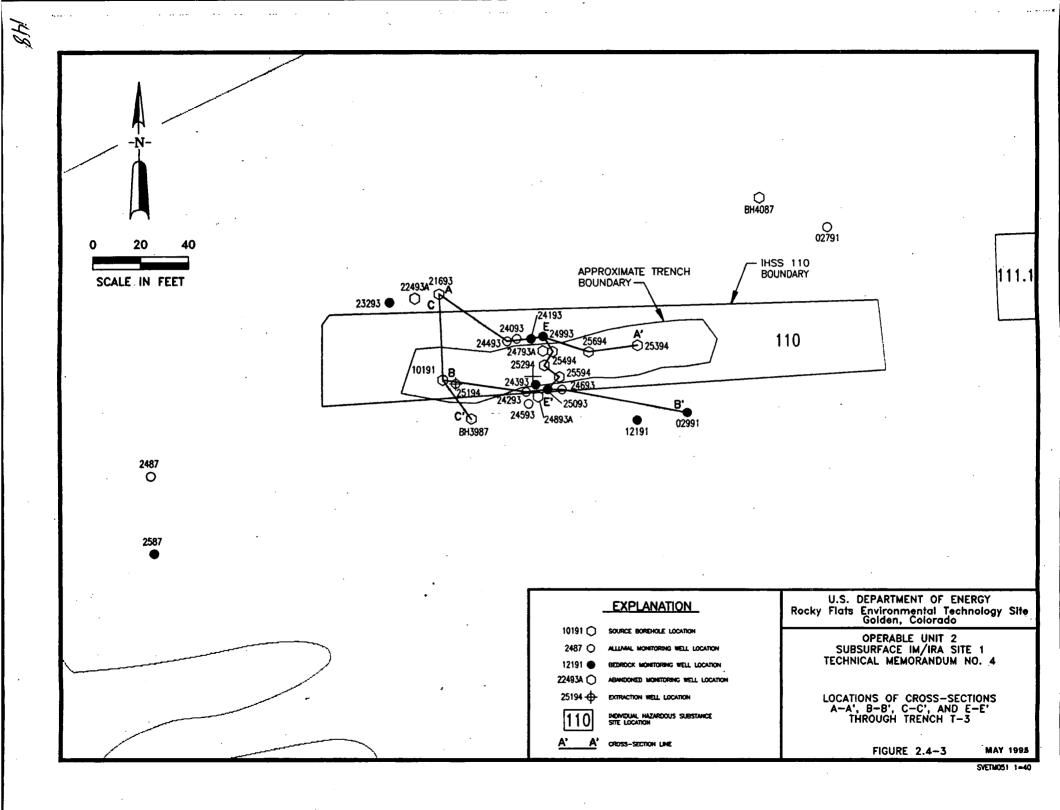
E - exceeds calibration range

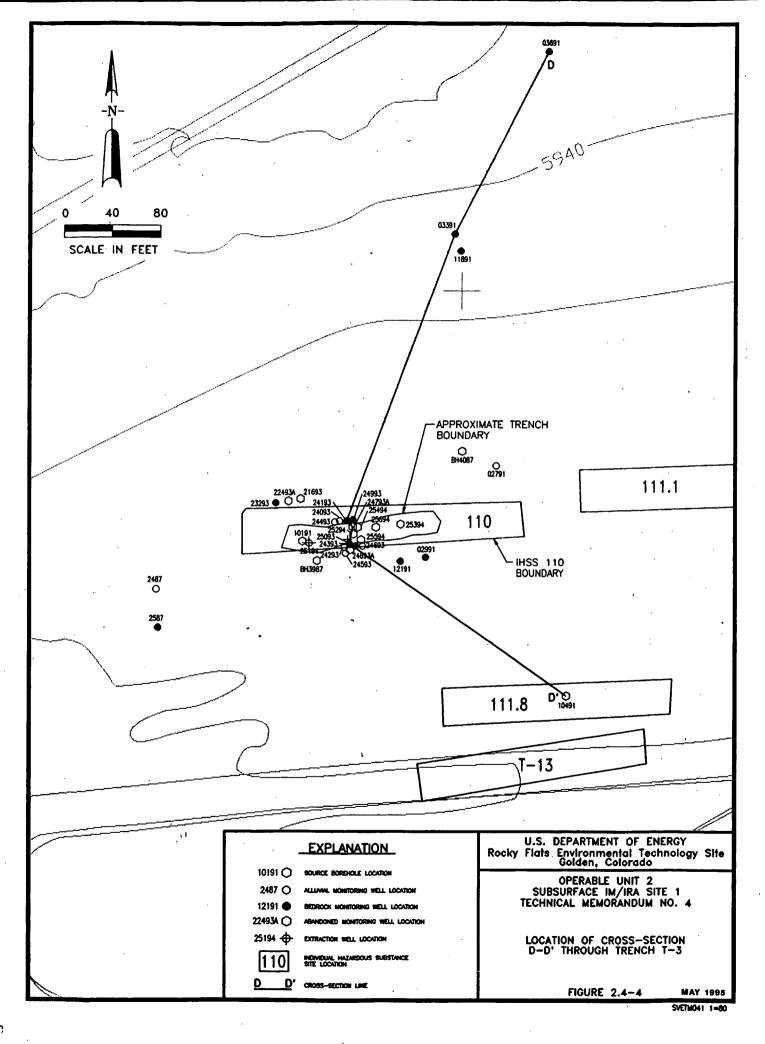
• - same phase - not biphasic

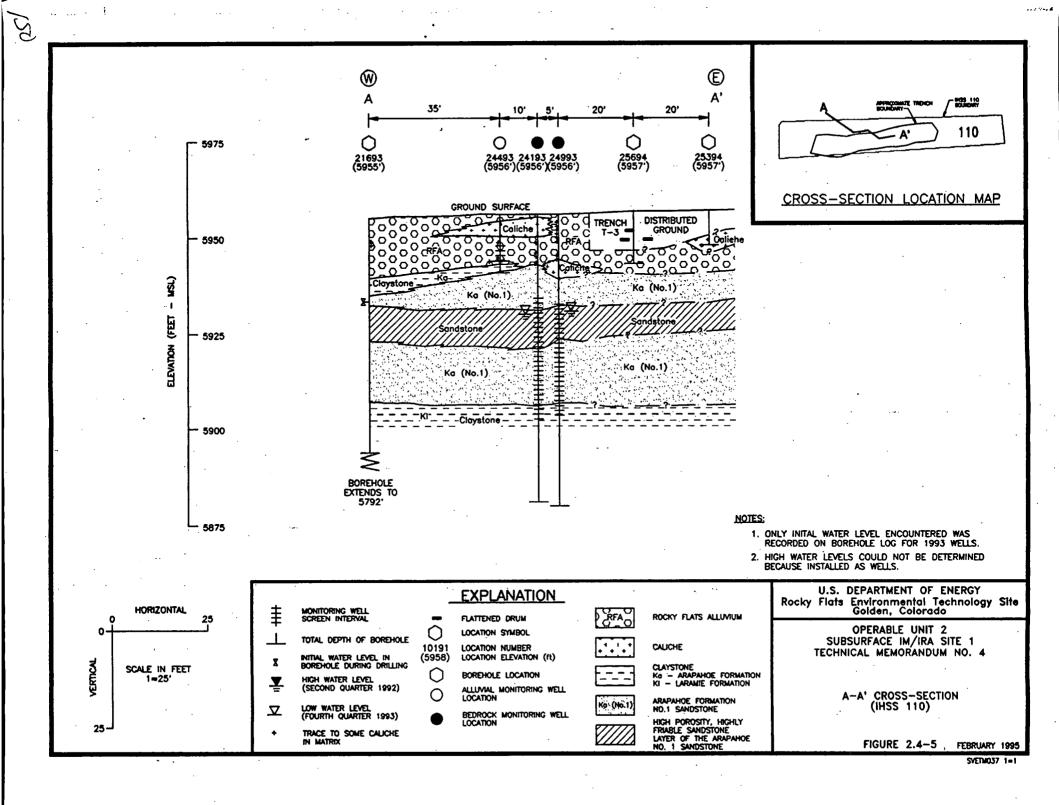
X assigned to diesel - sample contained HC throughout the range - result may be biased high

G assigned to gasoline - the sample is not gasoline or diesel, but believed to be some other HC

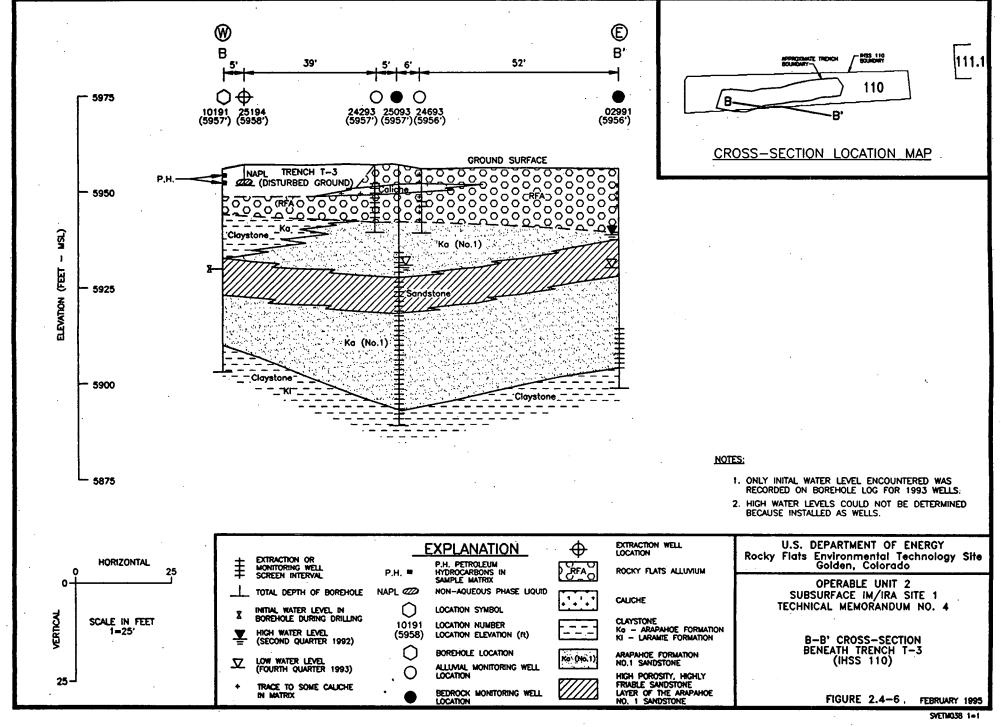




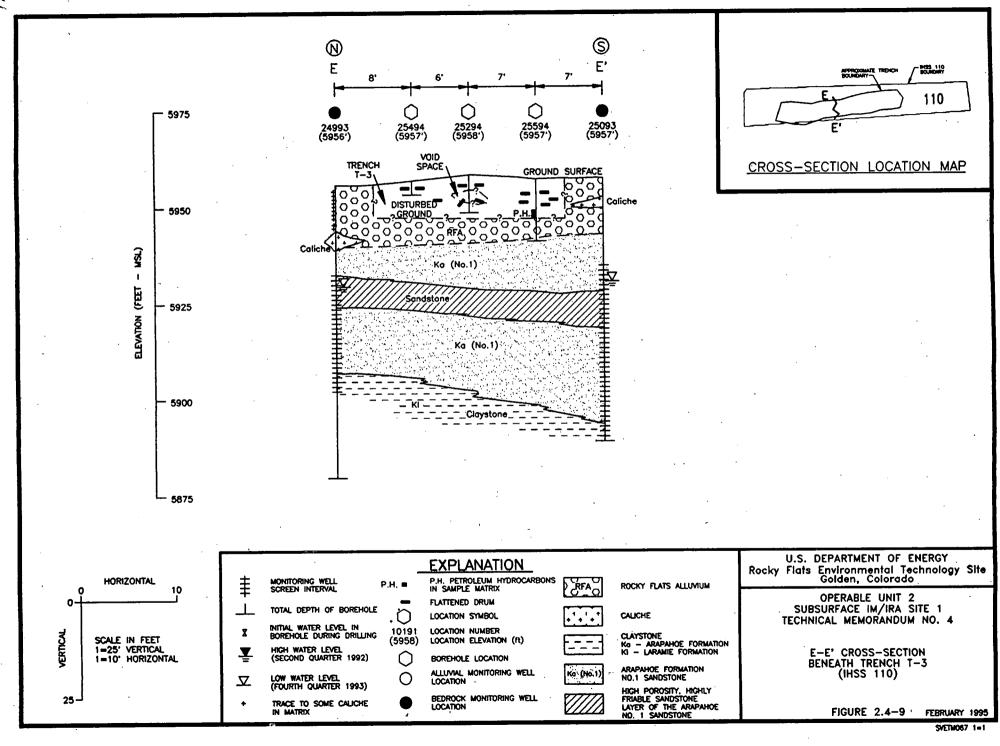




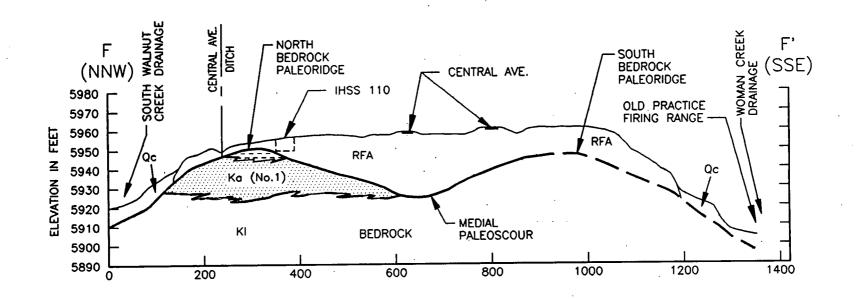


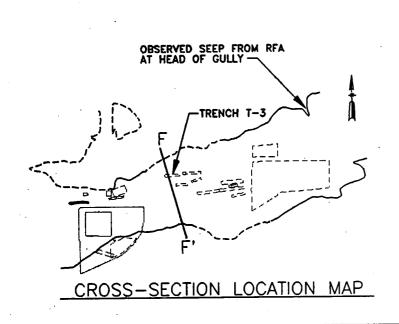


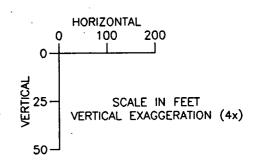
157











EXPLANATION

TOP OF BEDROCK SURFACE

Doshed Where Approximate Extrapolated

RFA ROCKY FLATS ALLUVIUM

Qc COLLUMUM

Ka (No.1) ARAPAHOE FORMATION No.1 SANDSTONE

KI LARAMIE FORMATION

U.S. DEPARTMENT OF ENERGY Rocky Flats Environmental Technology Site Golden, Colorado

OPERABLE UNIT 2
SUBSURFACE IM/IRA SITE 1
TECHNICAL MEMORANDUM NO.4

CROSS SECTION SHOWING ALLUVIAL AND BEDROCK FEATURES

FIGURE 2.4-18 F

.4-18 FEBRUARY 1995

CALIPER (INCHES)	NATURAL GAMMA * (CPS)	GENERALIZED CORE LITHOLOGY (BGS,FEET)	SHORT NORMAL RESISTIVITY (OHM METERS)	NEUTRON *	TUBE WAVE AMPLITUDE (RELATIVE)	DENSITY * (GM/CC) *
	CLAY % INCREASES TO RIGHT		0 20	APPARENT POROSITY INCREASES TO LEFT 2300 6300	150 0	1 3
3		0				
	}					
	}	10				-
	}	20CS		RACE .		}
1 =ZV		30		ARE <1800 CPS		}

LEGEND

TOP OF BEDROCK AT 15.6'

UNCONSOLIDATED SEDIMENTS

(QUATERNARY)

SANDSTONE

SILTSTONE

CLAYSTONE.

NO RECOVERY INTERVAL OR NOT SAMPLED

SCREENED INTERVAL FROM WELL 23293 PROJECTED ONTO PILOT BOREHOLE LITHOLOGIC COLUMN.

* LOG VALUES ABOVE 47' ARE ATTENUATED BY ISOLATION CASING.

EXPLANATION

BGS **BELOW GROUND SURFACE** (CPS) COUNTS PER SECOND (GM/CC) GRAMS PER CUBIC CENTIMETER

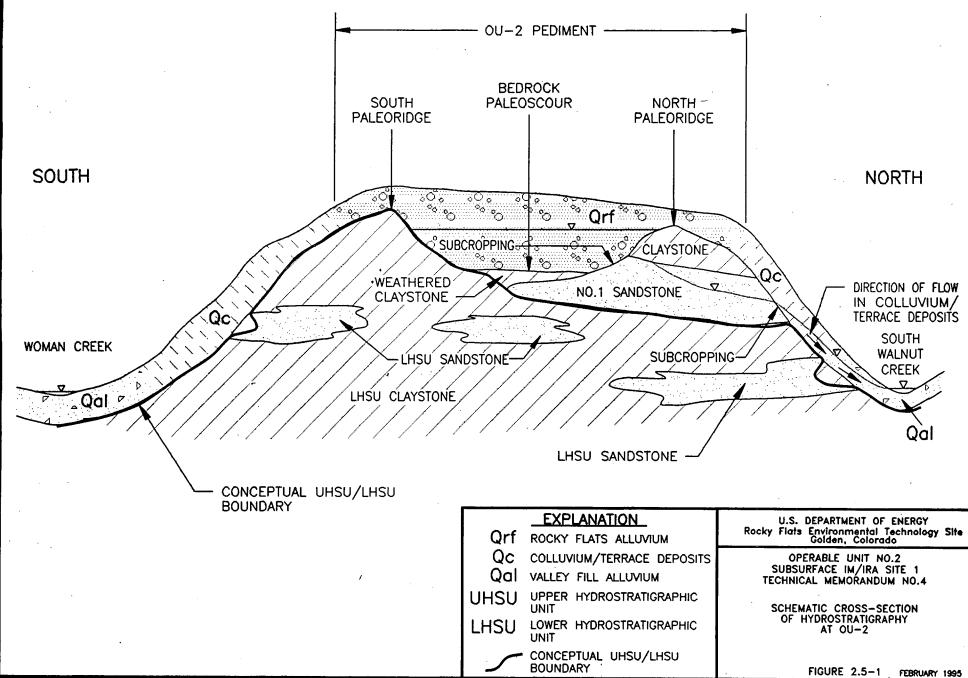
SS SANDSTONE **SLT** SILTSTONE CLAYSTONE CS

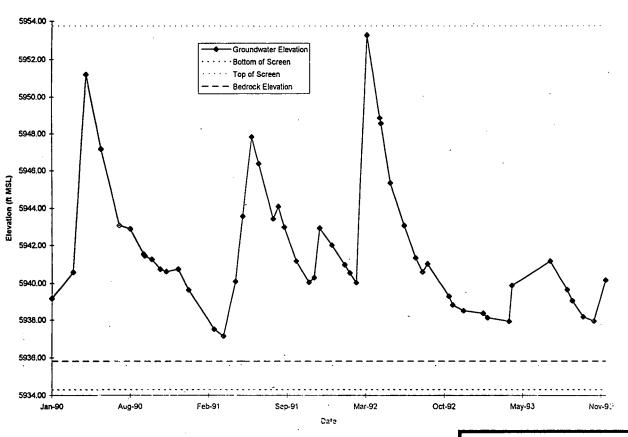
U.S. DEPARTMENT OF ENERGY Rocky Flats Environmental Technology Site Golden, Colorado

> **OPERABLE UNIT NO.2** SUBSURFACE IM/IRA SITE 1
> TECHNICAL MEMORANDUM NO. 4

GENERALIZED CORE LITHOLOGY AND GEOPHYSICAL LOGS COMPOSITE FOR PILOT BOREHOLE 21693

FIGURE 2.4-19



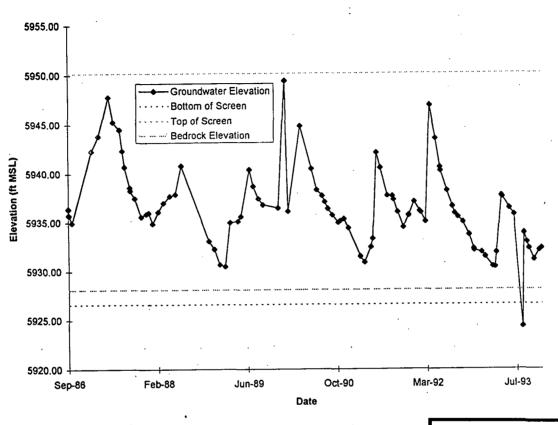


OPERABLE UNIT 2
SUBSURFACE IM/IRA SITE 1
TECHNICAL MEMORANDUM NO. 4

WELL B218789 HYDROGRAPH

FIGURE 2.5-4

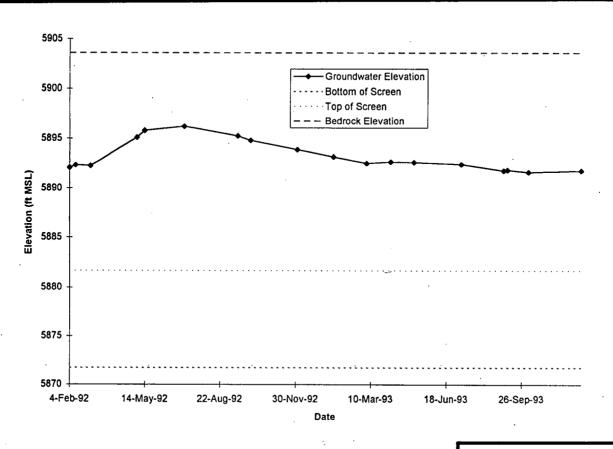




OPERABLE UNIT 2
SUBSURFACE IM/IRA SITE 1
TECHNICAL MEMORANDUM NO. 4

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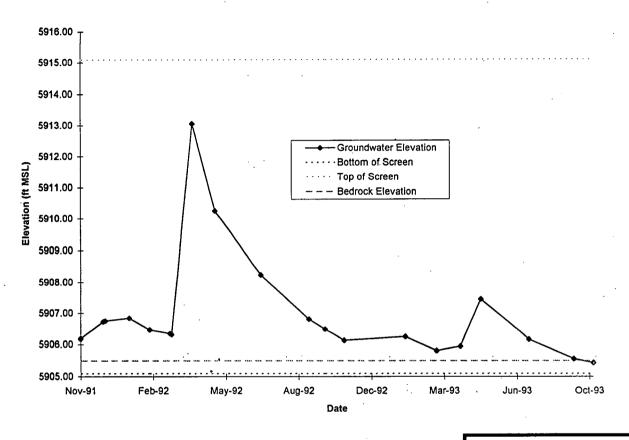
FIGURE 2.5-5



OPERABLE UNIT 2 SUBSURFACE IM/IRA SITE 1 TECHNICAL MEMORANDUM NO. 4

> WELL 12391 HYDROGRAPH

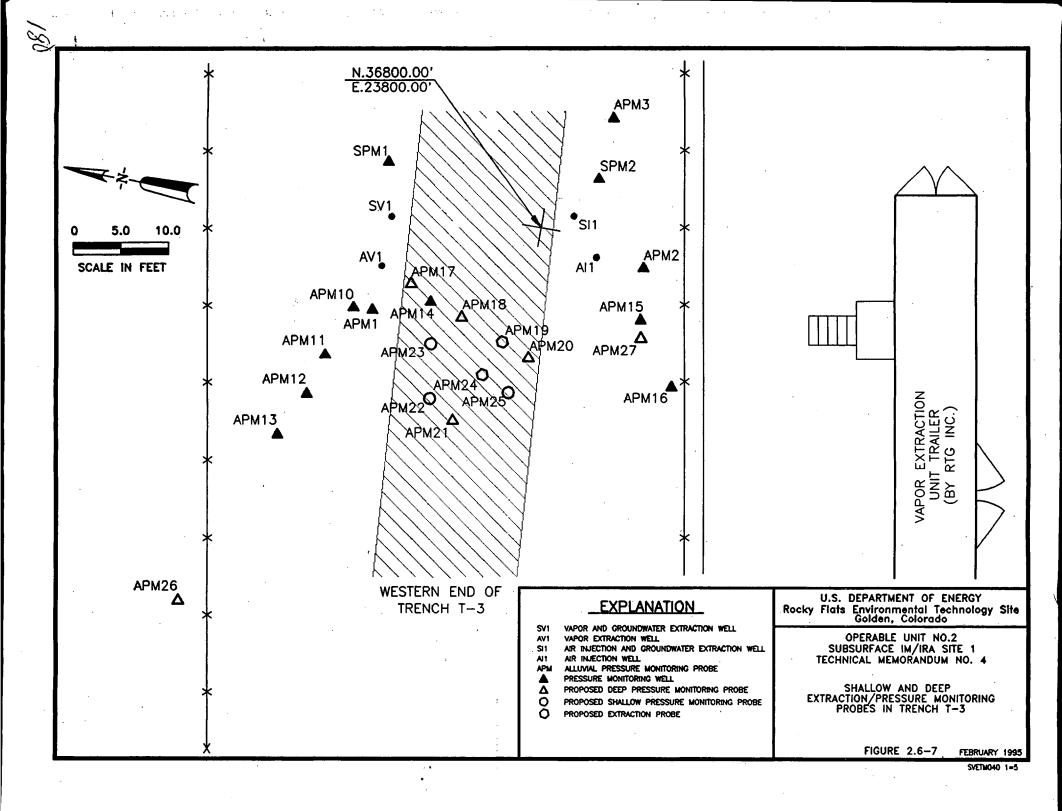
FIGURE 2.5-8

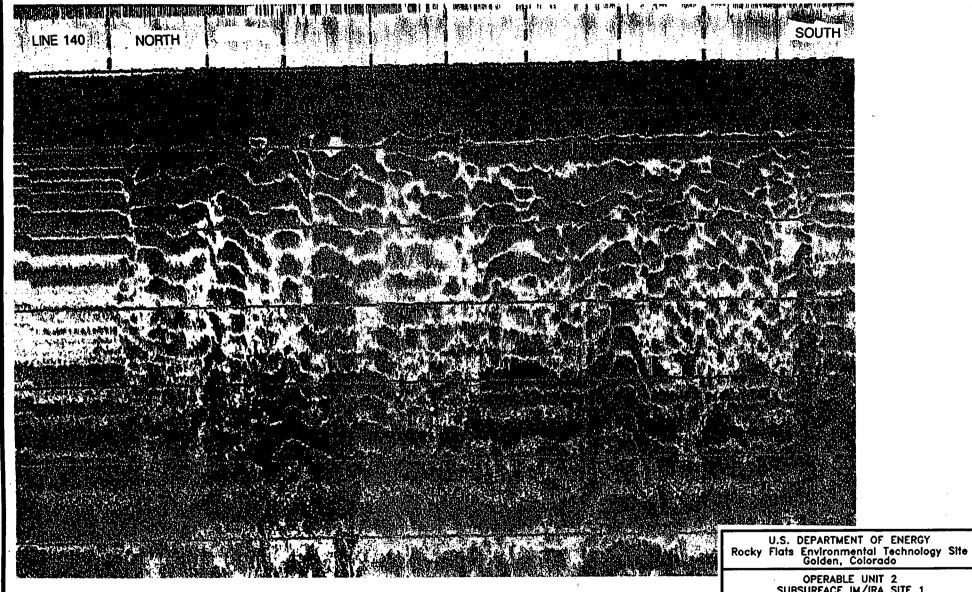


OPERABLE UNIT 2 SUBSURFACE IM/IRA SITE 1 TECHNICAL MEMORANDUM NO. 4

> WELL 05391 HYDROGRAPH

FIGURE 2.5-9

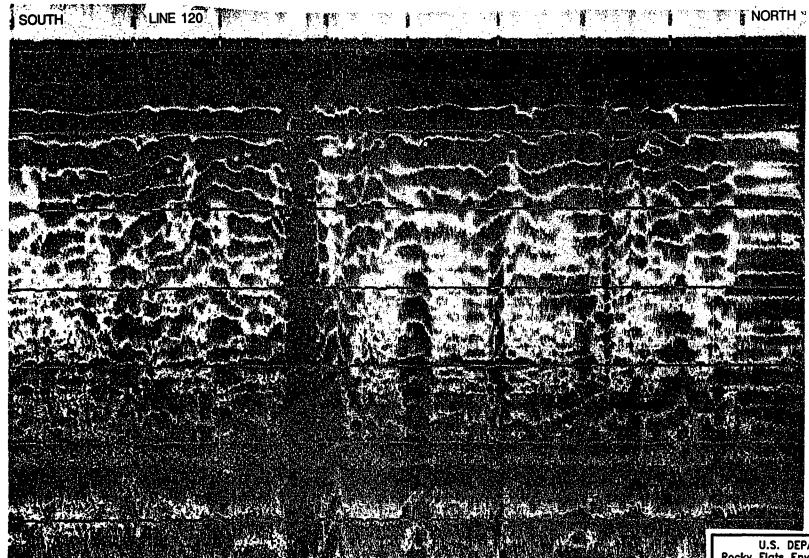




OPERABLE UNIT 2 SUBSURFACE IM/IRA SITE 1 TECHNICAL MEMORANDUM NO. 4

SAMPLE GROUND PENETRATING RADAR RAW DATA LINE 140

FIGURE 2.7-5



ROCKS AT GROUND

SURFACE -

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OPERABLE UNIT 2 SUBSURFACE IM/IRA SITE 1 TECHNICAL MEMORANDUM NO. 4

SAMPLE GROUND PENETRATING RADAR RAW DATA LINE 120

FIGURE 2.7-6

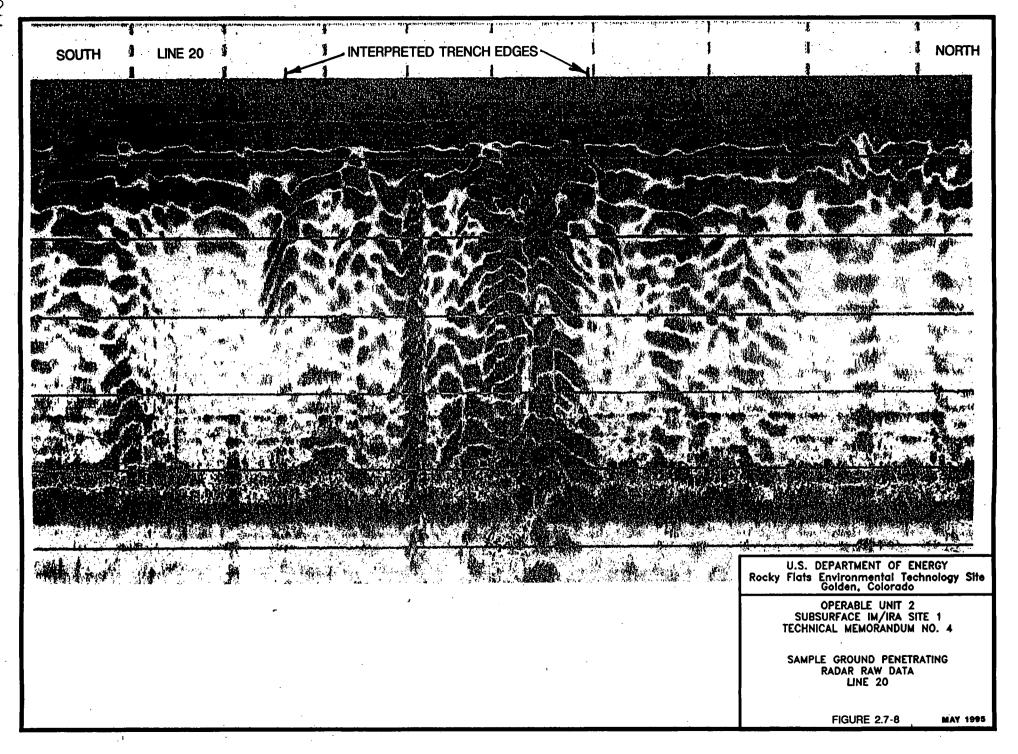
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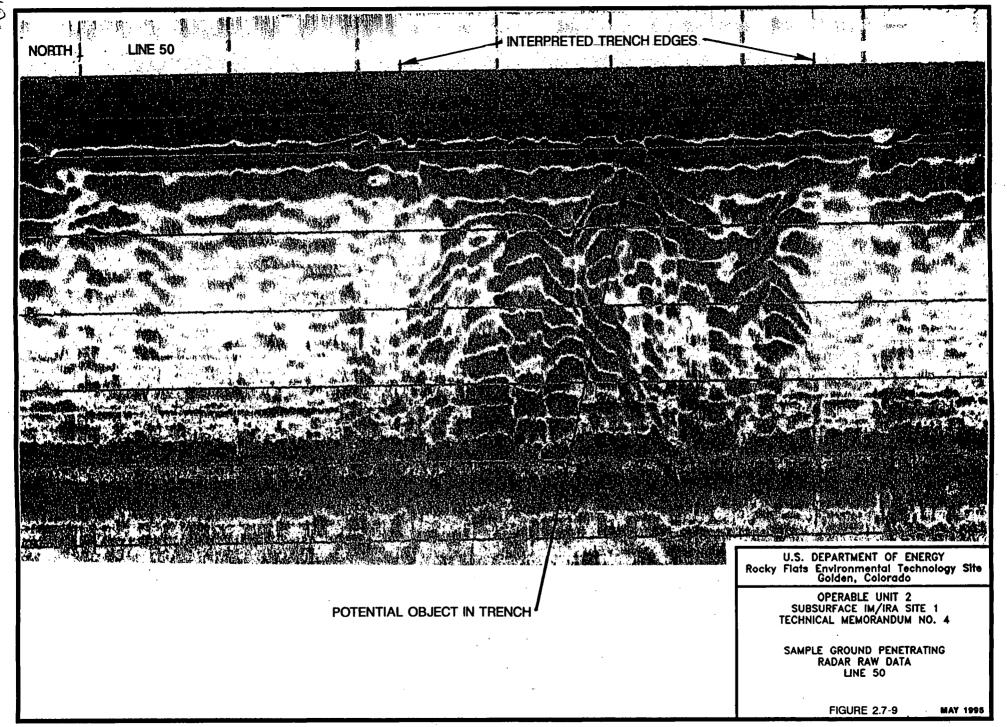
LNEO NORTH INTERPRETED TRENCH EDGES U.S. DEPARTMENT OF ENERGY Rocky Flats Environmental Technology Golden, Colorado SOUTH OPERABLE UNIT 2
SUBSURFACE IM/IRA SITE 1
TECHNICAL MEMORANDUM NO. SAMPLE GROUND PENETRATING
RADAR RAW DATA
LINE 0

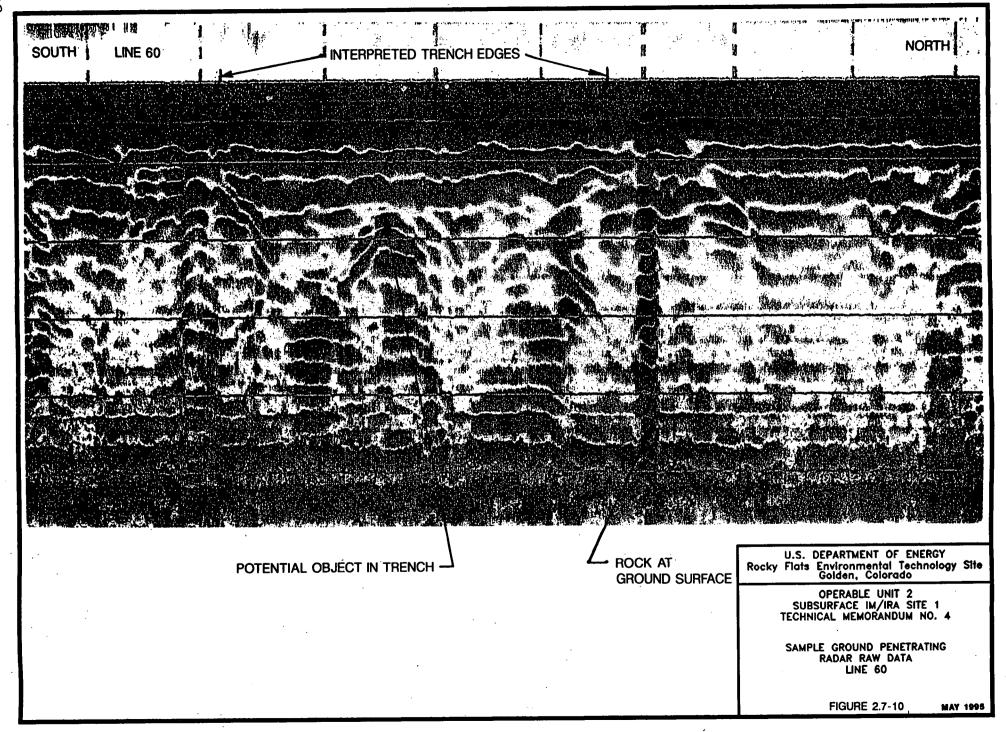
FIGURE 2.7-7

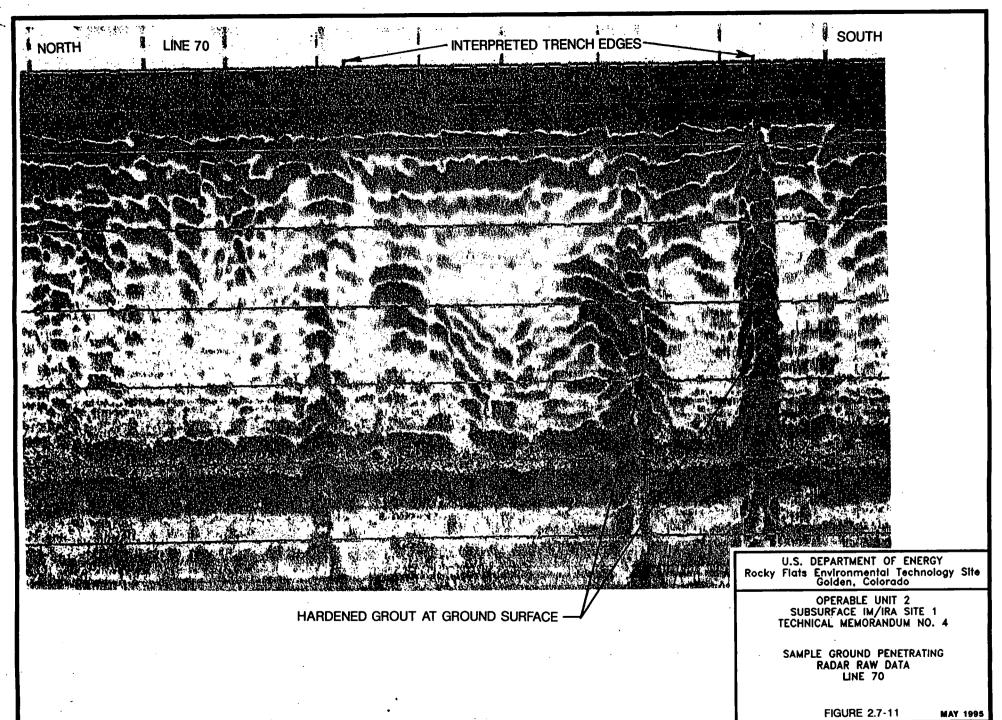
MAY 1995

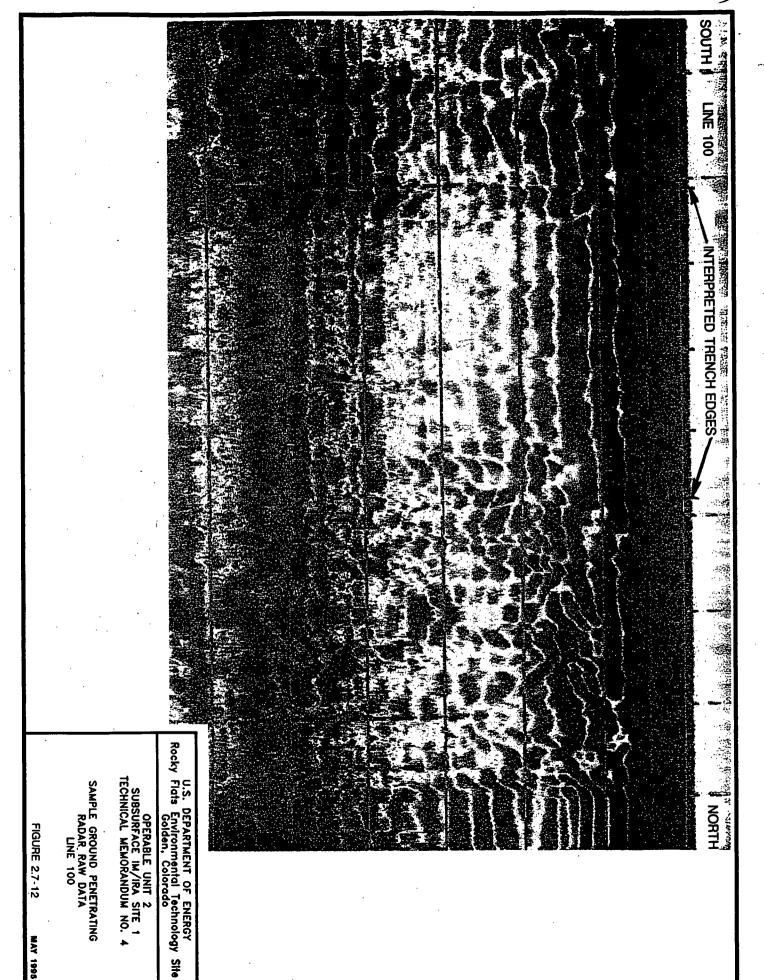
SHe



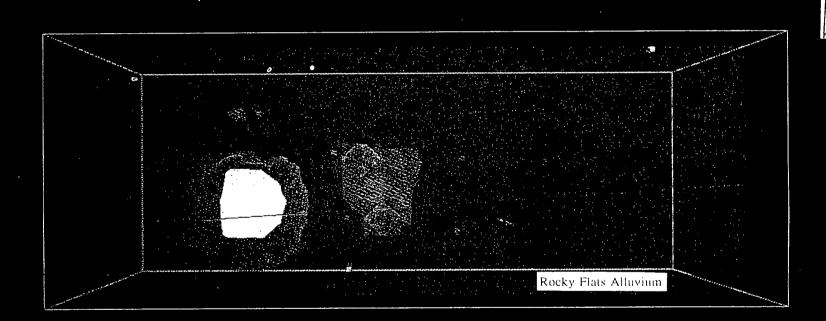








Rocky Flats IHSS 110 Geology and VOC Concentrations

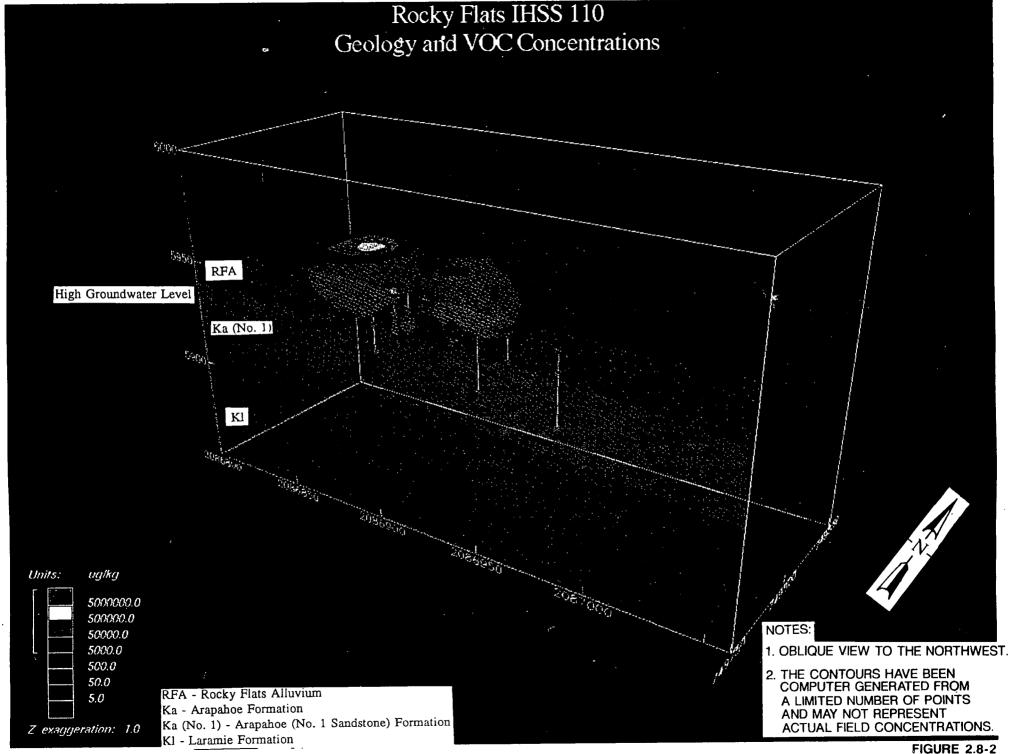


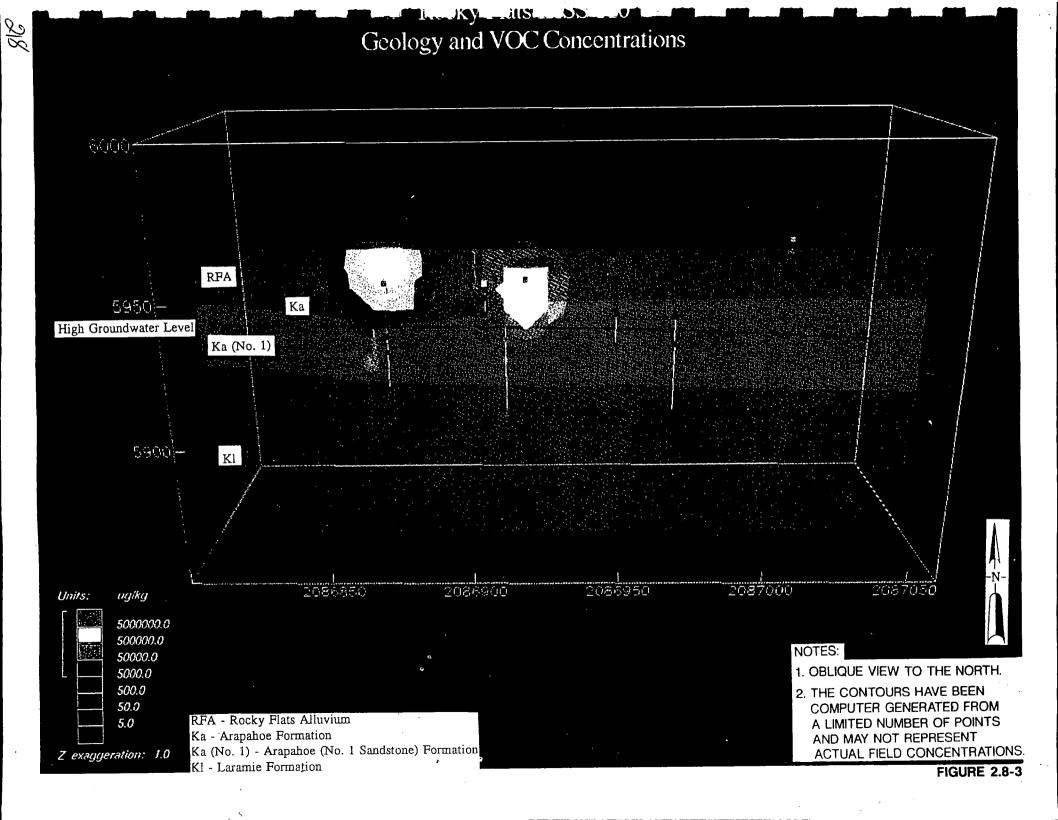
Units: ugikg 5000000.0 500000.0 50000.0 5000.0 500.0 50.0 5.0

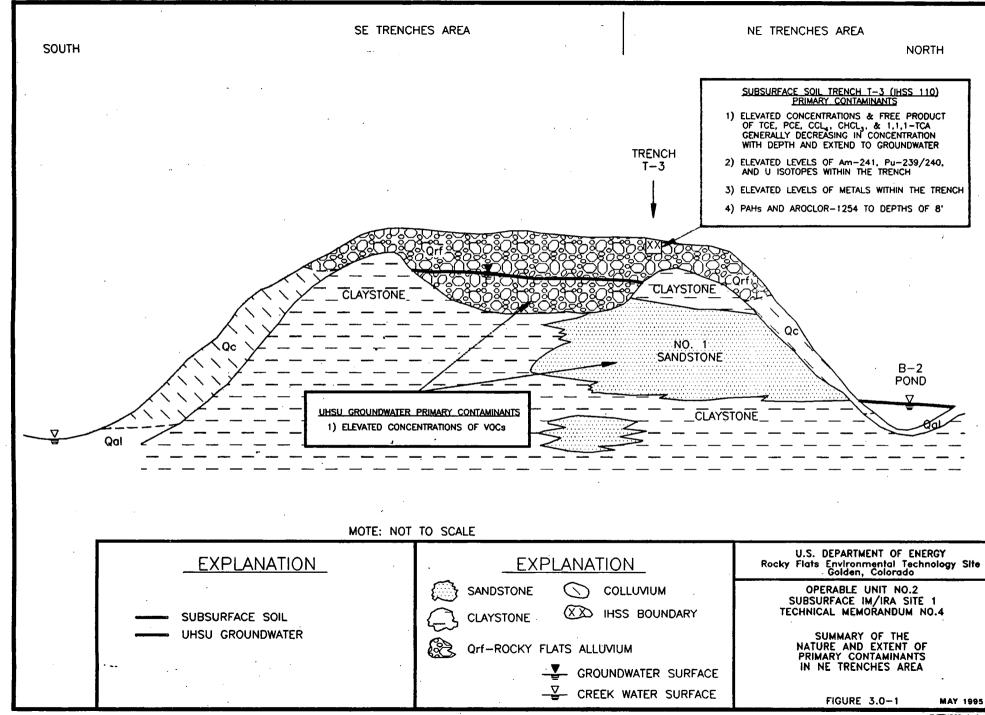
Z exaggeration: 1.0

NOTE:

THE CONTOURS HAVE BEEN COMPUTER GENERATED FROM A LIMITED NUMBER OF POINTS AND MAY NOT REPRESENT ACTUAL FIELD CONCENTRATIONS







THIS TARGET SHEET REPRESENTS AN OVER-SIZED MAP / PLATE FOR THIS DOCUMENT: (Ref: N/A)

Final

Technical Memorandum No. 4
Site Model of Hydrogeologic/
Contamination Distribution
for Trench T-3; IHSS 110: OU-2
OU02 Subsurface IM/IRA
Soil Vapor Extraction Pilot Test
Site No. 1

Volume 1 Text and Figures

May 1995

Plate 2.5-1:

Ou-2 Seep Locations and Geologic Features

May 1995

CERCLA Administrative Record Document, BZ-A-000690

U.S. DEPARTEMENT OF ENERGY ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

GOLDEN, COLORADO

THIS TARGET SHEET REPRESENTS AN OVER-SIZED MAP / PLATE FOR THIS DOCUMENT: (Ref: N/A)

Final

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Volume 1 Text and Figures

May 1995

Plate 2.5-1:

Ou-2 Seep Locations and Geologic Features

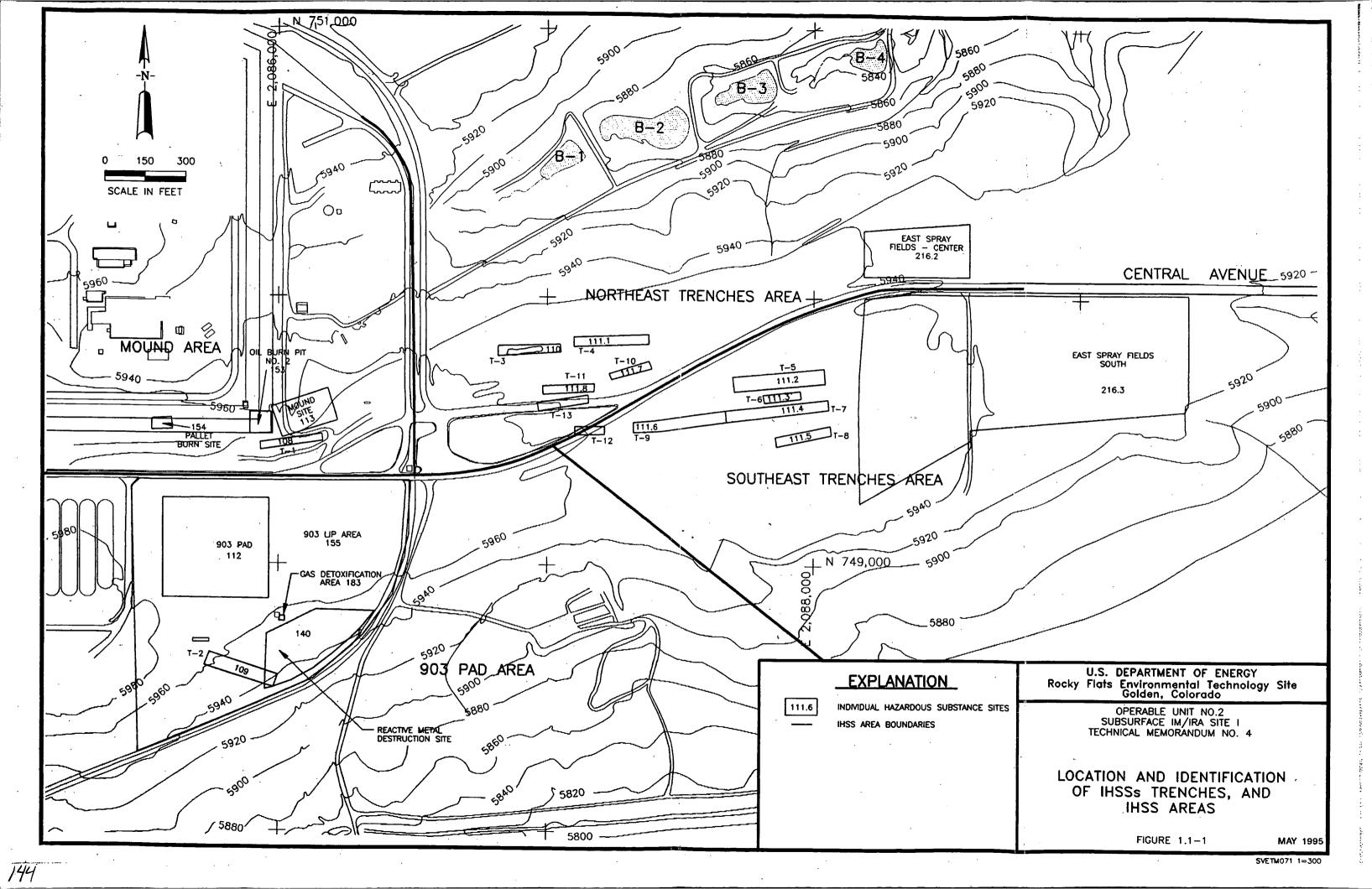
May 1995

CERCLA Administrative Record Document, BZ-A-000690

U.S. DEPARTEMENT OF ENERGY ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

GOLDEN, COLORADO

222/222

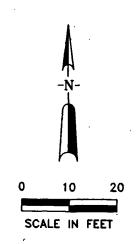




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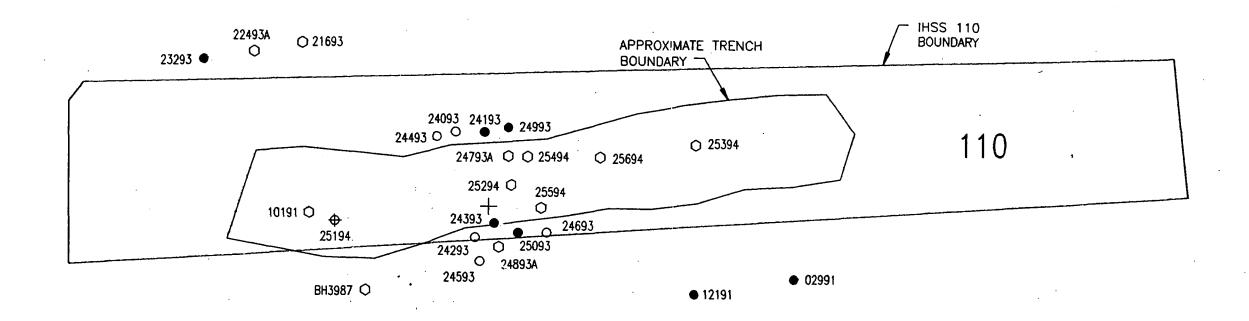
LIQUID COLLECTED FROM BOREHOLE 25194

FIGURE 2.2-1



вн4087 ф

02791 O



<u>EXPLANATION</u>

10191 O SOURCE BOREHOLE LOCATION

2487 ALLIMAL MONITORING WELL LOCATION

12191 ● BEDROCK MONITORING WELL LOCATION

22493A ○ ABANDONED MONITORING WELL LOCATION

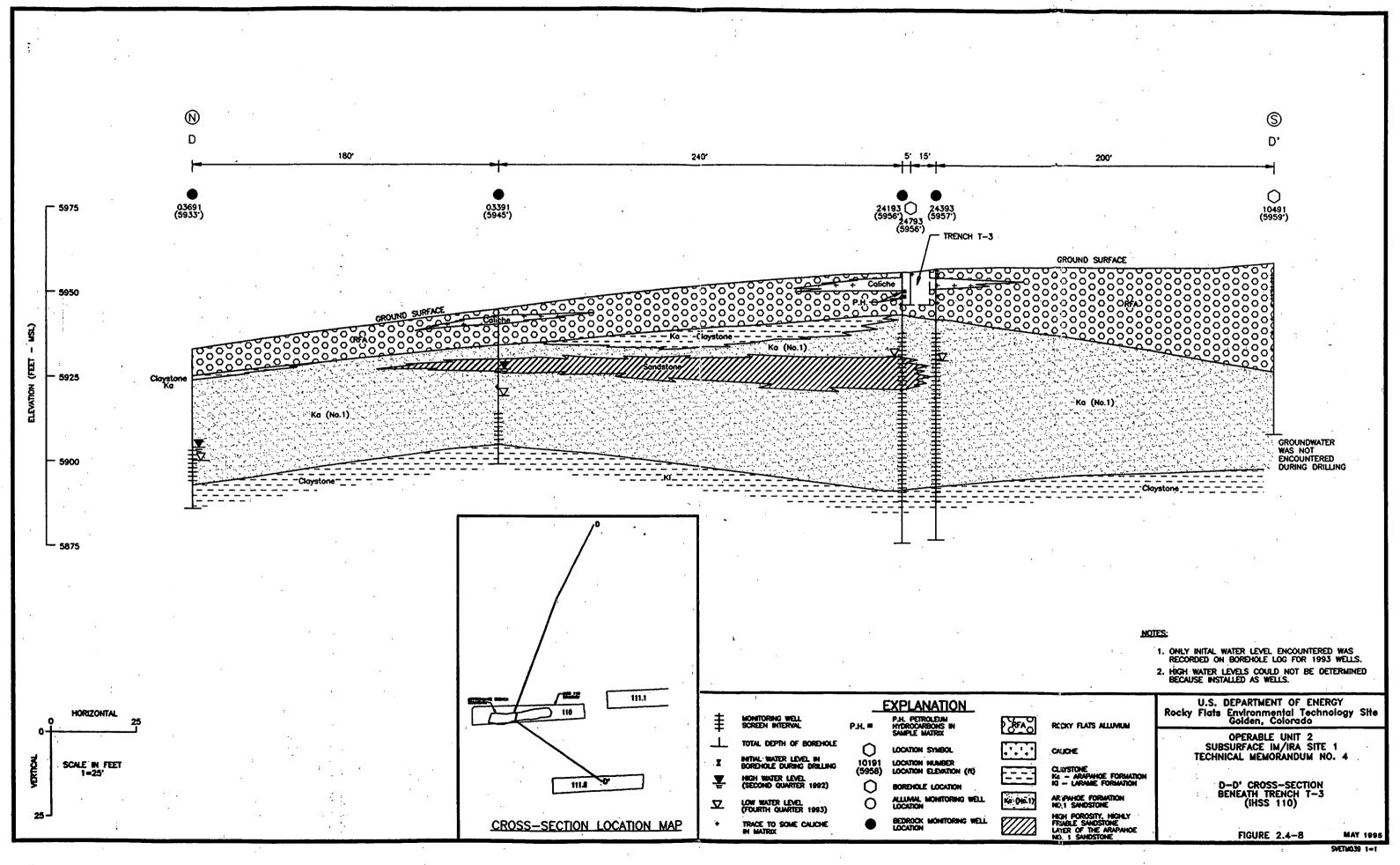
indmidual hazardous substance site location

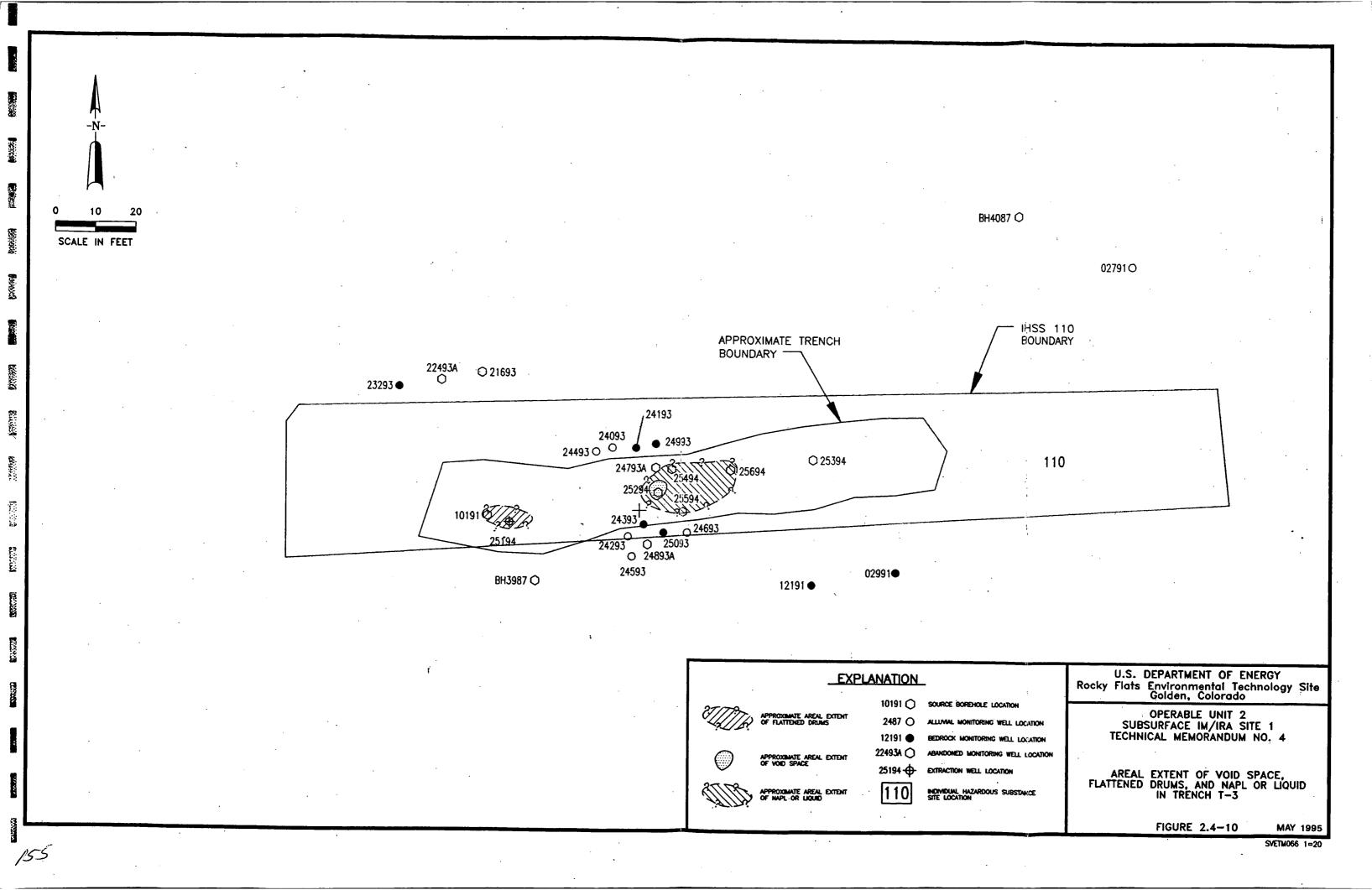
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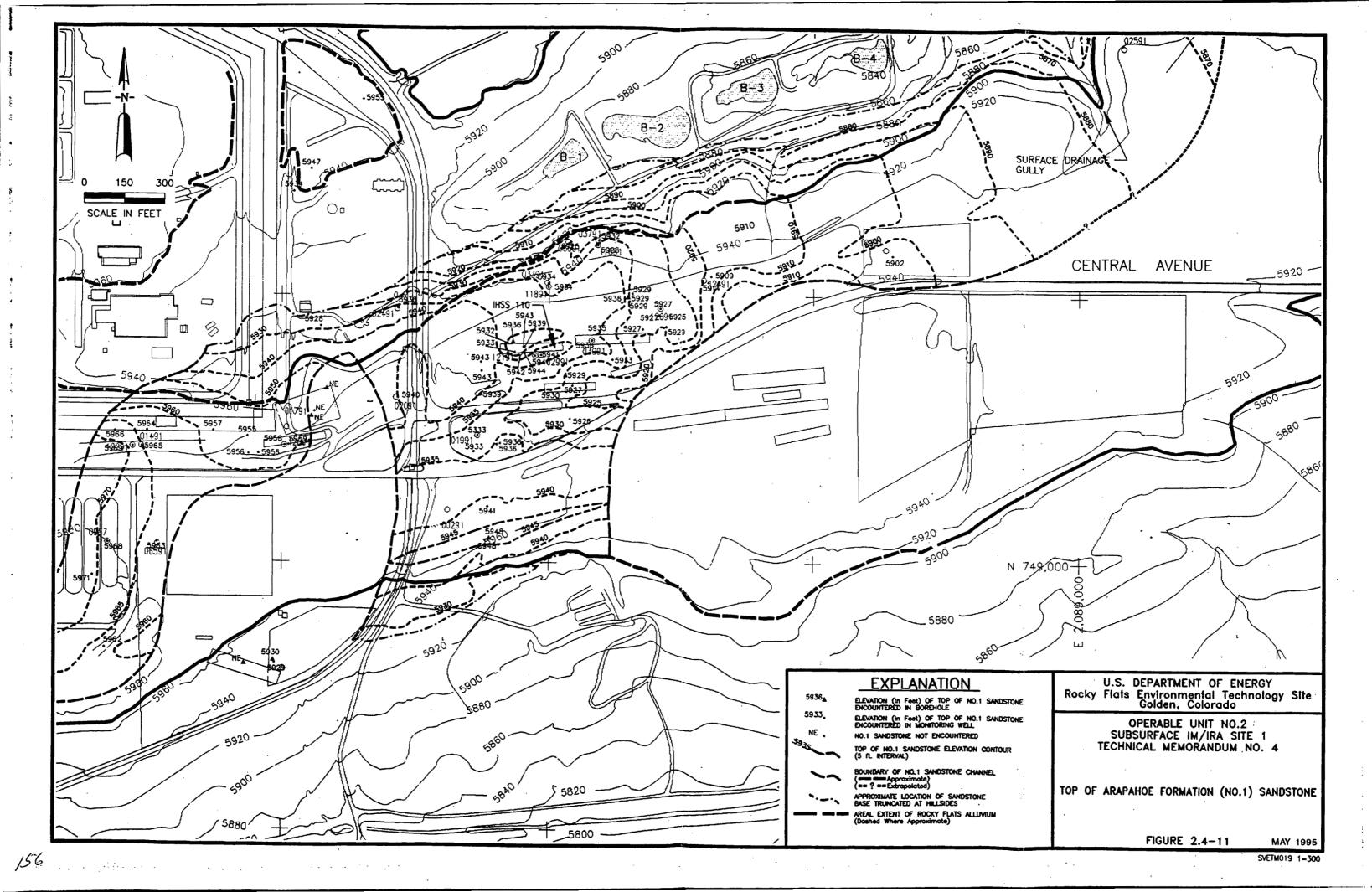
OPERABLE UNIT 2
SUBSURFACE IM/IRA SITE 1
TECHNICAL MEMORANDUM NO. 4

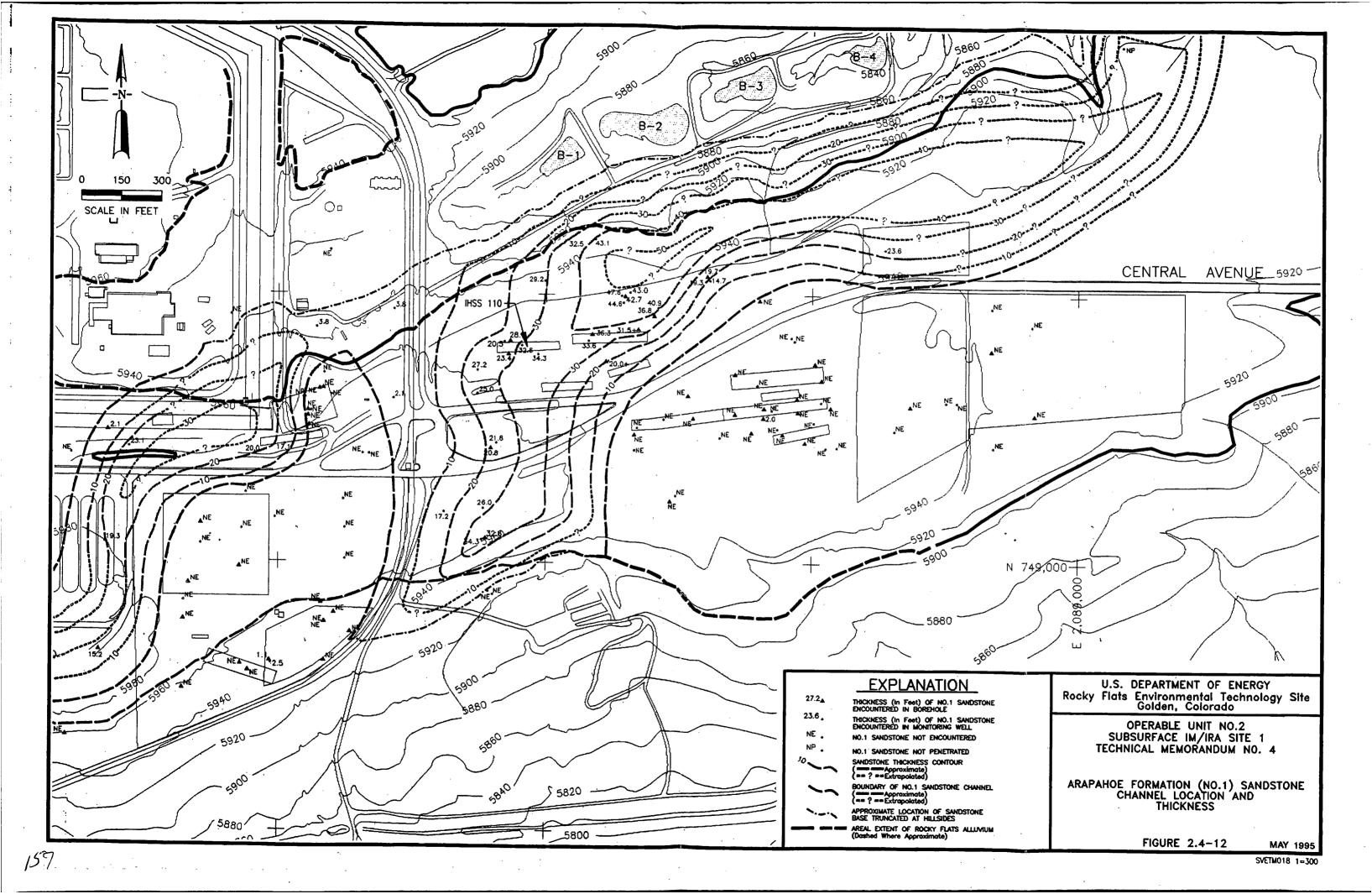
BOREHOLE AND MONITORING WELL LOCATIONS IN THE VICINITY OF TRENCH T-3

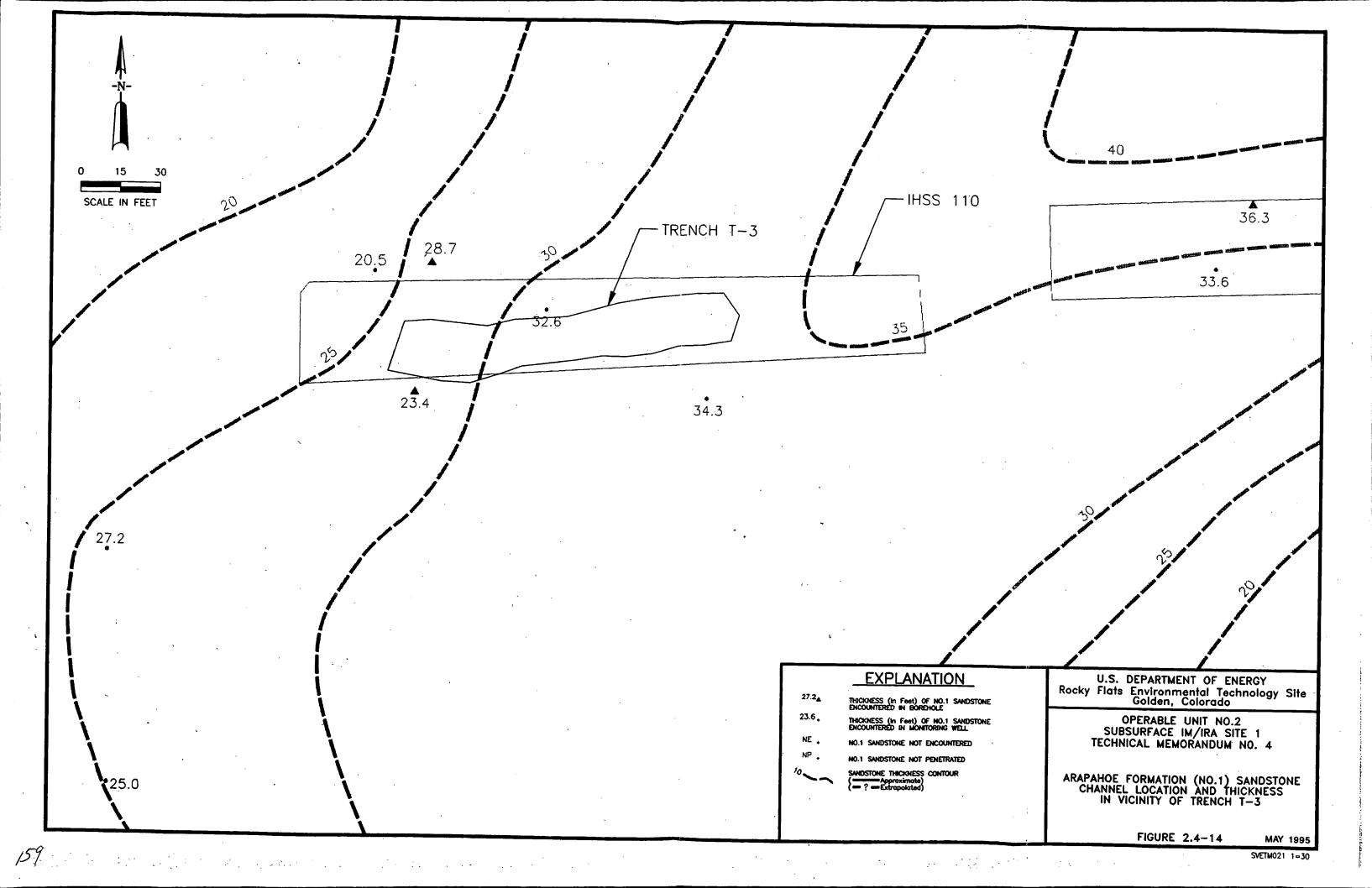
FIGURE 2.4-1

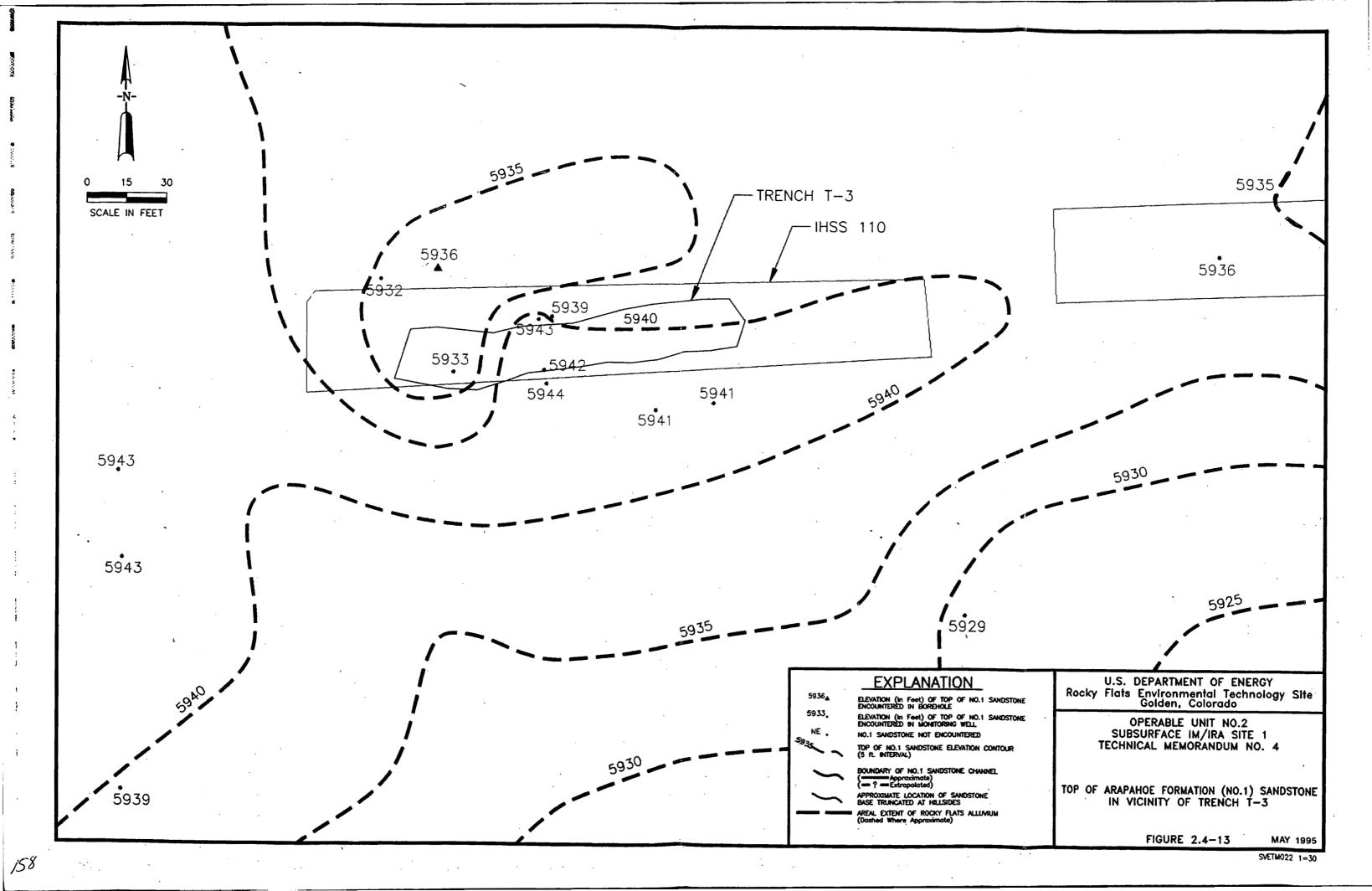


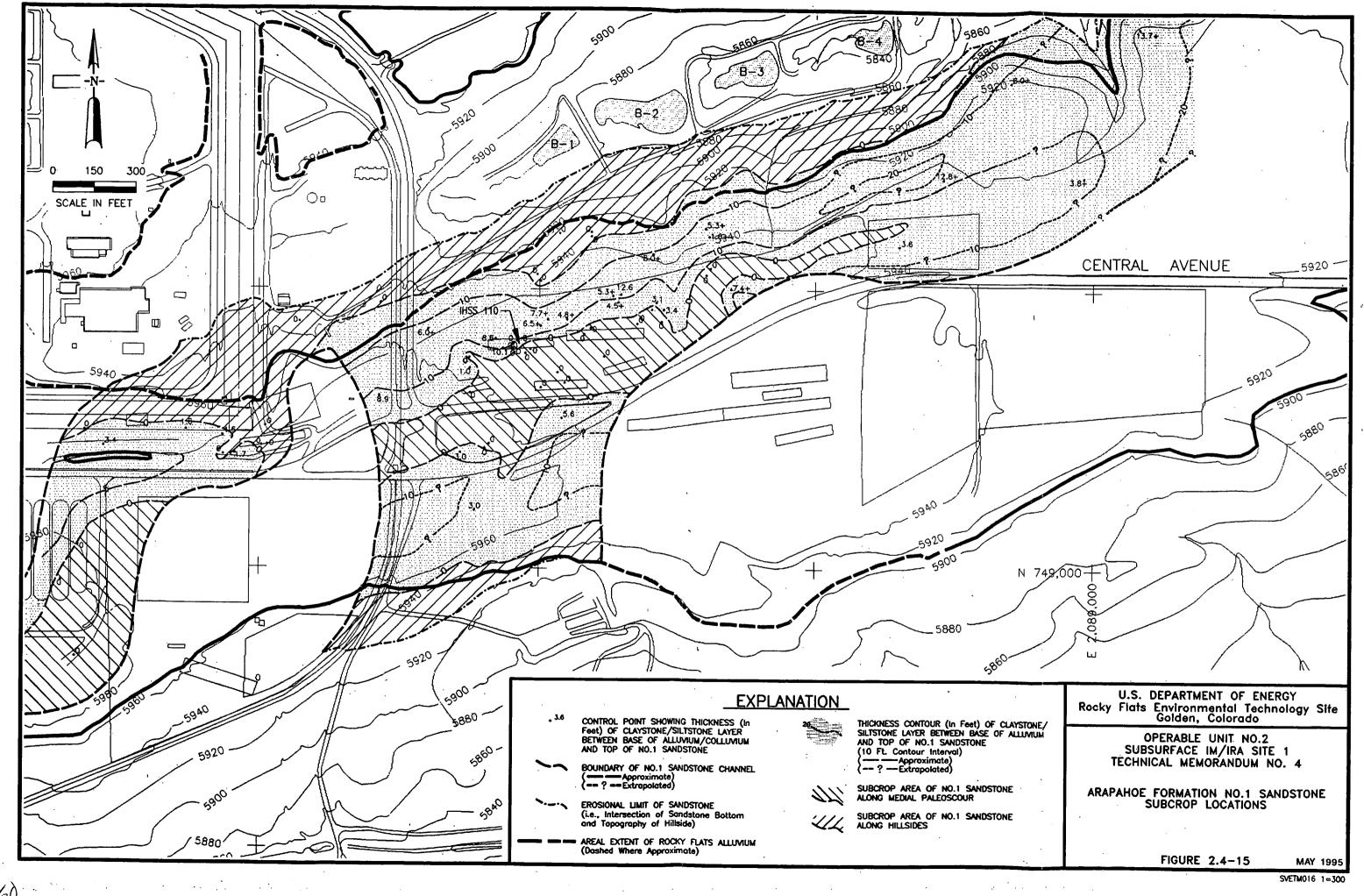


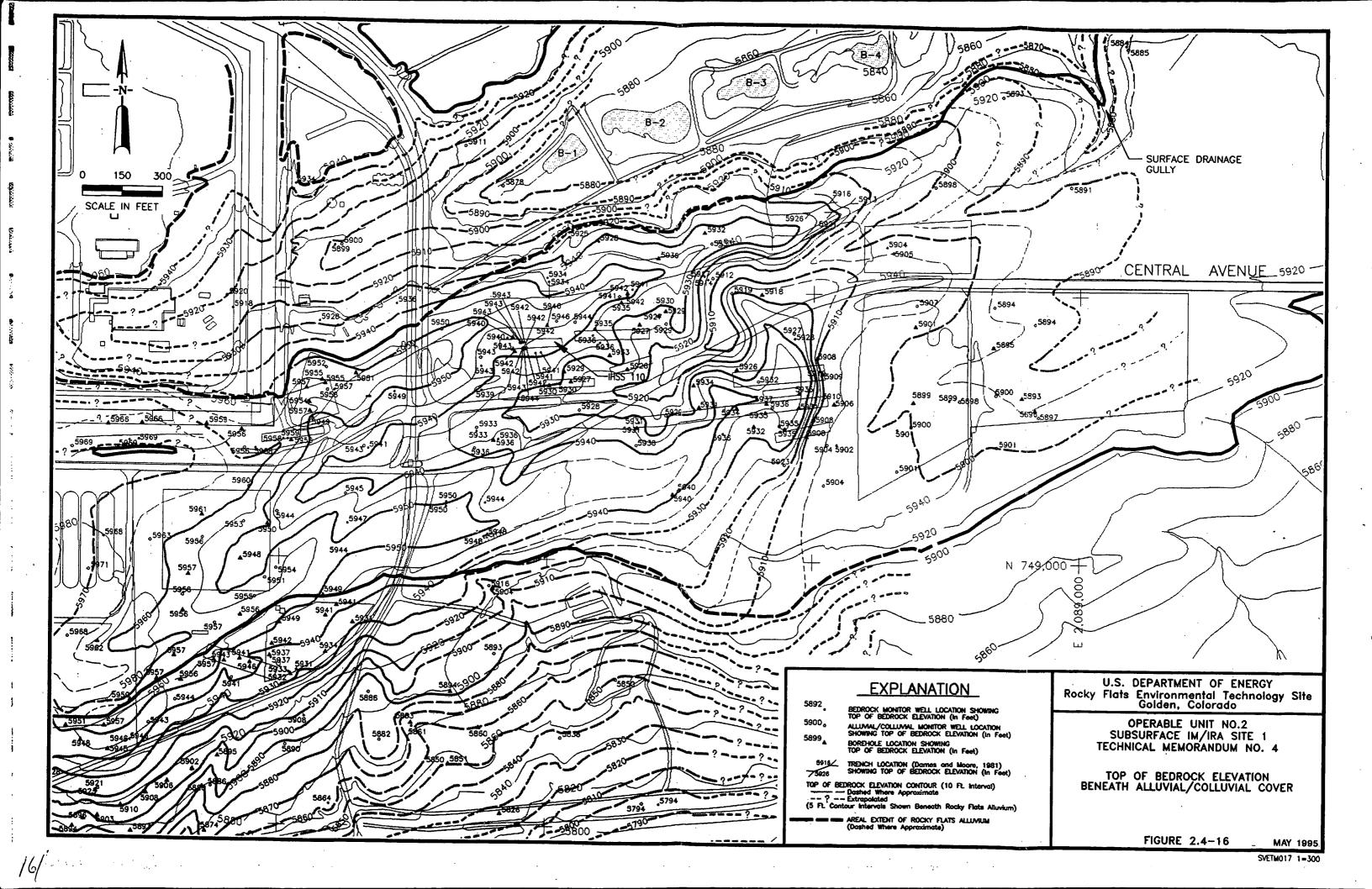


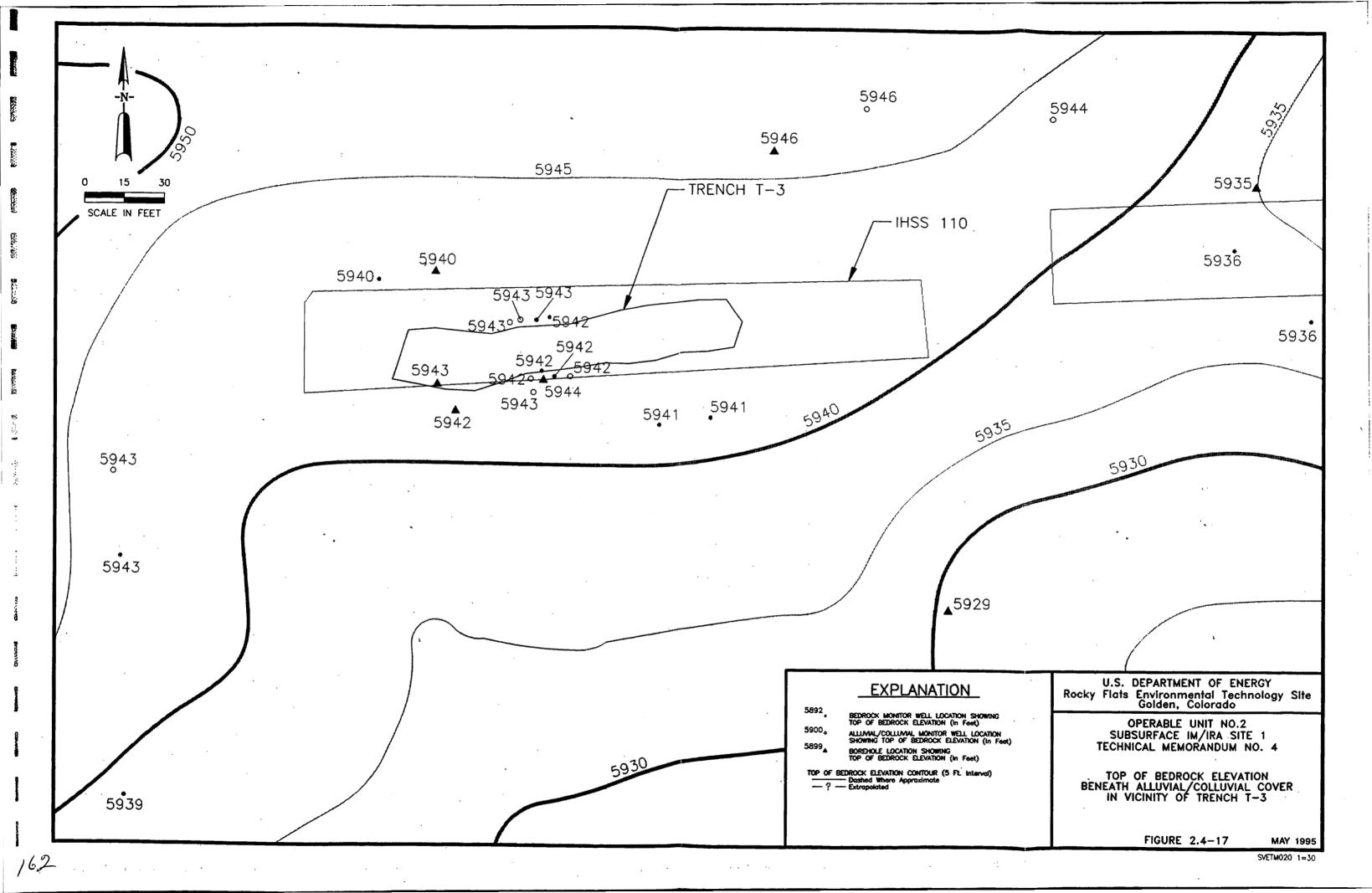


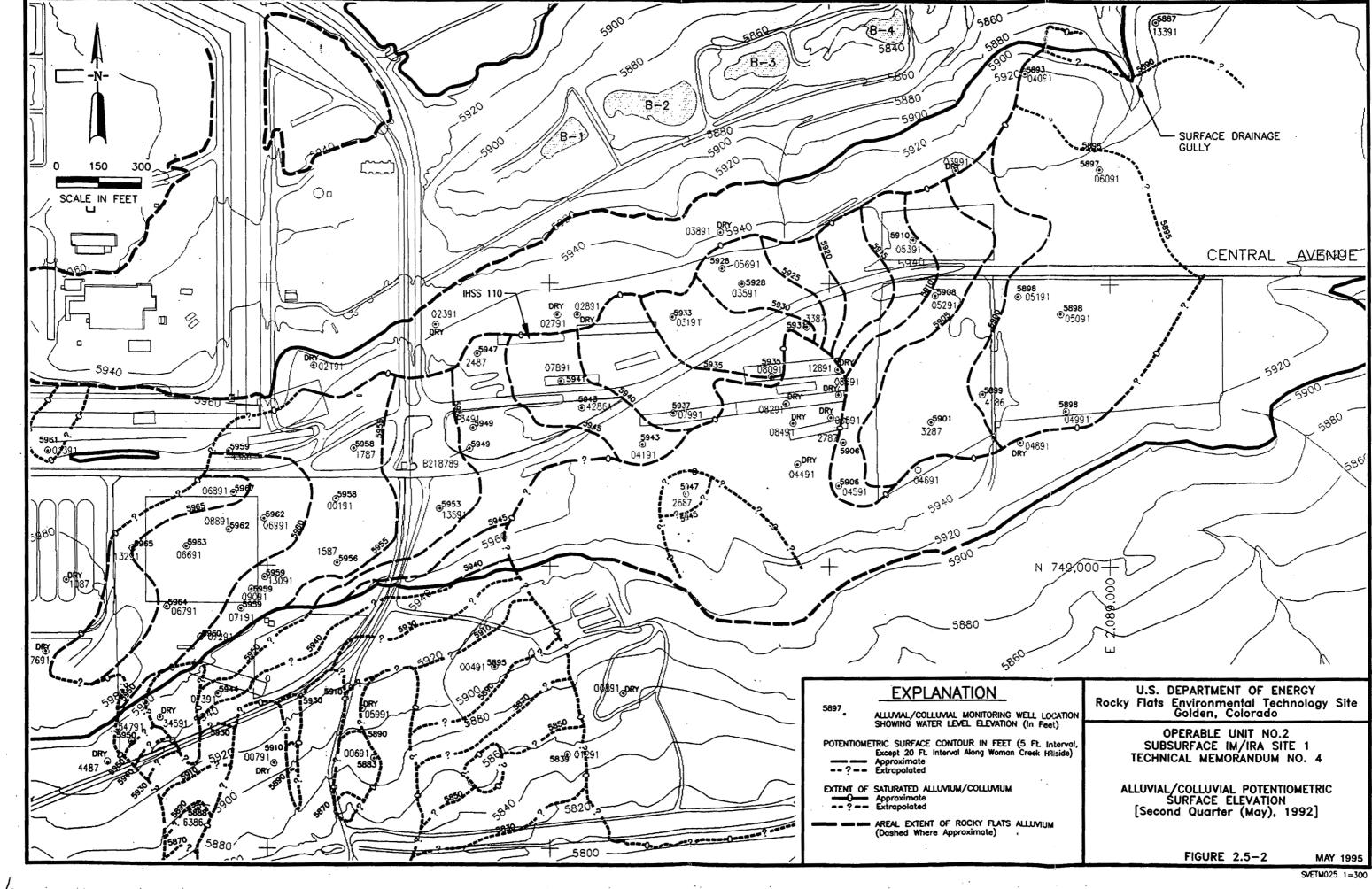


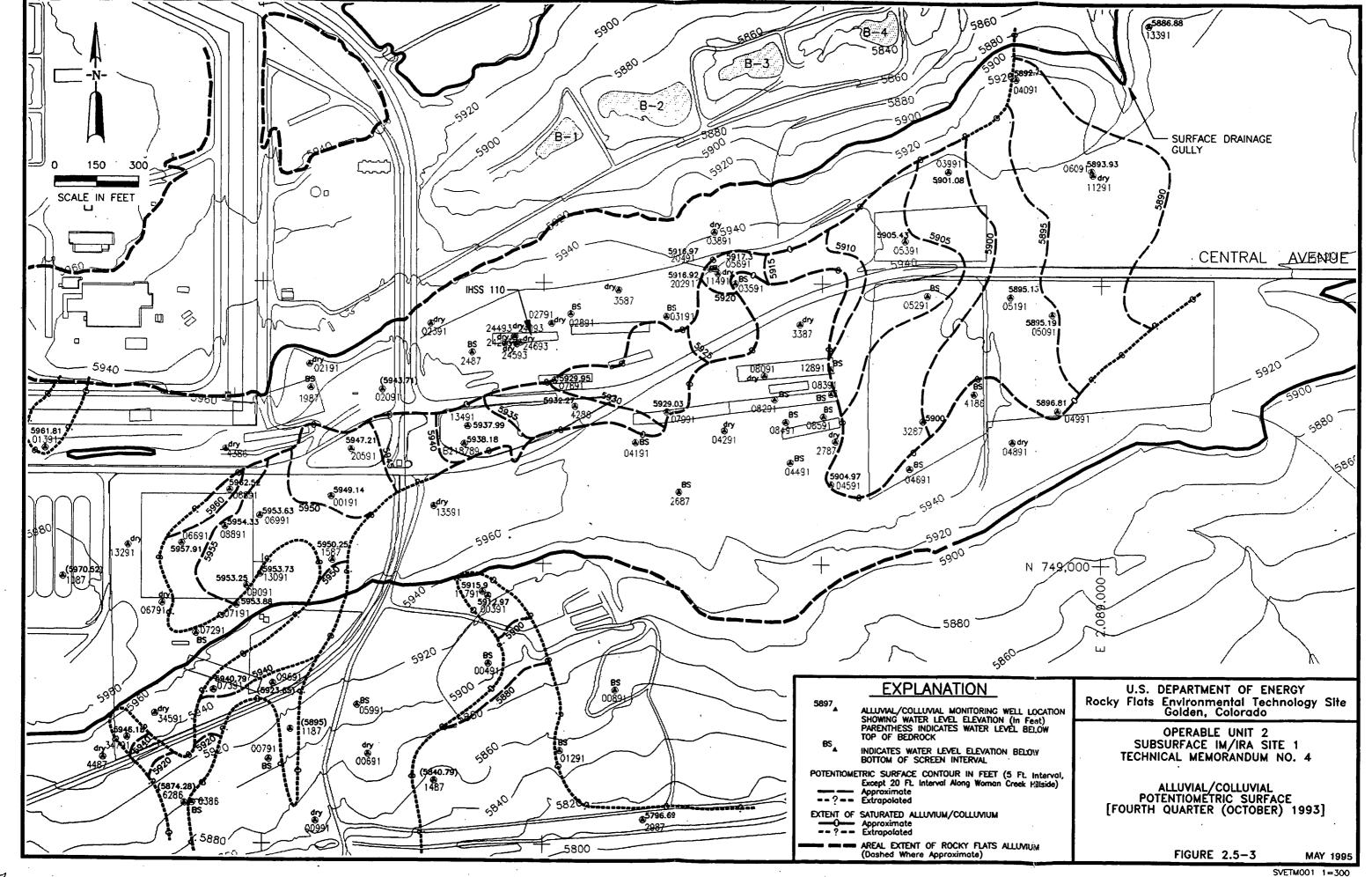




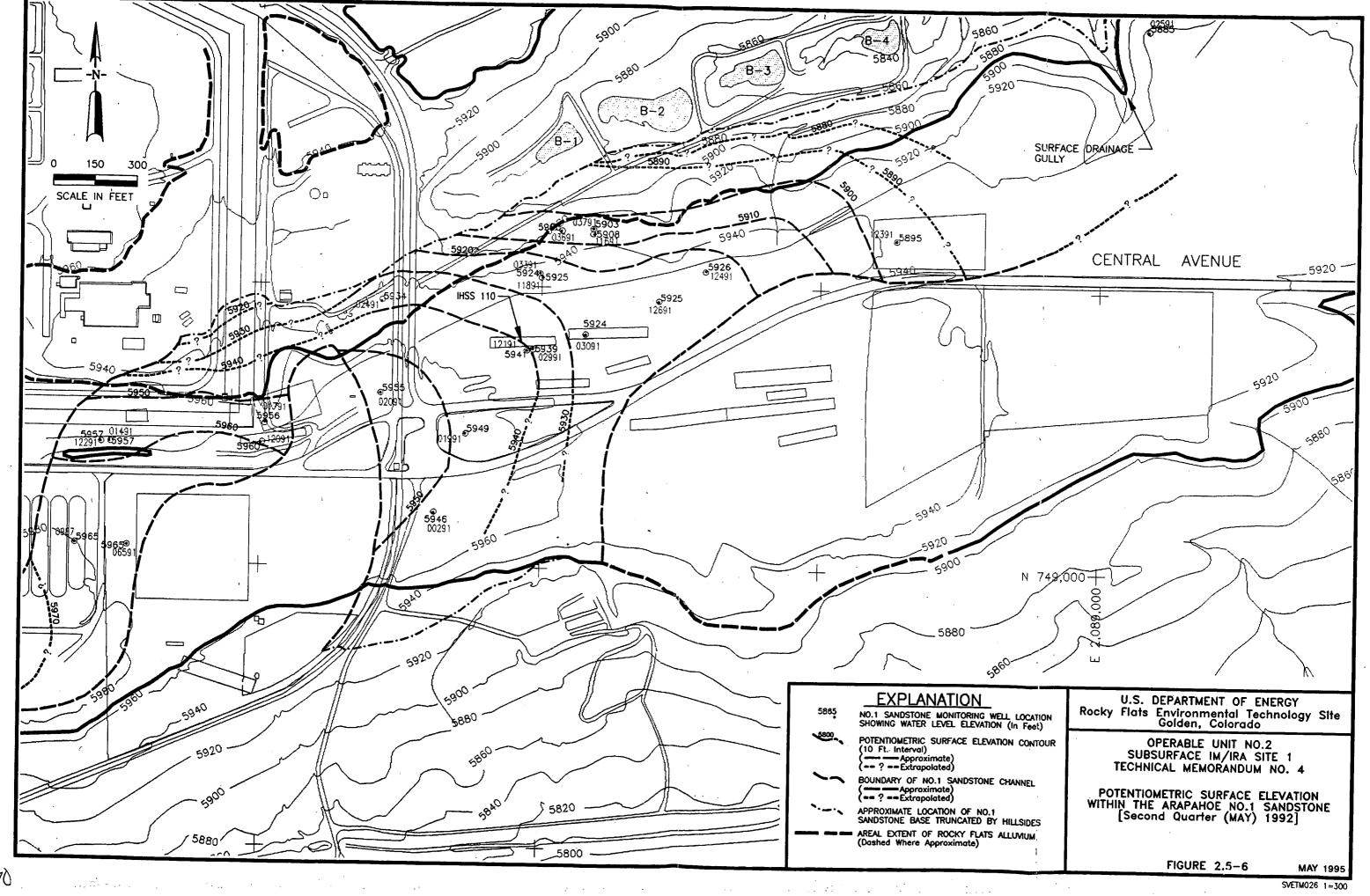


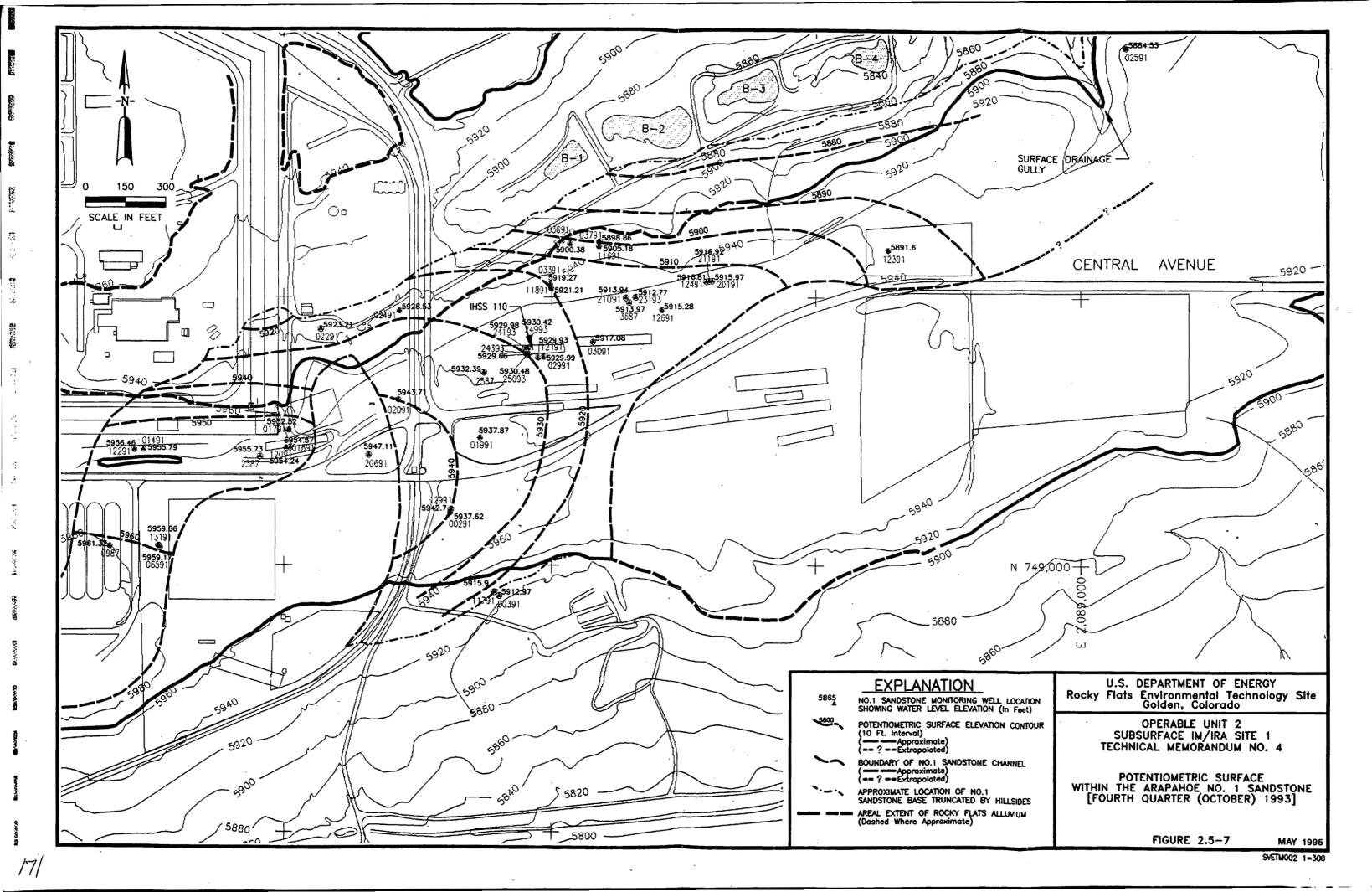






i esti





ANALYTE ABBREVIATIONS

VOLATILE ORGANIC COMPOUNDS

1,1,1,2-PCA	1.1.1.2-TETRACHLOROETHANE
1.1.2.2-PCA	1.1.2.2-TETRACHLOROETHANE
1.1.1-TCA	1.1.1-TRICHLOROETHANE
1.1-DCA	1.1-DICHLOROETHANE
1.1-DCE	1,1-DICHLOROETHENE
1,2-DCA	1.2-DICHLOROETHANE
1.2-DCE	1.2-DICHLOROETHENE
CCL	CARBON TETRACHLORIDE
CHCL.	CHLOROFORM
cis-1,2-DCE	Cis-1,2-DICHLOROETHENE
PCE	TETRACHLOROETHENE
TCE	TRICHLOROETHENE
1,2,3-TCB	1,2,3-TRICHLOROBENZENE
1,2,4-TCB	1,2,4-TRICHLOROBENZENE
TRANS-1,2-DCE	TRANS-1,2-DICHLOROETHENE
1,3-DCB	1,3-DICHLOROBENZENE
1,4-DCB	1,4-DICHLOROBENZENE
cis-1,3-DCP	cis-1,3-DICHLOROPROPANE
1,2,3-TCP	1,2,3-TRICHLOROPROPANE
ÇOC	CHEMICAL OF CONCERN
CHC	CHLORINATED HYDROCARBON

METALS AND OTHER COMPOUNDS

Al As Ba Bc	ALUMINUM ARSENIC BARIUM BERYLLIUM
Cd	CADMIUM
Ca	CALCIUM
CN	CYANIDE
Cr	CHROMIUM
Co	COBALT
Cu	COPPER
Hg	MERCURY
Fe	IRON
K	POTASSIUM
Li	LITHIUM
Mg	MAGNESIUM
Mn	MANGANESE
Mo .	MOLYBDENUM
Na	SODIUM
Ni	NICKEL
Pb	LEAD
Sp	ANTIMONY
Se	SELENIUM
Si	SILICON
Sn	TIN
Sr	STRONTIUM
Ā	VANADIUM
Zn	ZINC

RADIONUCLIDES

Am-241	AMERICIUM-241
Cs-137	CESIUM-137
Pu-239	PLUTONIUM-239
Pu-239/240	PLUTONIUM-239/240
Ra-226	RADIUM-226
Ra-228	RADIUM-228
Sr-89.90	STRONTIUM-89,90
Sr-90	STRONTIUM-90
U-233,234	URANIUM-233,234
U-235	URANIUM-235
U-238	URANIUM-238

OTHER ABBREVIATIONS

(D) DISSOLVED (FILTERED SAMPLE) (T) TOTAL (UNFILTERED SAMPLE)

LABORATORY QUALIFIERS

- B = ORGANICS (VOLATILES, SEMIVOLATILES, PESTICIDES) INDICATES CHEMICAL WAS IN BOTH THE SAMPLE AND METHOD BLANK
- B-RV = INDICATES CHEMICAL WAS IN BOTH THE SAMPLE AND METHOD BLANK BUT IS CONSIDERED TO BE A REAL VALUE.
- B-ND = INDICATES CHEMICAL WAS IN BOTH THE SAMPLE AND METHOD BLANK BUT IS CONSIDERED TO BE A NON-DETECTED RESULT.
 - B = INORGANIC (METALS & INORGANICS) DETECTED CONCENTRATION WAS LESS THAN CRQL
 - B = RADIONUCLIDES THE ACTIVITY IN THE METHOD BLANK EXCEEDED THE MDA
 - C = PESTICIDE RESULT WHERE IDENTIFICATION WAS CONFIRMED BY GC/MS
 - C = RADIONUCLIDES INDICATED ELEVATED TDS
 - E = ORGANICS CHEMICAL EXCEEDS CALIBRATION RANGE OF THE INSTRUMENT
 - E = INORGANIC REPORTED VALUE IS ESTIMATED DUE TO INTERFERENCE
 - F = ALPHA SPECTROMETRY FWHM EXCEEDED ACCEPTANCE LIMITS
 - D = ORGANICS ANALYSIS WAS PERFORMED AT A DILUTION
 - J = ORGANICS POSITIVELY IDENTIFIED RESULT IS CONSIDERED TO BE ESTIMATED
 - J = INORGANICS & RADIONUCLIDES ESTIMATED QUANTIFICATION
 - N = METALS SPIKE RECOVERIES IN THE MATRIX SPIKE SAMPLE DID NOT MEET ADVISORY LIMITS
 - S = METALS THE REPORTED VALUE WAS DETERMINED BY THE METHOD OF STANDARD ADDITION (MSA)
 - U = ALL ANALYSES ANALYZED CHEMICAL WAS NOT DETECTED ABOVE THE SAMPLE QUANTITATION LIMIT
 - W = METALS POST DIGESTION SPIKE DID NOT MEET CONTROL LIMITS
 - X = OPEN AND DEFINED BY LABORATORY
 - Y = RADIONUCLIDES CHEMICAL YIELD EXCEEDED ACCEPTANCE LIMITS
 - * = METALS MATRIX DUPLICATE ANALYSIS DO NOT MEET ADVISORY LIMITS

VALIDATION CODES AND QUALIFIERS

- A = RESULT ACCEPTED WITH QUALIFICATIONS
- AJ = RESULT ACCEPTED, BUT WAS ESTIMATED
- J = ESTIMATED RESULT DUE TO OUTSIDE HOLDING TIME, IMPROPERLY PRESERVED, QUALITY CONTROL FARAMETER OUTSIDE CONTROL LIMIT
- R = REJECTED RESULT
- U = ALL ANALYSES ANALYZED CHEMICAL WAS NOT DETECTED ABOVE THE SAMPLE QUANTITATION LIMIT
- V = VALID RESULT
- VA = VALID RESULT WITH QUALIFICATIONS

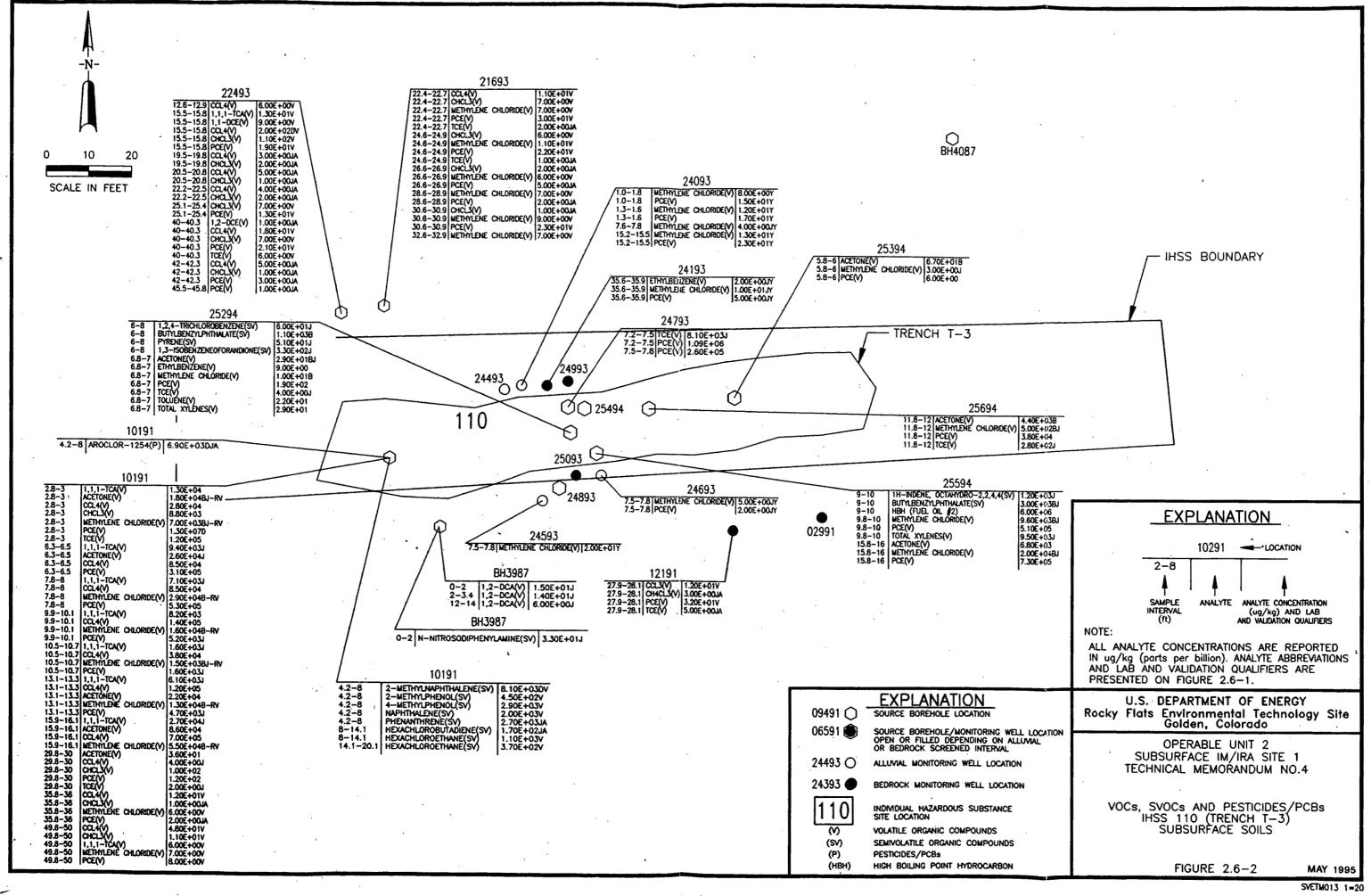
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Rocky Flats Environmental Technology Site
Golden, Colorado

OPERABLE UNIT 2
SUBSURFACE IM/IRA SITE 1
TECHNICAL MEMORANDUM NO. 4

ANALYTE ABBREVIATIONS, LABORATORY AND VALIDATION QUALIFIERS

FIGURE 2.6-1

MAY 1995



SOIL SYMBOLS



GP POORLY—GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES

GM SILTY GRAVELS, GRAVEL-SAND-SILT

GC CLAYEY GRAVELS, GRAVEL-SAND-CLAY

SW WELL-GRADED SANDS, GRAVELLY SANDS,

SP POORLY-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES

SM SILTY SANDS, SAND-SILT MIXTURES

SC CLAYEY SANDS, SAND-CLAY, MIXTURES

ML INORCANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY

CL INORGANIC CLAYS OF LOW TO MEDIUM
PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS
SILTY CLAYS, LEAN CLAYS

CH INORGANIC CLAYS OR HIGH PLASTICITY,

LIST OF CROSS-SECTION UNITS

Qrf = rocky flats allumium
Qc = collumium Ka = arapahoe formation Ka(No.1) = arapahoe formation no. 1 sandstone Ka/KI = arapahoe or laramie formation KI(ss) = laramie formation sandstone

BEDROCK SYMBOLS



SANDSTONE



SILTY SANDSTONE



CLAYEY SANDSTONE

SILTS

SILTSTONE



SANDY SILTSTONE



CLAYEY SILTSTONE



CLAYSTONE



SANDY CLAYSTONE



SILTY CLAYSTONE



CALICHE

L		

NO RECOVERY OF SAMPLED INTERVAL NOT LOGGED

WATER LEVEL AND LOCATION SYMBOLS

5/92 MEASURED HIGH WATER LEVEL AND DATE

INITIAL WATER AT TIME OF DRILLING

ALLUMAL/COLLUVIAL MONITORING WELL LOCATION

BEDROCK MONITORING WELL LOCATION

SOURCE BOREHOLE LOCATION

SOURCE BOREHOLE AND MONITORING WELL LOCATION

09991 LOCATION NUMBER. LAST 2 DIGITS INDICATE YEAR IN WHICH LOCATION WAS DRILLED

GROUNDWATER ANALYTE DATA

● CCI₄

CARBON TETRACHLORIDE

CHCI,

CHLOROFORM

● TCE

TRICHLOROETHENE

▲ PCE

TETRACHLOROETHENE

O TOTAL Xylenes

TOTAL VOCs

280

CONCENTRATION (ug/Kg).

LINE CONNECTING CONCENTRATION VALUES AT SAMPLE POINTS ABOVE WATER LEVEL AT THE TIME OF DRILLING. INFERRED WHERE LIMITED DATA EXISTS.

LINE CONNECTING CONCENTRATION VALUES AT SAMPLE POINTS BELOW WATER LEVEL AT THE TIME OF DRILLING. INFERRED WHERE LIMITED DATA EXISTS.

INFERRED G

INFERRED GEOLOGICAL CONTACT

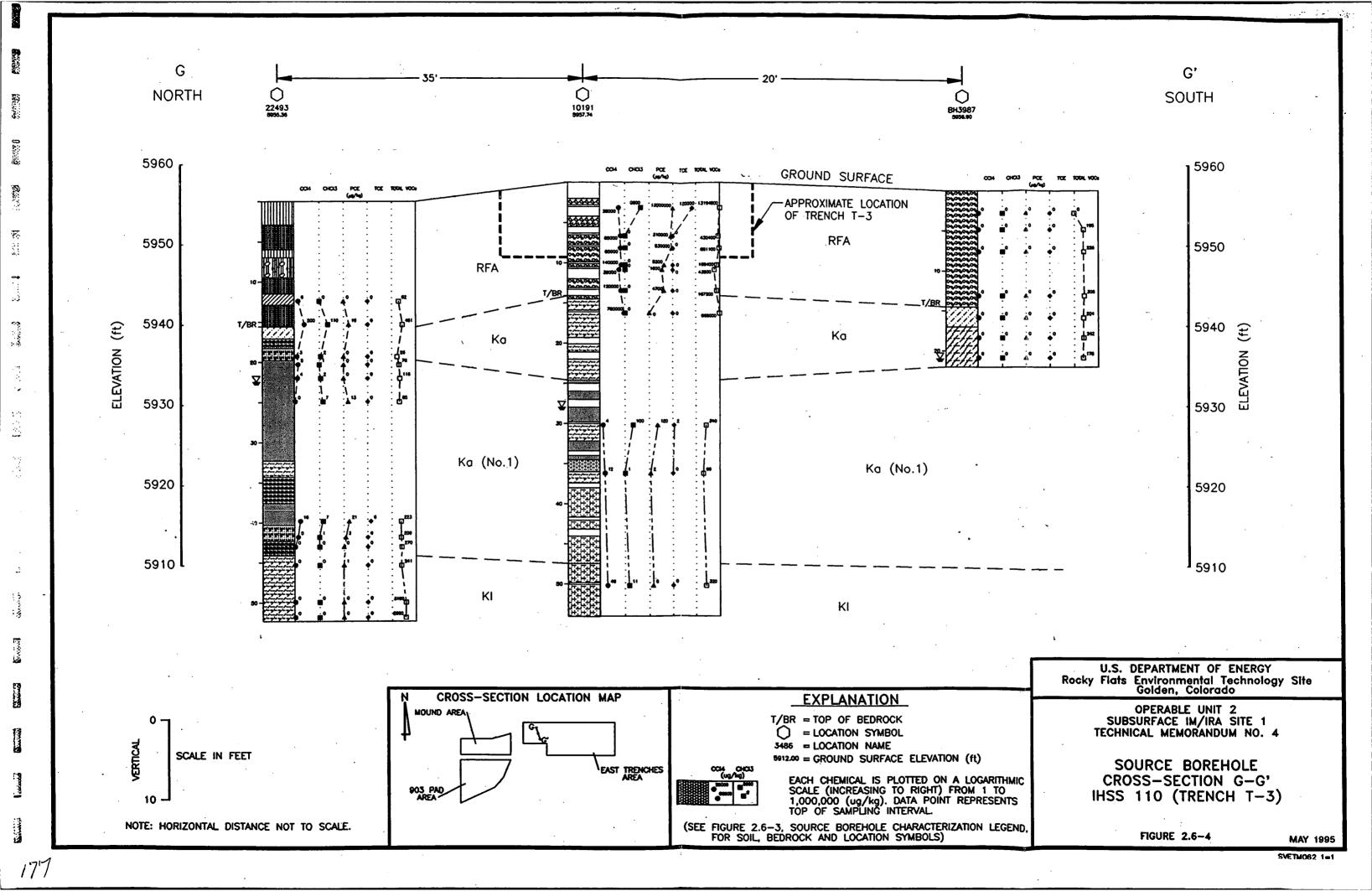
U.S. DEPARTMENT OF ENERGY Rocky Flats Environmental Technology Site Golden, Colorado

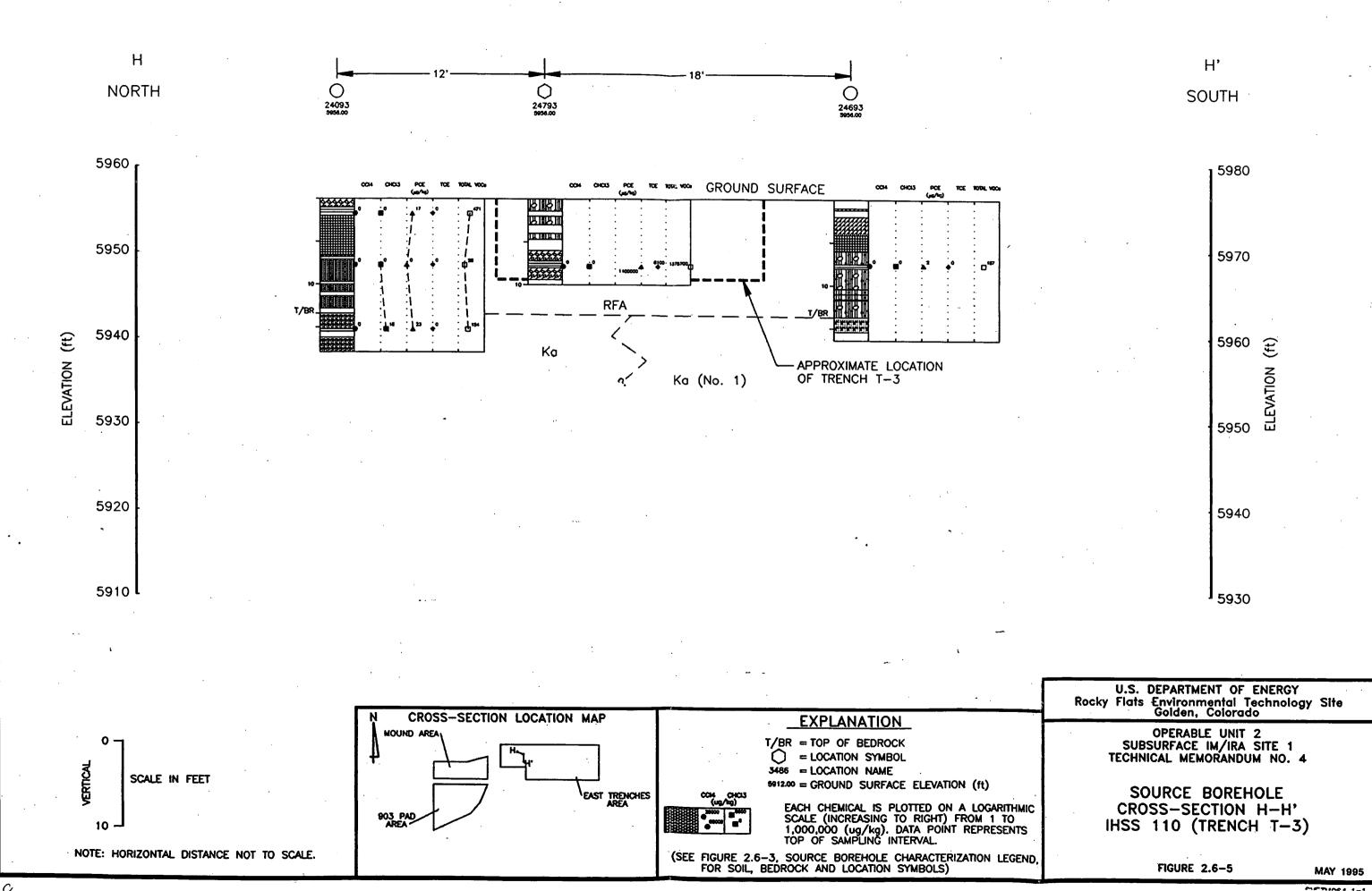
> OPERABLE UNIT NO.2 SUBSURFACE IM/IRA SITE 1 TECHNICAL MEMORANDUM NO. 4

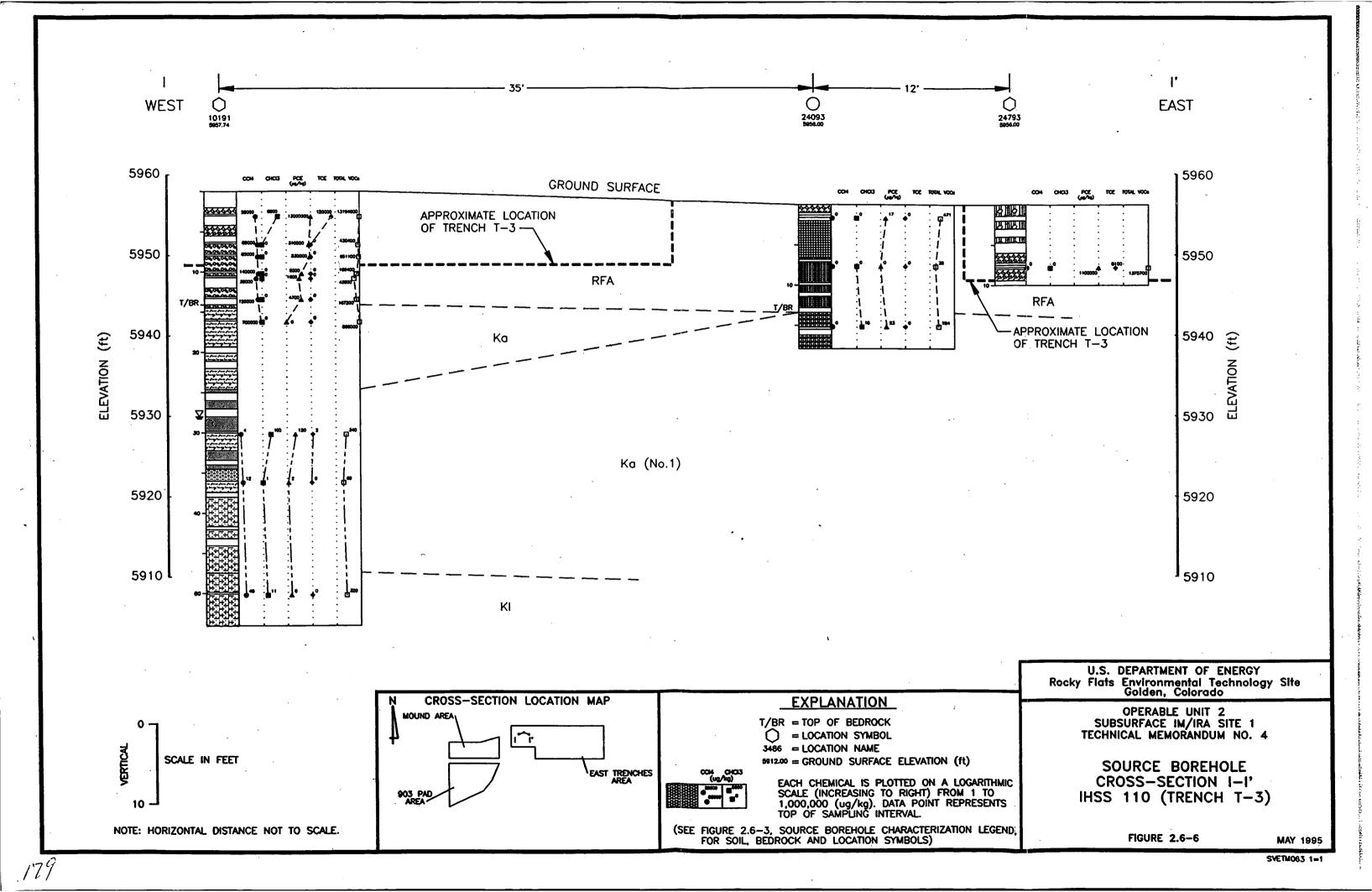
SOURCE BOREHOLE CROSS-SECTION LEGEND

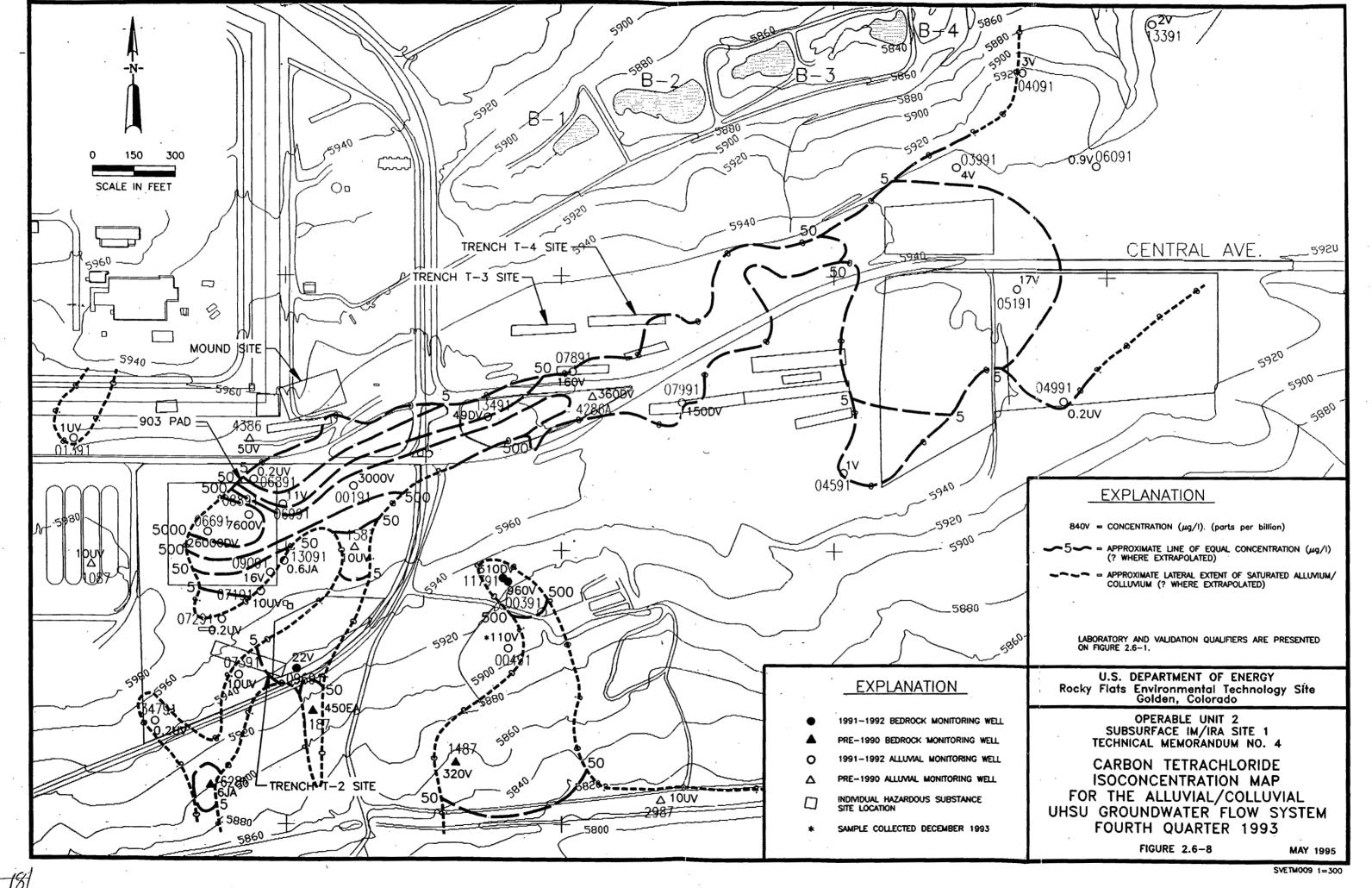
FIGURE 2.6-3

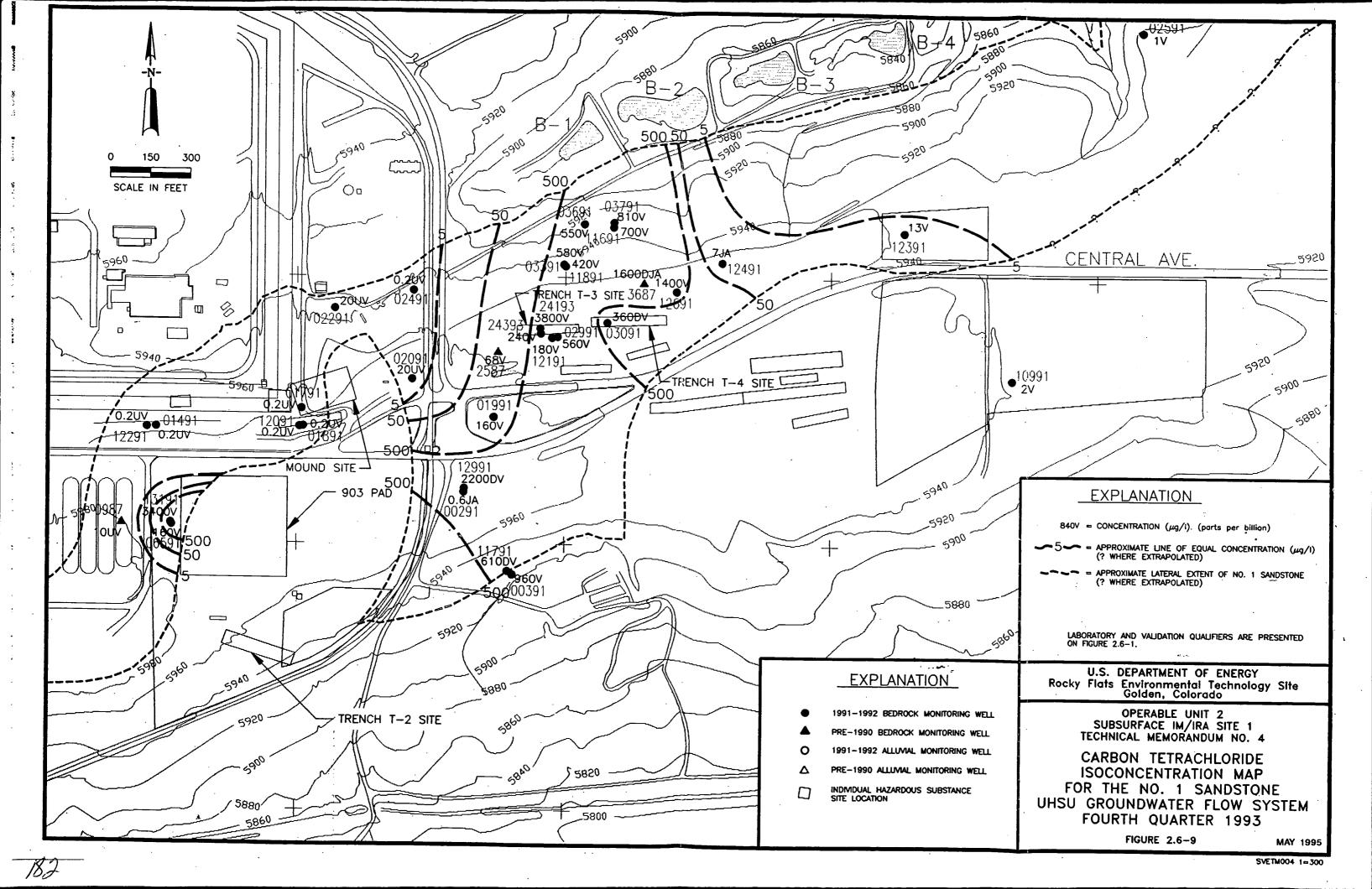
MAY 1995

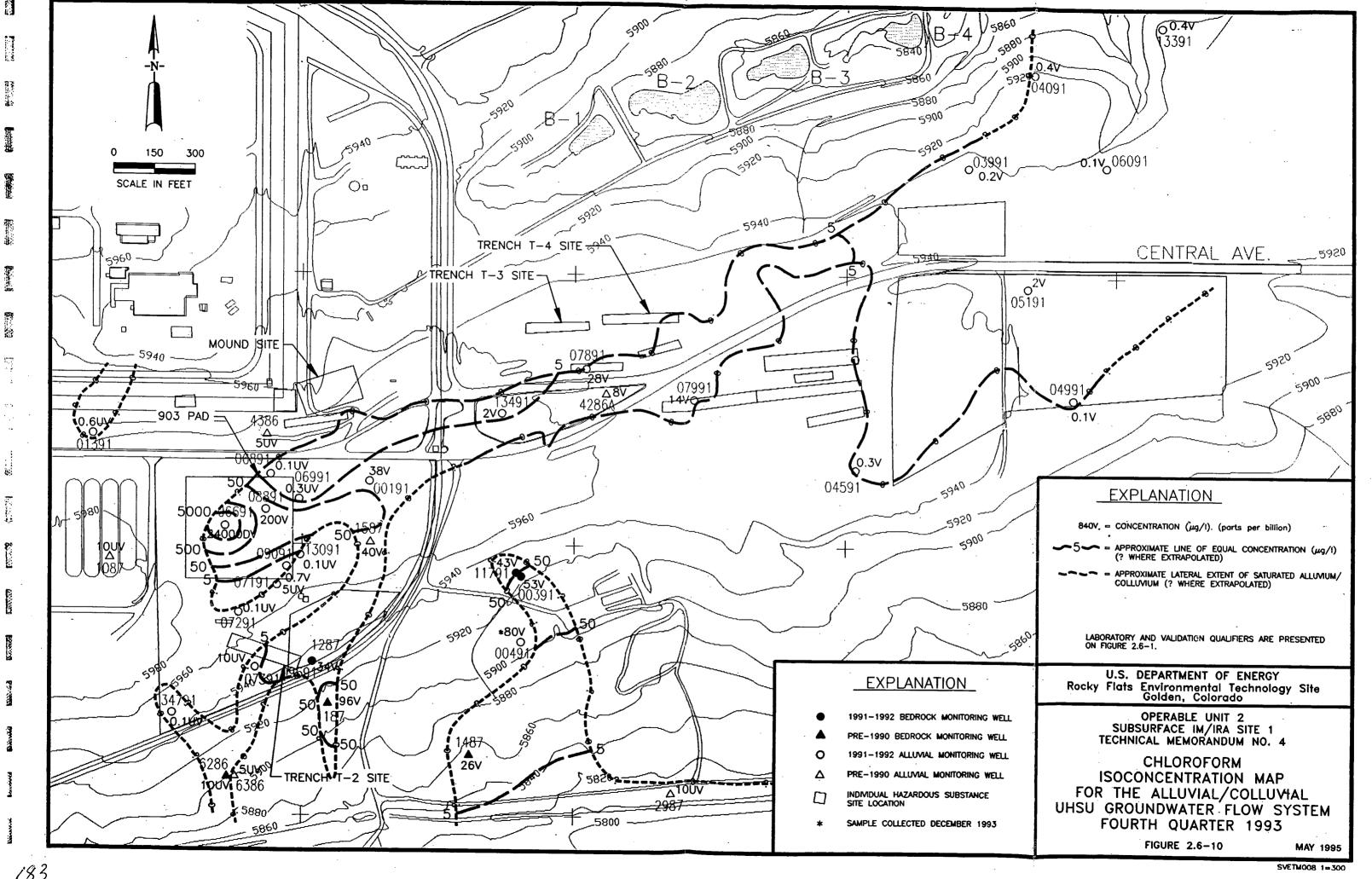


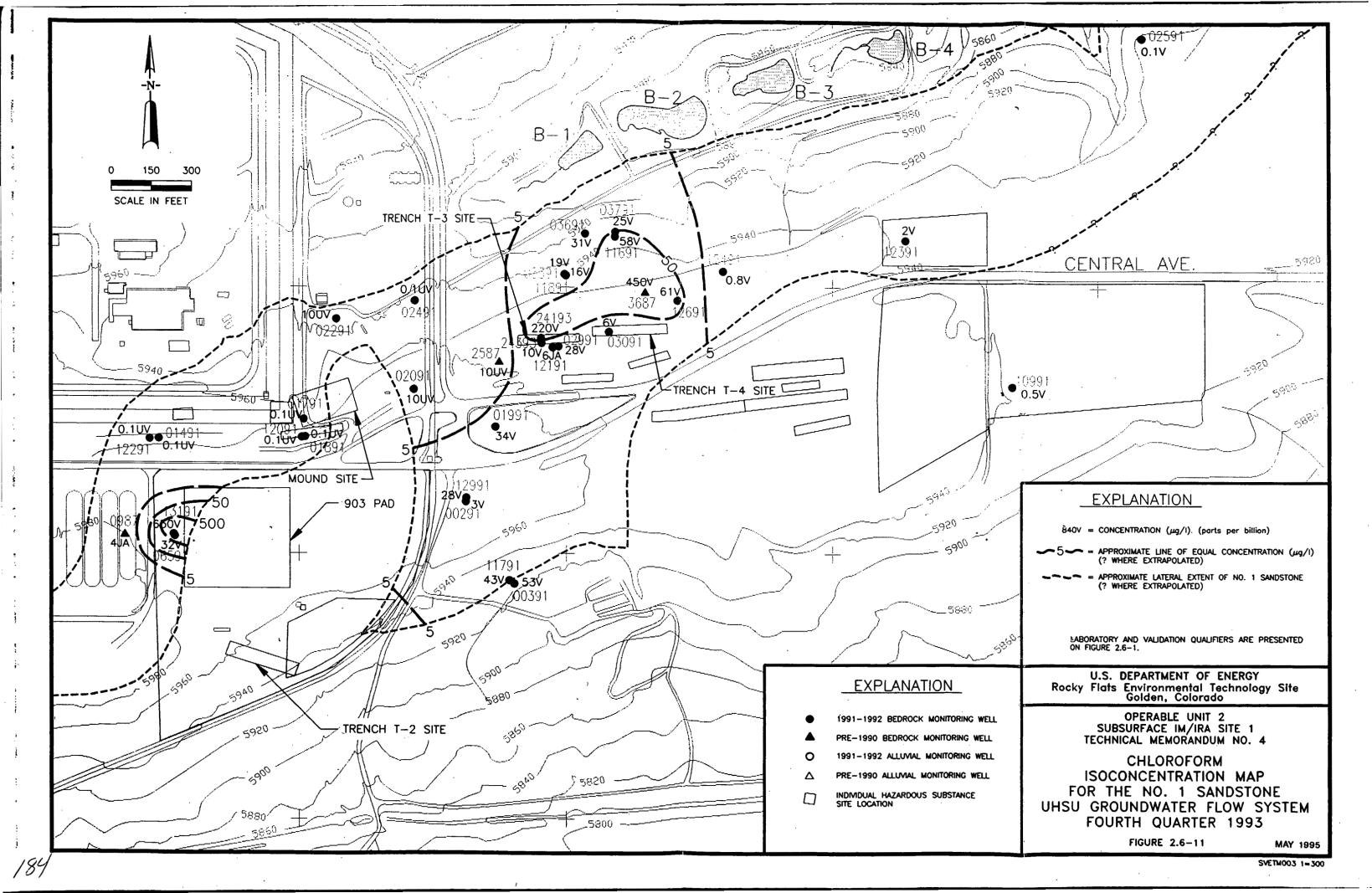


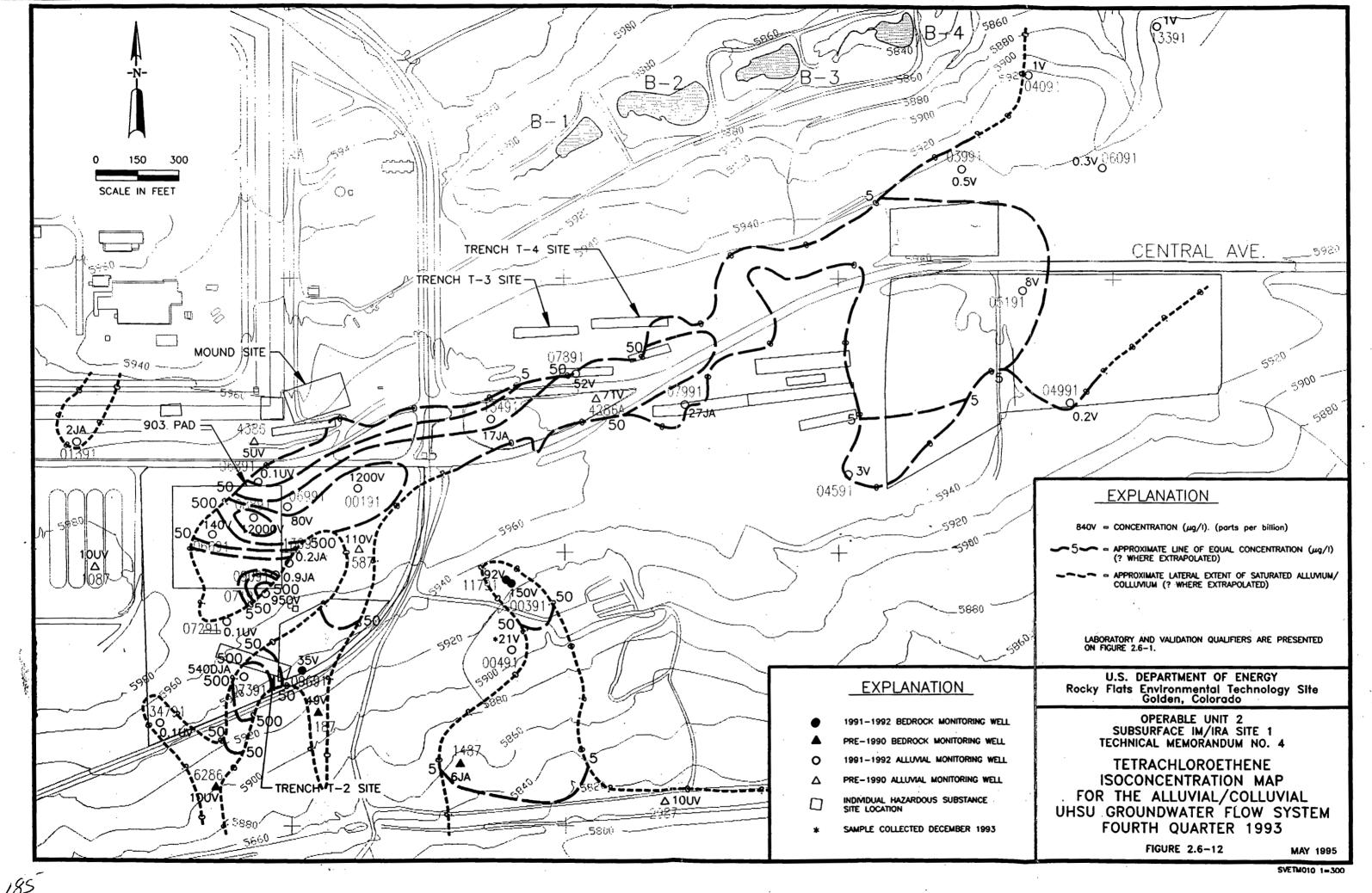


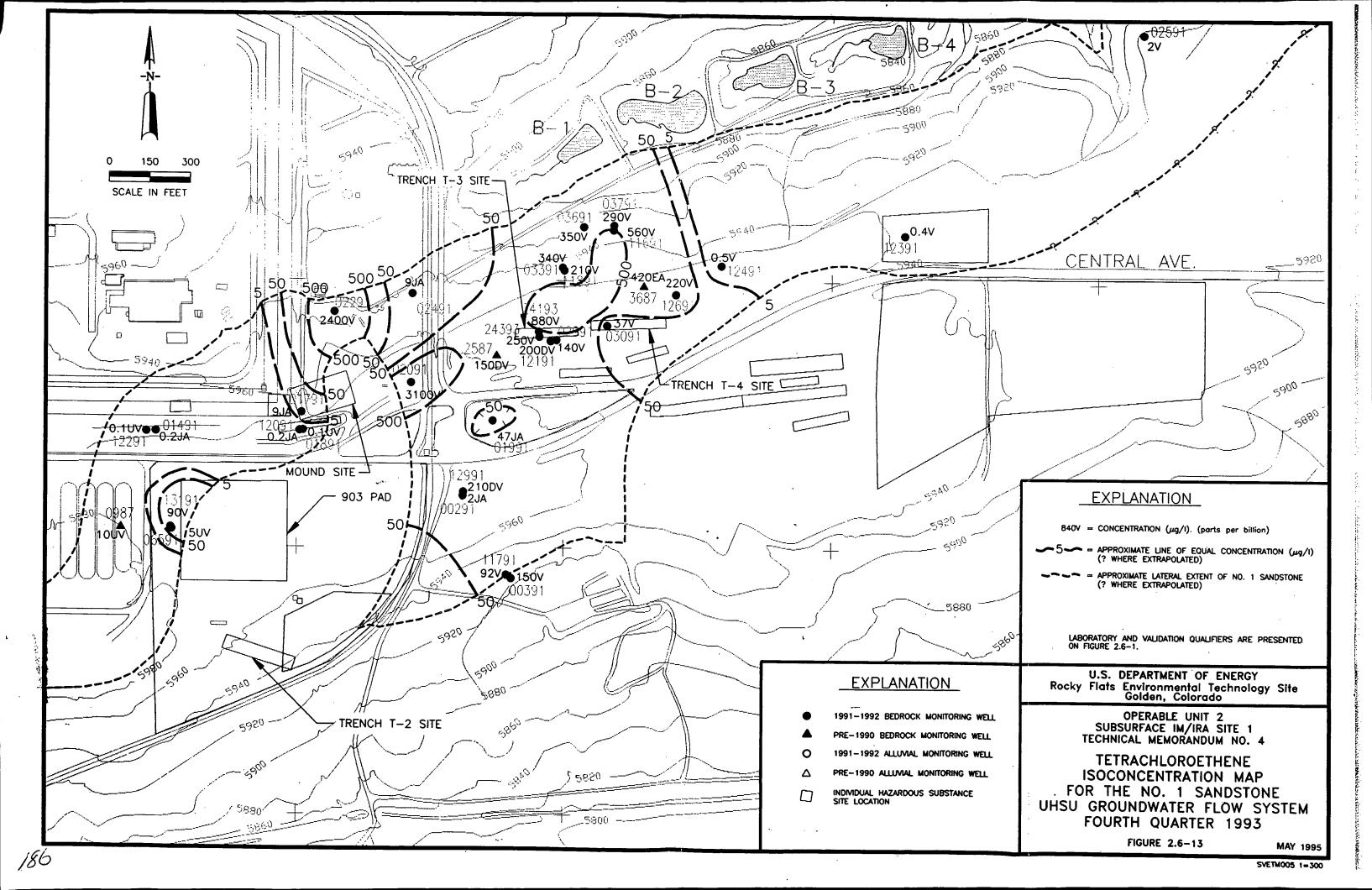


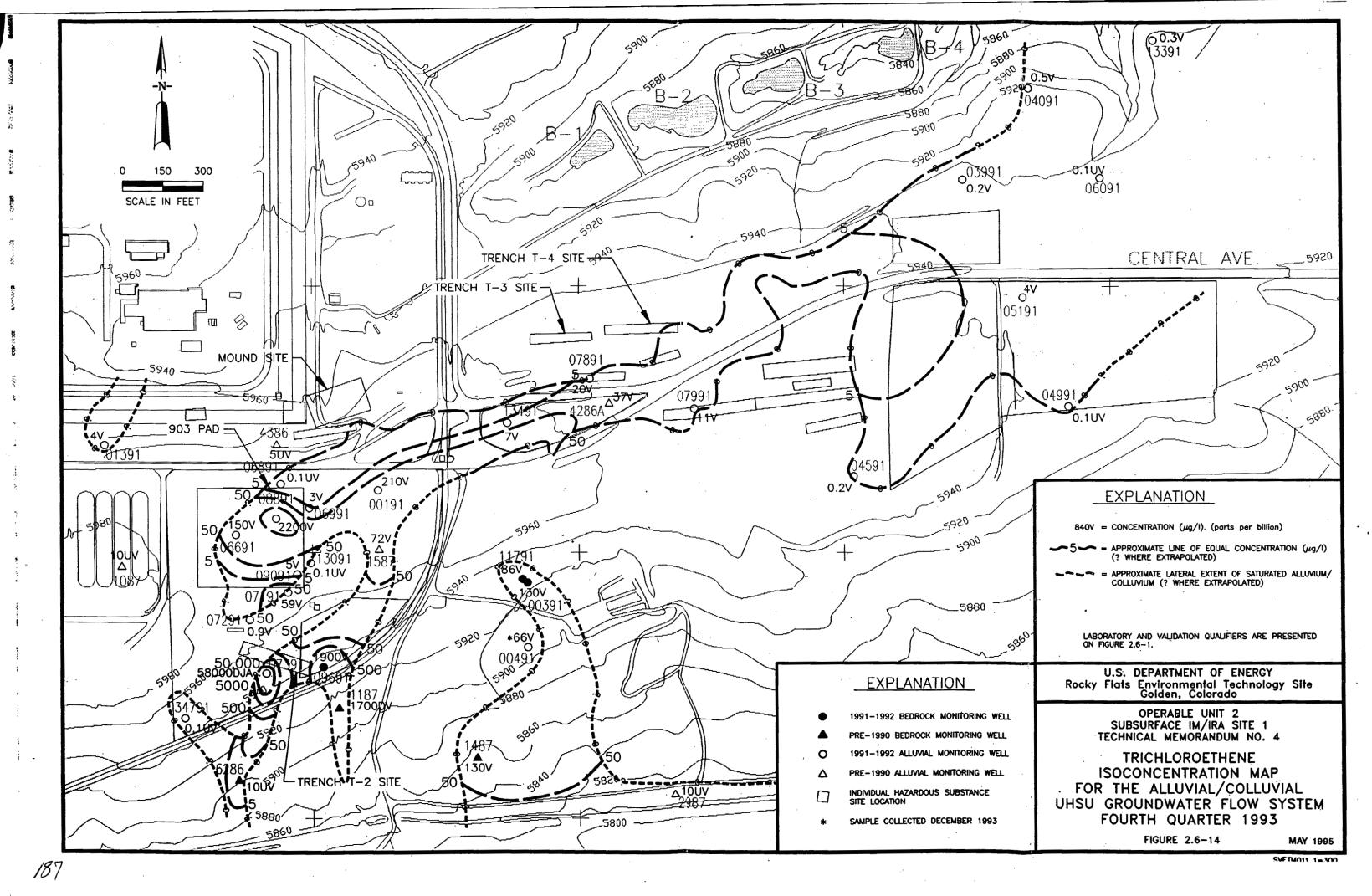


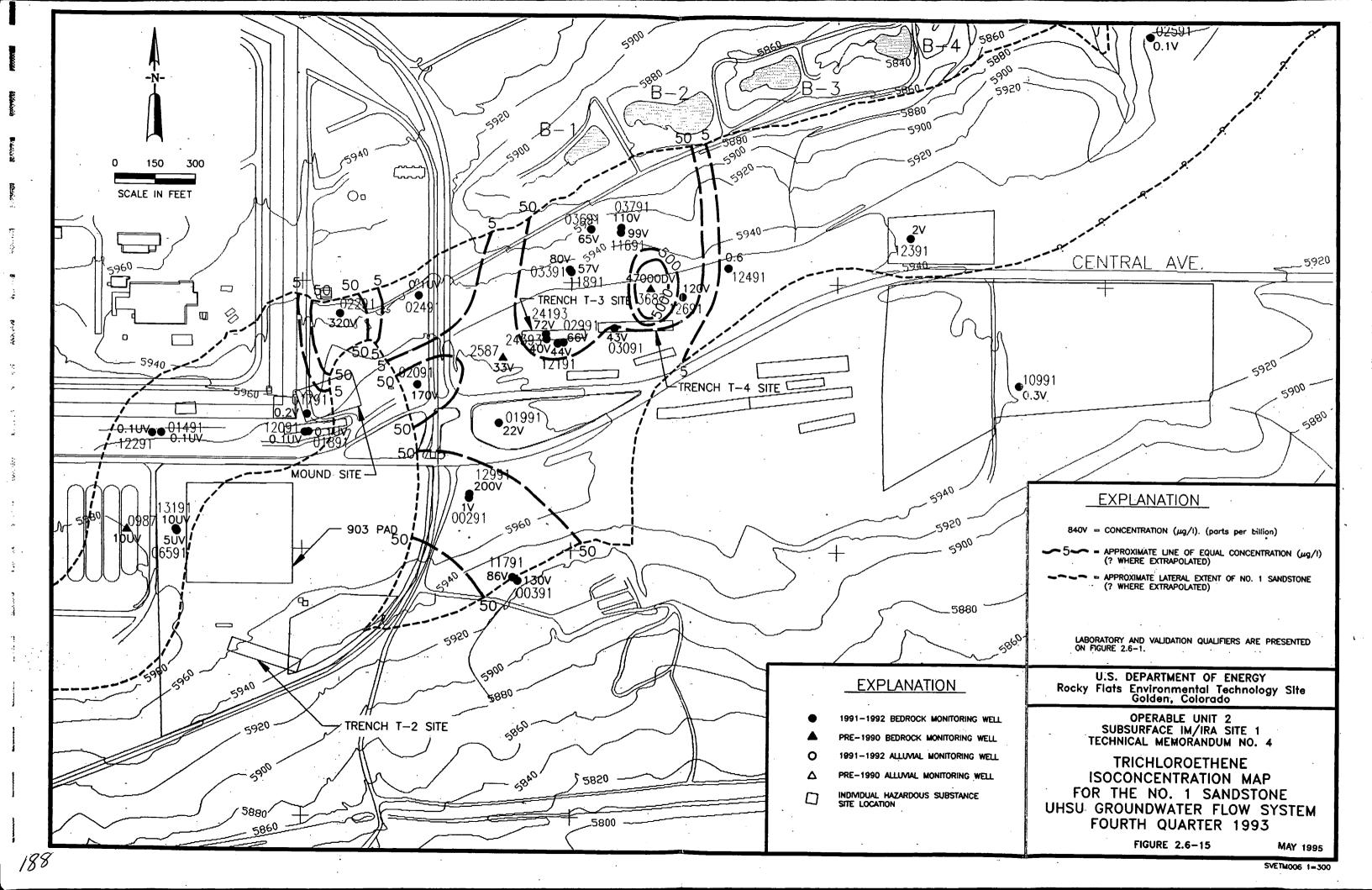


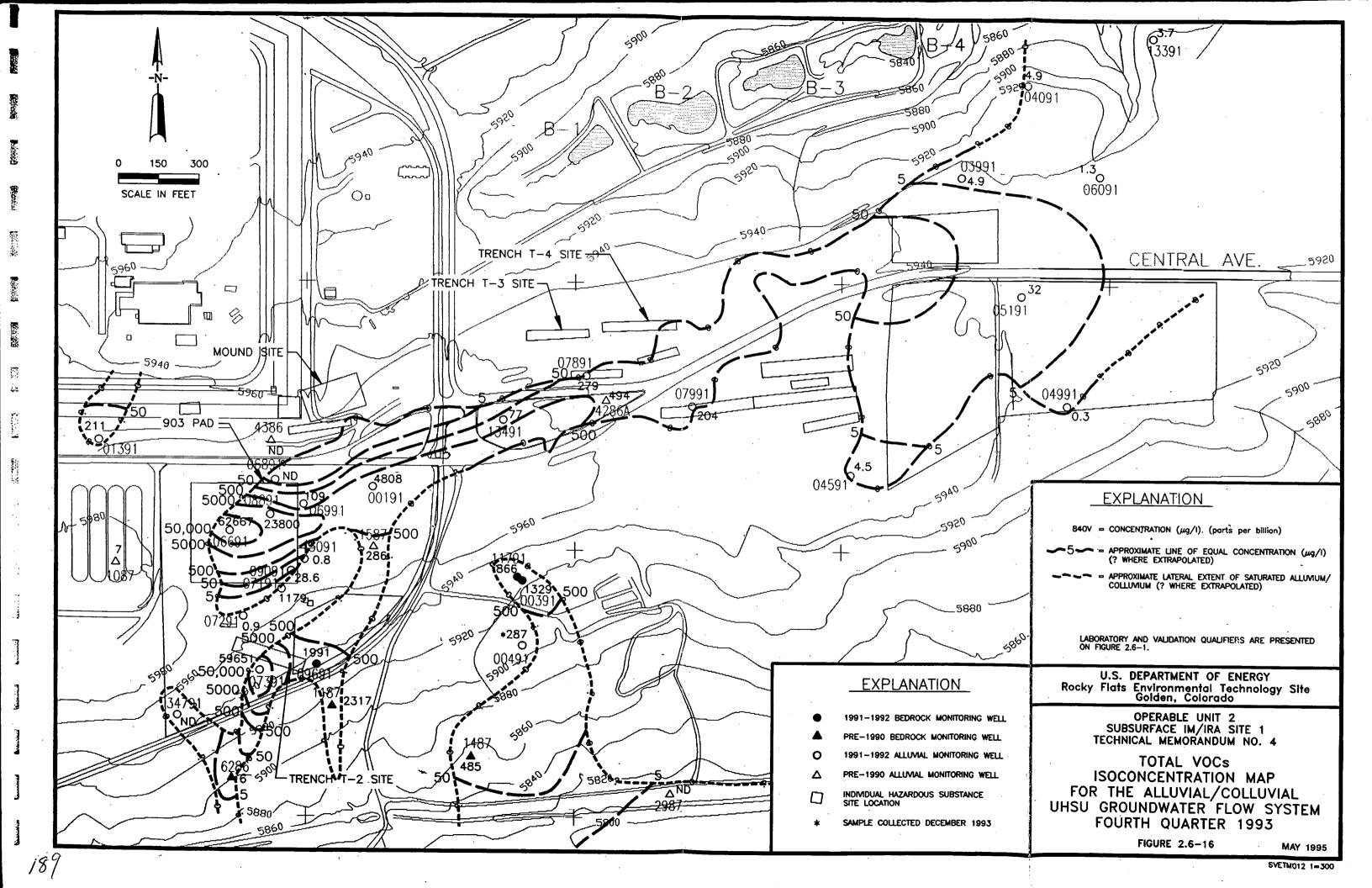


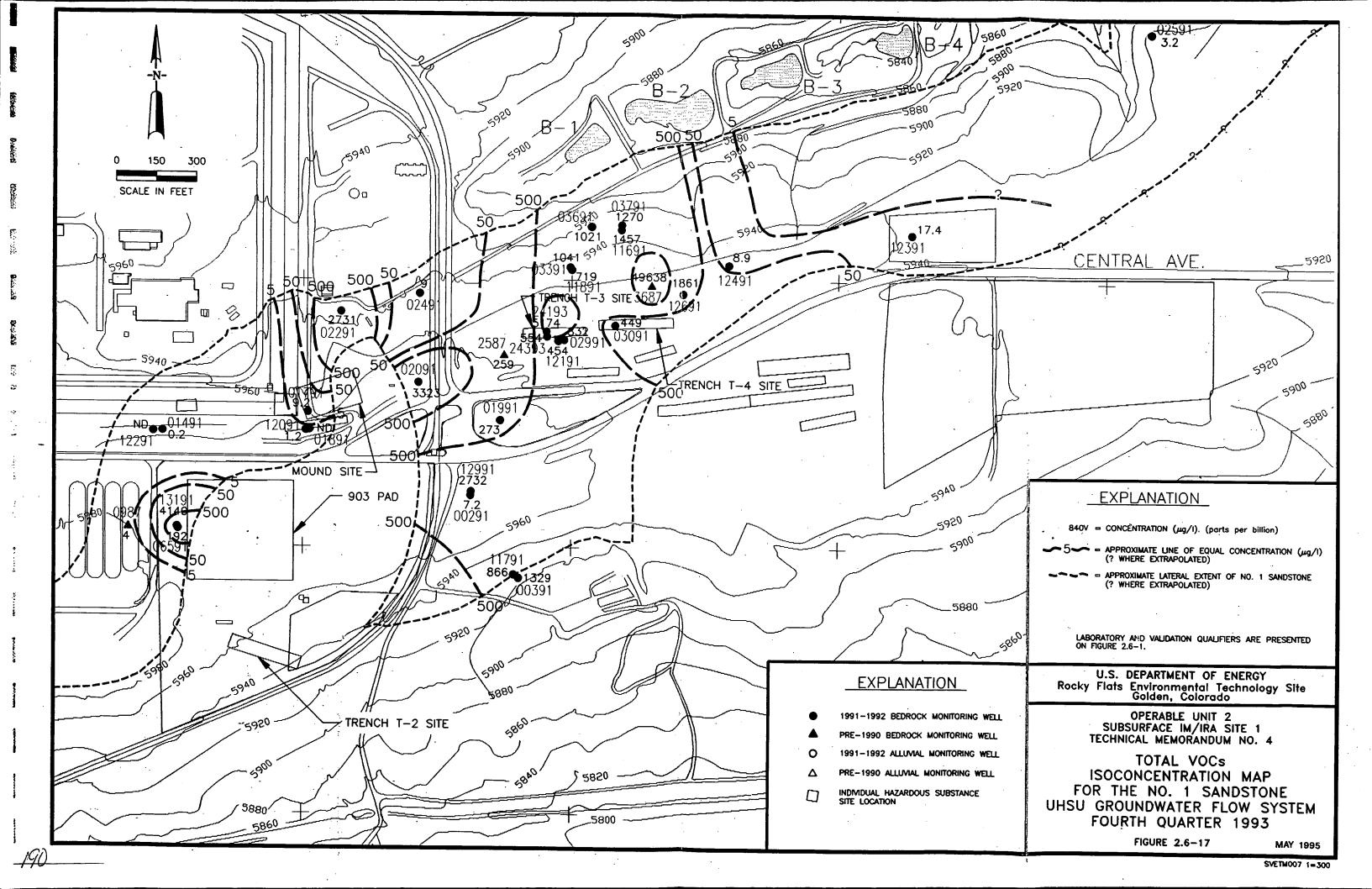


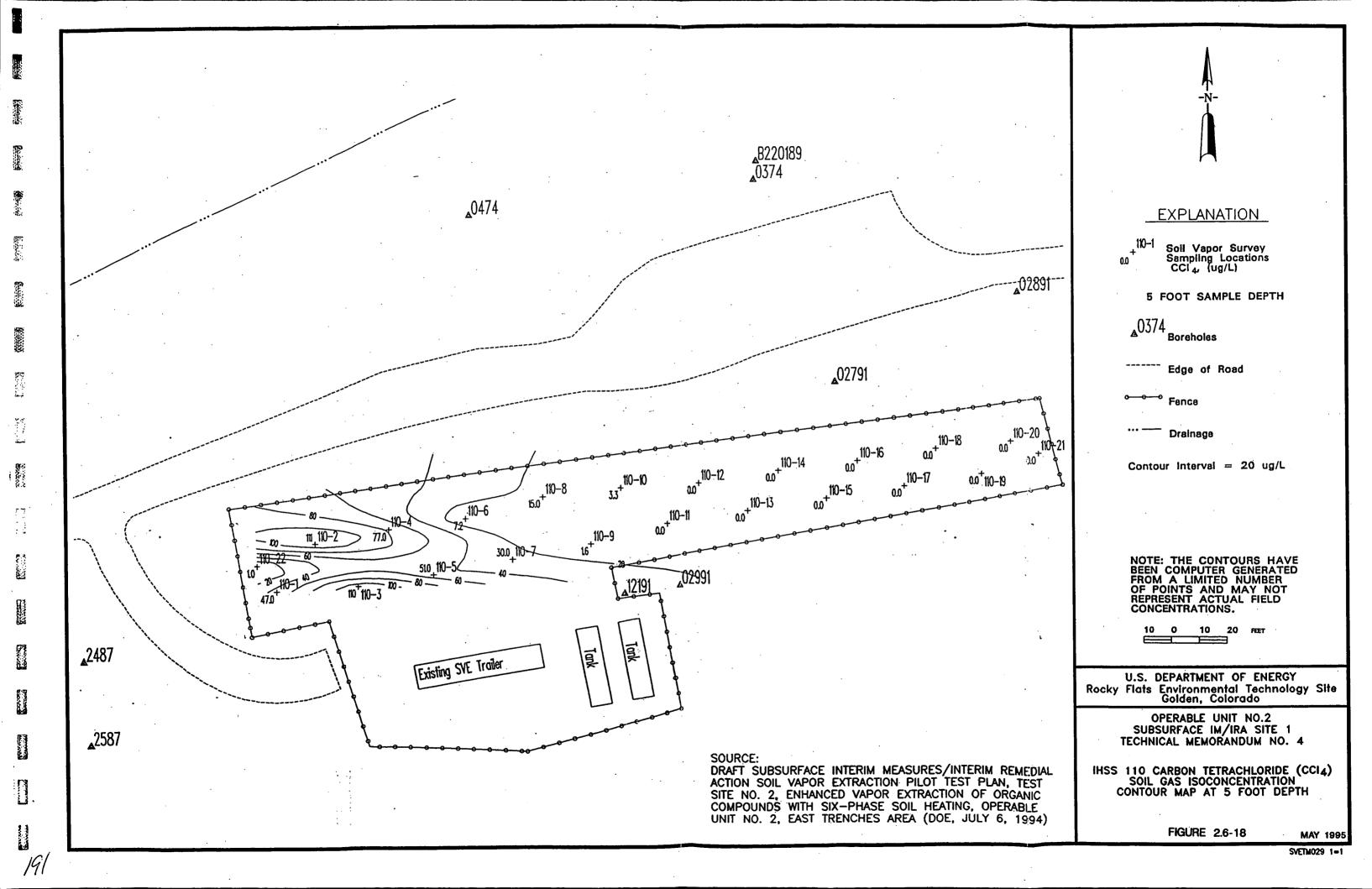


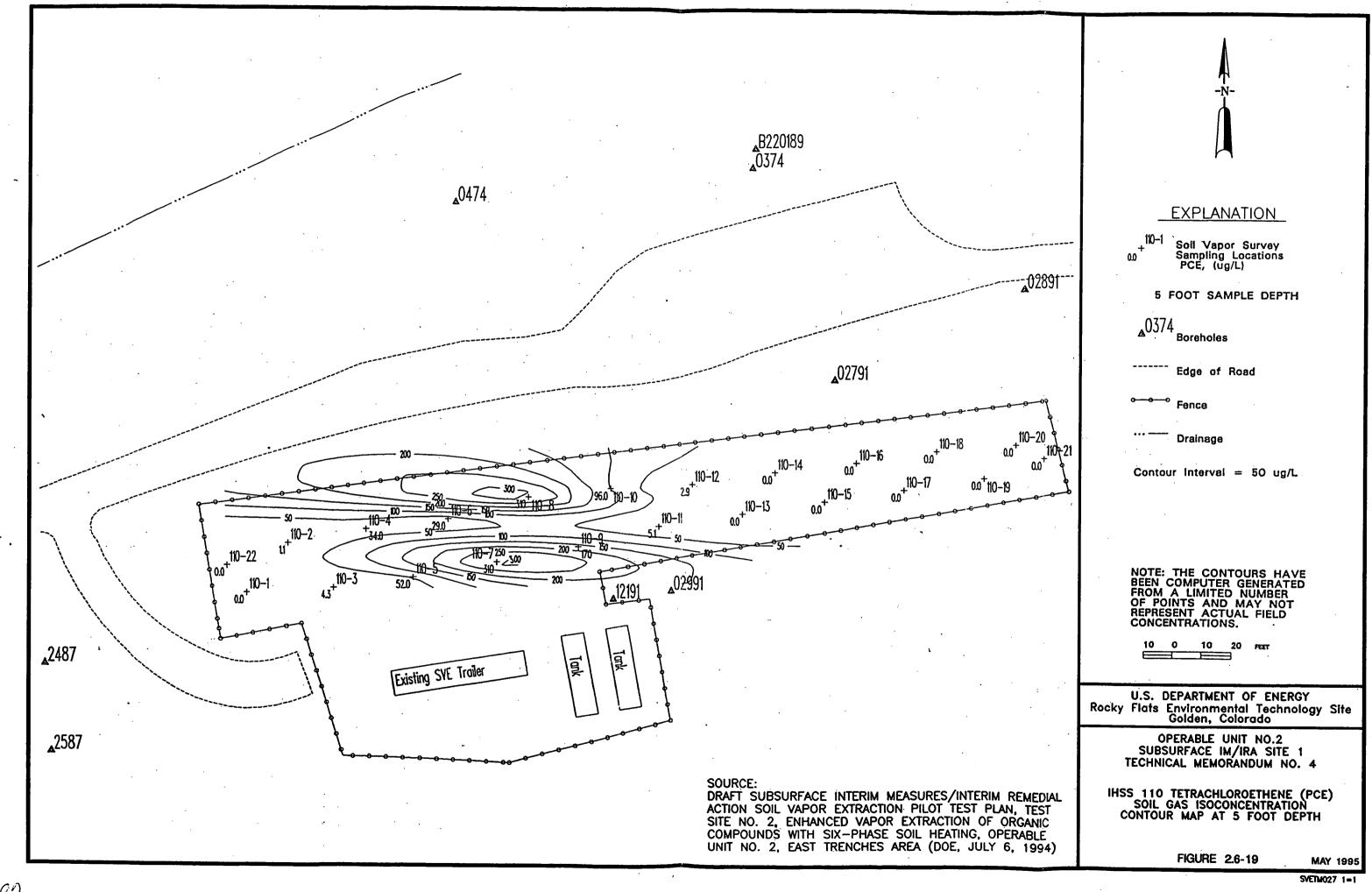


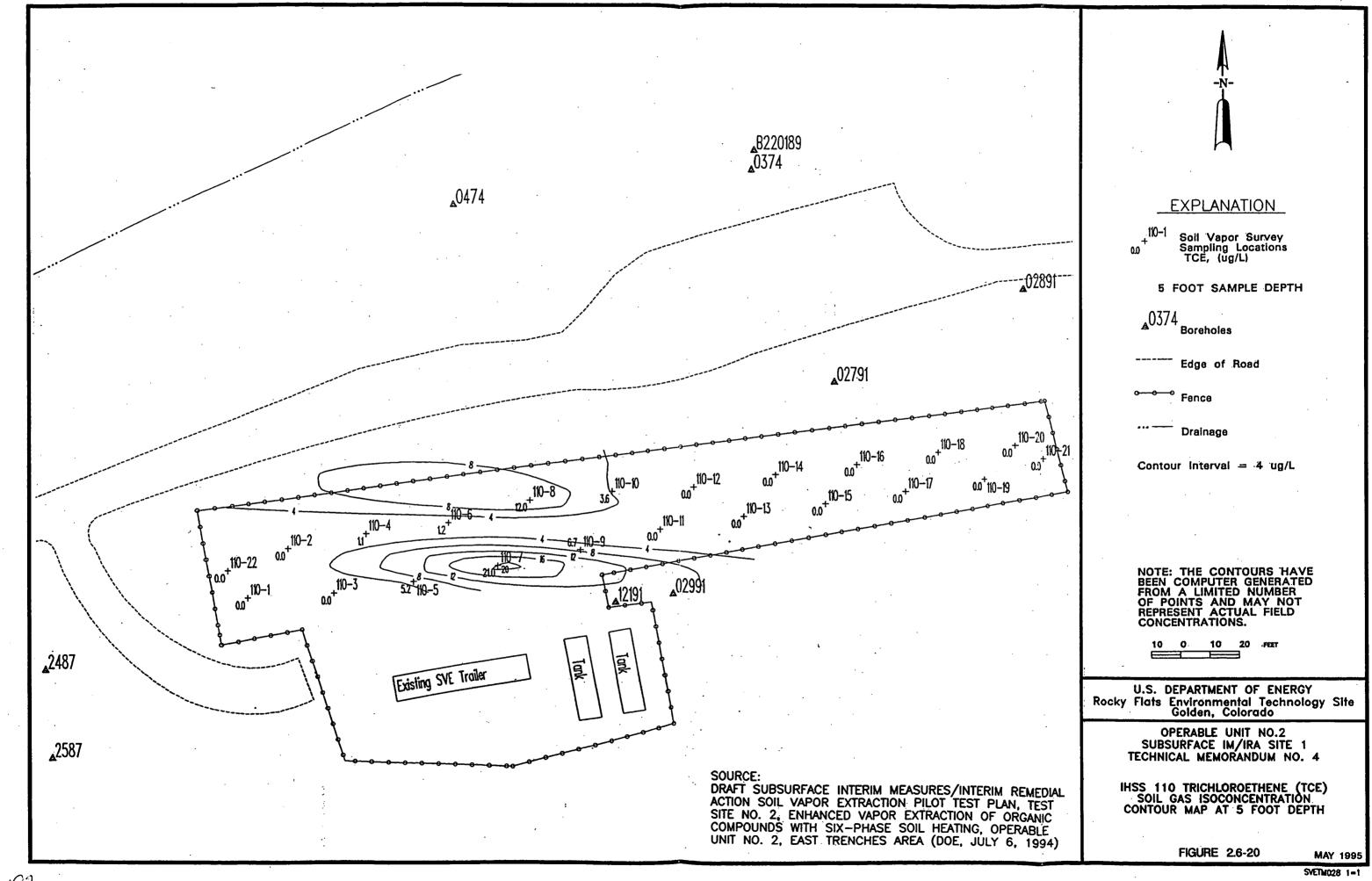










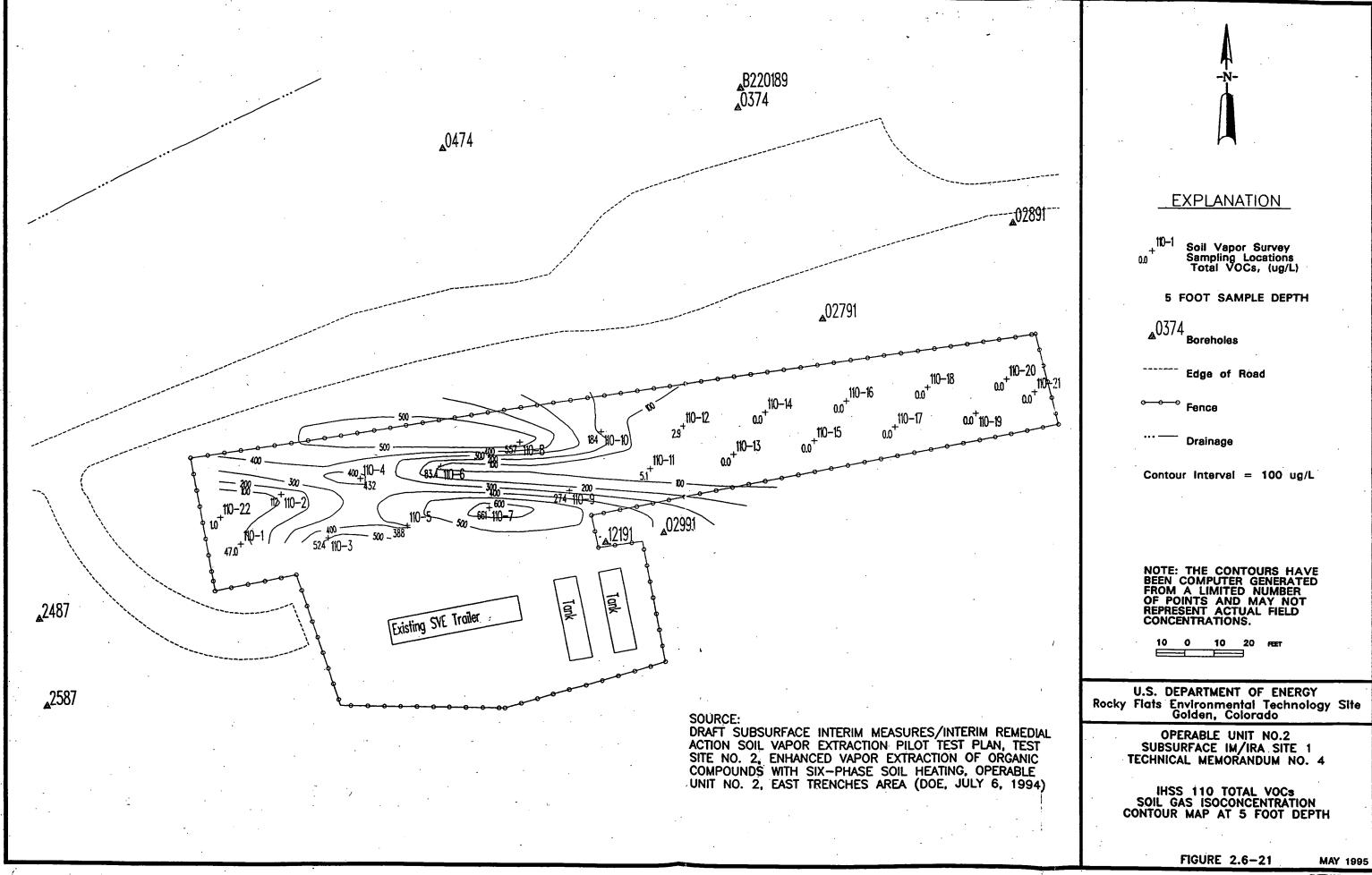


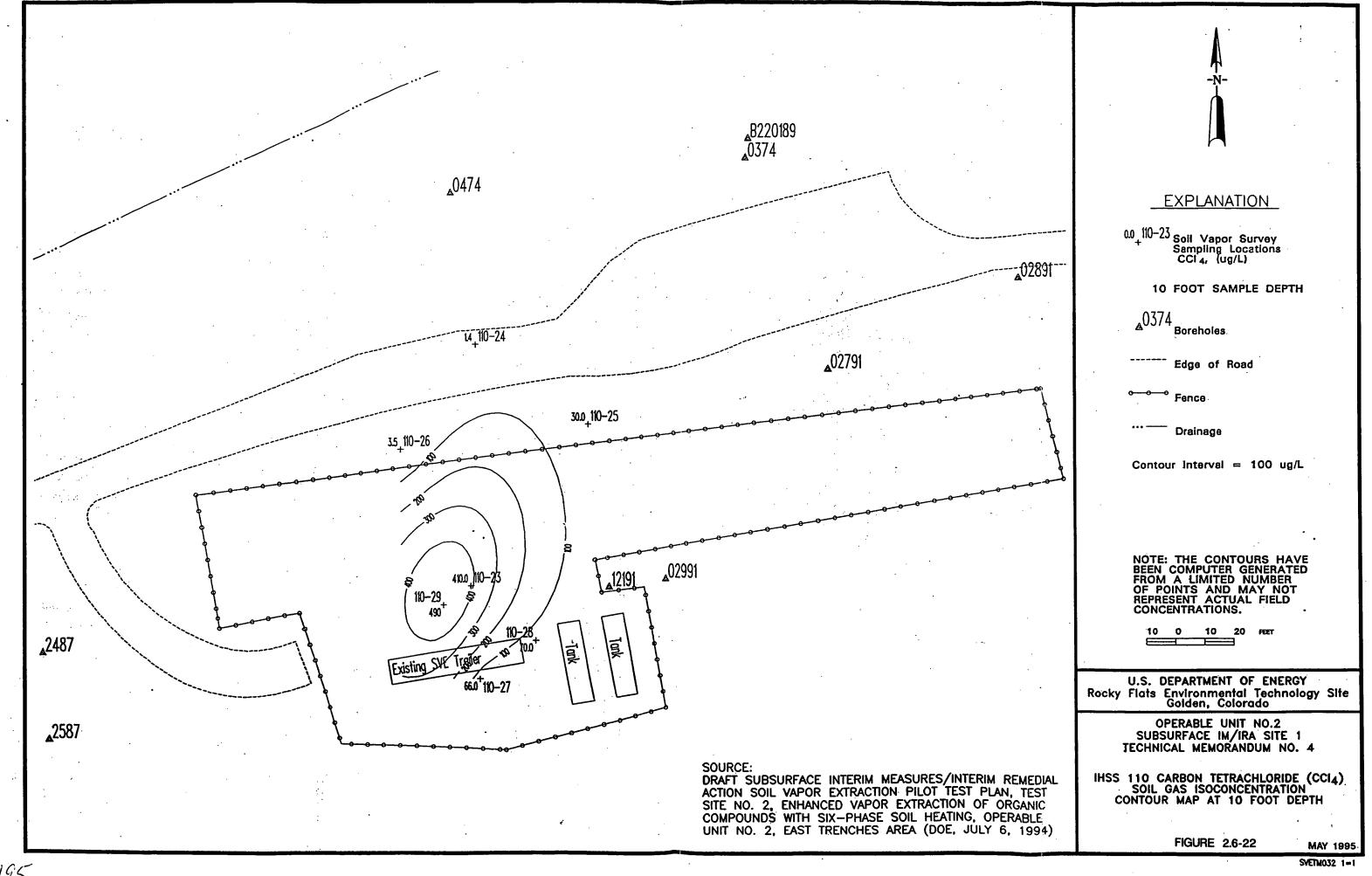
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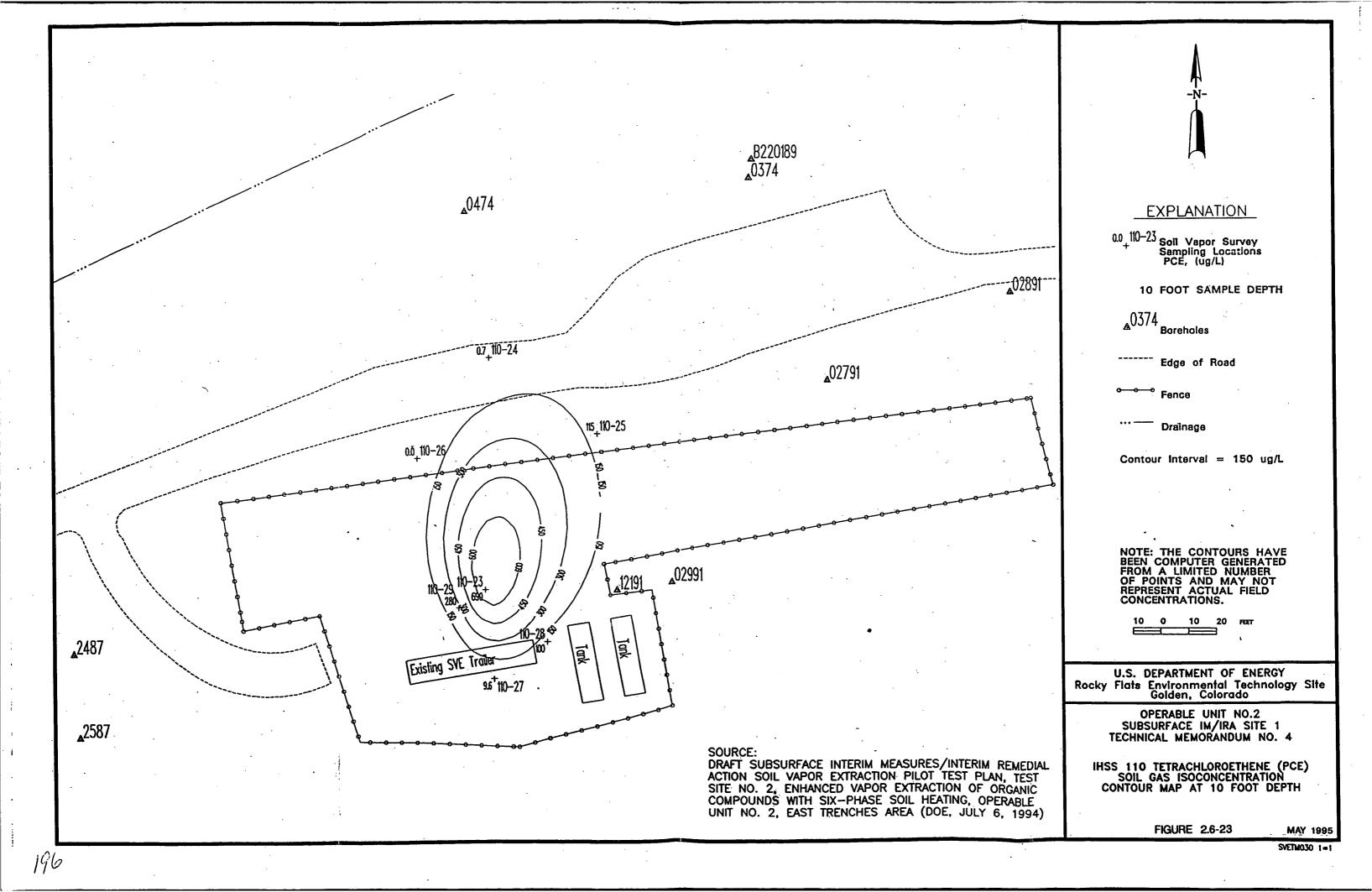
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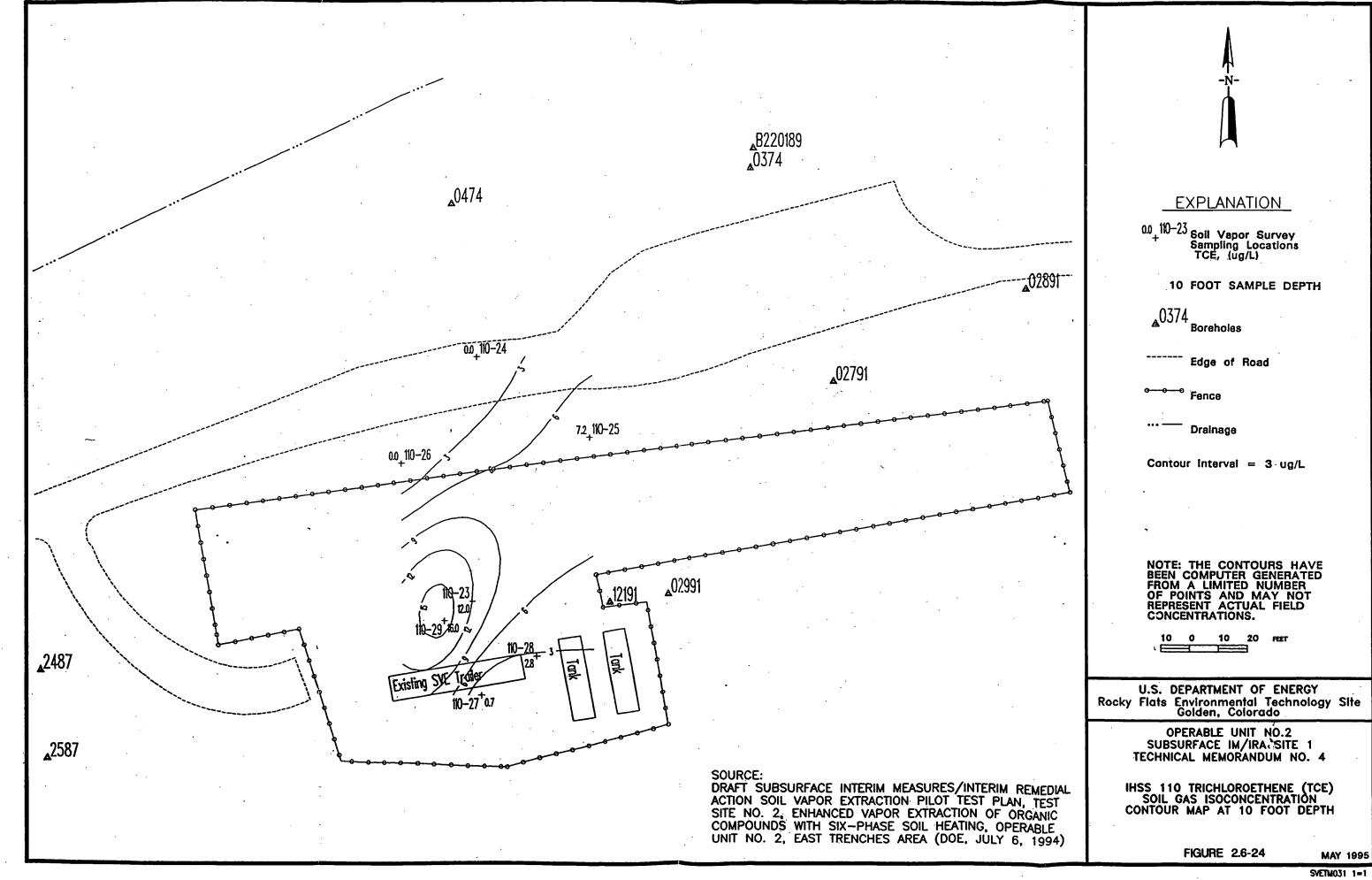
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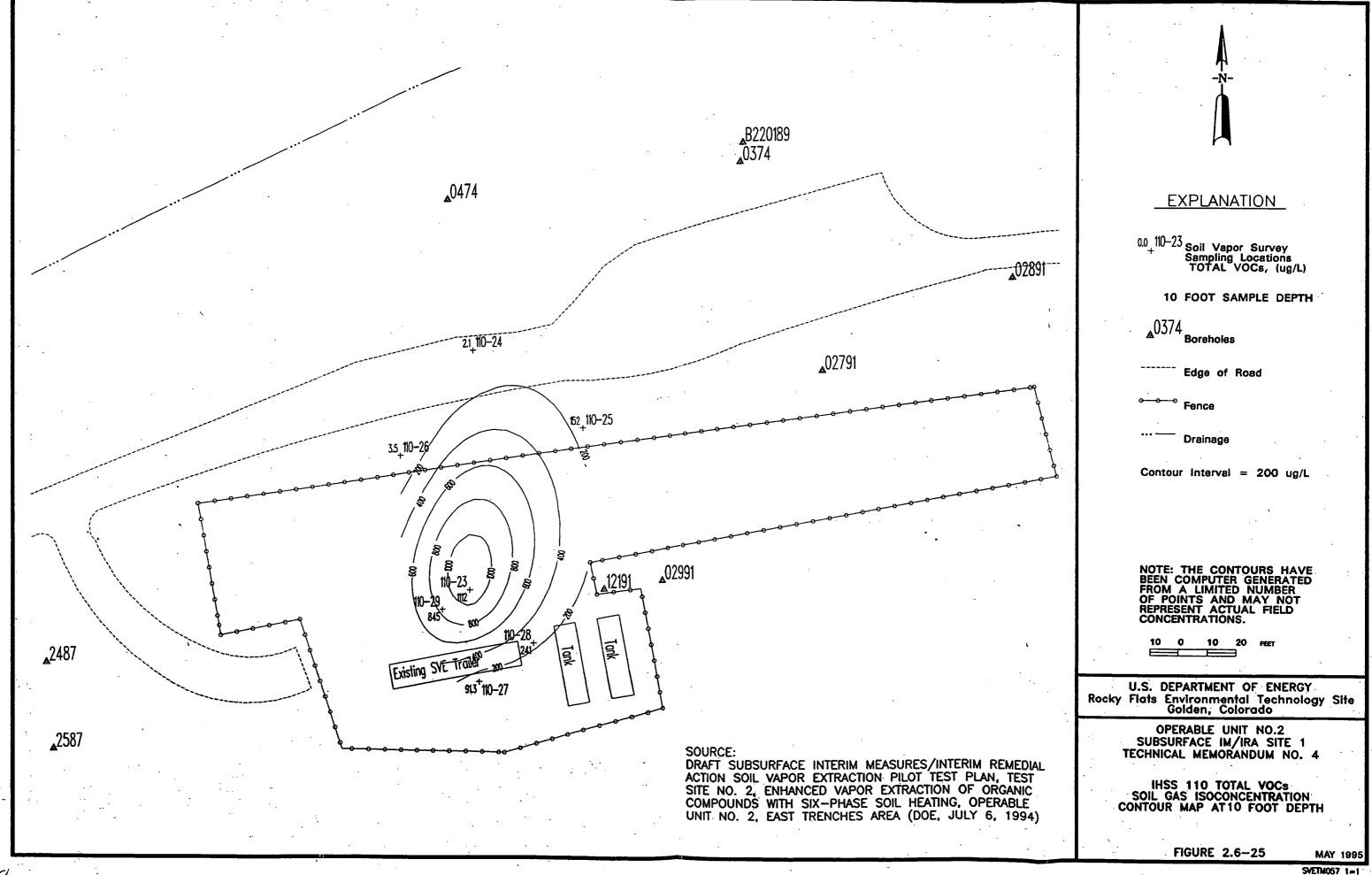
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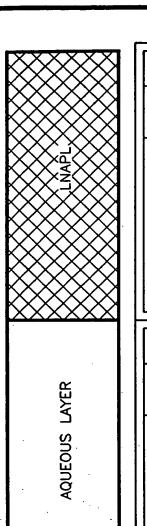












FLOATING LAYER (LNAPL)							
DETECTED VOC ANALYTE	DETECTED SVOC ANALYTE	DETECTED TPH ANALYTE	RADIONUCLIDE SCREEN ANALYTE(2)	AVTIVITY (pCi/L)			
VOC SVOC		GASOLINE(2) DIESEL(3)	GROSS BETA GROSS ALPHA	803,000 749,000			

AQUEOUS LAYER DETECTED DETECTED DETECTED **RADIONUCLIDE** VOC ANALYTE SVOC ANALYTE SCREEN ANALYTE(1) ACTIVITY (pCi/L) TPH **ANALYTE** 2-METHYLPHENOL 4-METHYLPHENOL 2-METHYLNAPHTHALENE GASOLINE(2) DIESEL(3) GROSS BETA GROSS ALPHA **ACETONE** 803,000 METHYLENE CHLORIDE 749,000 1,1-DCA 2-BUTANONE PHENANTHRENE DI-N-BUTYLPHTHALATE CHCI, 1,1,1-TCA BIS(2-ETHYLHEXYL)PHTHALATE TCE PCE ETHYLBENZENE M,P-XYLENE 0-XYLENE

SINKING LAYER (DNAPL)

DNAPL LAYER DISSOLVED DURING SHIPMENT TO LABORATORY

NAPL

- (1) ONE RADIONUCLIDE SCREEN WAS PERFORMED PRIOR TO SHIPMENT ON THE FLOATING OIL AND WATER LAYERS.
- (2) GASOLINE RANGE ORGANICS (C6 THROUGH C12).
- (3) DIESEL RANGE ORGANICS (C12 THROUGH C24).

EXPLANATION

PCI/L = PICOCURIE PER LITER
LNAPL = LIGHT NON-AQUEOUS PHASE LIQUID
DNAPL = DENSE NON-AQUEOUS PHASE LIQUID
VOC = VOLATILE ORGANIC COMPOUND
SVOC = SEMI-VOLATILE ORGANIC COMPOUND
TPH = TOTAL PETROLEUM HYDROCARBON

OTE:
ANALYTE ABBREVIATIONS ARE PRESENTED ON FIGURE 2.6—1

U.S. DEPARTMENT OF ENERGY
Rocky Flats Environmental Technology Site
Golden, Colorado

OPERABLE UNIT 2
SUBSURFACE IM/IRA SITE 1
TECHNICAL MEMORANDUM NO. 4

SUMMARY OF DETECTED ANALYTES FOR LIQUIDS COLLECTED FROM BOREHOLE 25194 IN NOVEMBER 1994

FIGURE 2.6-26

MAY 1995

SVETM068 1=1

•	
LINAPL (1)	
LNAPL (2)	
AQUEOUS LAYER (3)	

FLOATING LAYER	R (1) (LNAPL 1)						
DETECTED VOC ANALYTE	DETECTED SVOC ANALYTE	DETECTED TPH ANALYTE	RADIONUCLIDE SCREEN ANALYTE	ACTIMITY (pCi/L)	SELECTED RADIONUCLIDE	ACTIVITY (pCi/g)	SAMPLE NUMBER
TCE PCE	NAPHTHALENE 2-METHYLNAPHTHALENE PHENANTHRENE DI-N-BUTYLPHTHALATE PYRENE CHRYSENE BIS(2-ETHYLHEXYL)PHTHALATE	GASOLINE(5) DIESEL(6)	GROSS BETA GROSS ALPHA	42,000 19,400	Am-241 Pu-239/240 U-233/234 U-235 U-238	NA NA NA NA	C0639

FLOATING LAYER	R (2) (LNAPL 2)						
DETECTED VOC ANALYTE	DETECTED SVOC ANALYTE	DETECTED TPH ANALYTE	RADIONUCLIDE SCREEN ANALYTE(4)	ACTIMTY (pCi/L)	SELECTED RADIONUCLIDE	ACTIMITY (pCi/g)	SAMPLE NUMBER
TCE PCE	NAPHTHALENE 2-METHYLNAPHTHALENE FLUORENE PHENANTHRENE DI-N-BUTYLPHTHALATE BIS(2-ETHYLHEXYL)PHTHALATE	GASOLINE(5) DIESEL(6)	GROSS BETA GROSS ALPHA	39,400 22,600	Am-241 Pu-239/240 U-233/234 U-235 U-238	0.008 0.029 1.96 0.35 15.5	C0640

AQUEOUS LAYER	R						
DETECTED VOC ANALYTE	DETECTED SVOC ANALYTE	DETECTED TPH ANALYTE	RADIONUCLIDE SCREEN ANALYTE(4)	ACTIVITY (pCi/L)	SELECTED RADIONUCLIDE	ACTIMITY (pCi/g)	SAMPLE NUMBER
TCE PCE	PHENOL 2-METHYLPHENOL 4-METHYLPHENOL 2,4-DIMETHYLPHENOL 2,4-DIMETHYLPHENOL NAPHTHALENE 2-METHYLNAPHTHALENE FLUORENE PHENANTHRENE DI-N-BUTYLPHTHALATE CHRYSENE BIS(2-ETHYLHEXYL)PHTHALATE	GASOLINE(5) DIESEL(6)	GROSS BETA GROSS ALPHA	39,400 22,600	Am-241 Pu-239/240 U-233/234 U-235 U-238	1.62 1.16 398.0 101.0 3,240.0	C0670

DNAPL

SINKING LAYER (DNAPL)

NO SAMPLE WAS COLLECTED IN FIELD

- (1) FLOATING LAYER SEPARATED DURING SAMPLING (SAMPLE NUMBER C0639)
- (2) FLOATING LAYER SEPARATED AT LABORATORY (SAMPLE NUMBER C0640)
- (3) AQUEOUS LAYER SEPARATED AT LABORATORY (SAMPLE NUMBER C0670)
- (4) ONE RADIONUCLIDE SCREEN WAS PERFORMED PRIOR TO SHIPMENT ON THE FLOATING OIL (2) AND WATER LAYERS.
- (5) GASOLINE RANGE ORGANICS (C8 THROUGH C12).
- (6) DIESEL RANGE ORGANICS (C_{12} THROUGH C_{24}).

EXPLANATION

pCi/L = PICOCURIC PER LITER
pCi/g = PICOCURIC PER GRAM
LNAPL = LIGHT NON-AQUEOUS PHASE LIQUID
DNAPL = DENSE NON-AQUEOUS PHASE LIQUID
VOC = VOLATILE ORGANIC COMPOUND
SVOC = SEMI-VOLATILE ORGANIC COMPOUND
TPH = TOTAL PETROLEUM HYDROCARBON
NA = NOT AVAILABLE

NOTE:

ANALYTE ABBREVIATIONS ARE PRESENTED ON FIGURE 2.6-1.

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SUMMARY OF DETECTED ANALYTES FOR LIQUID COLLECTED FROM EXTRACTION WELL 25194 IN DECEMBER 1994

FIGURE 2.6-27

MAY 1995

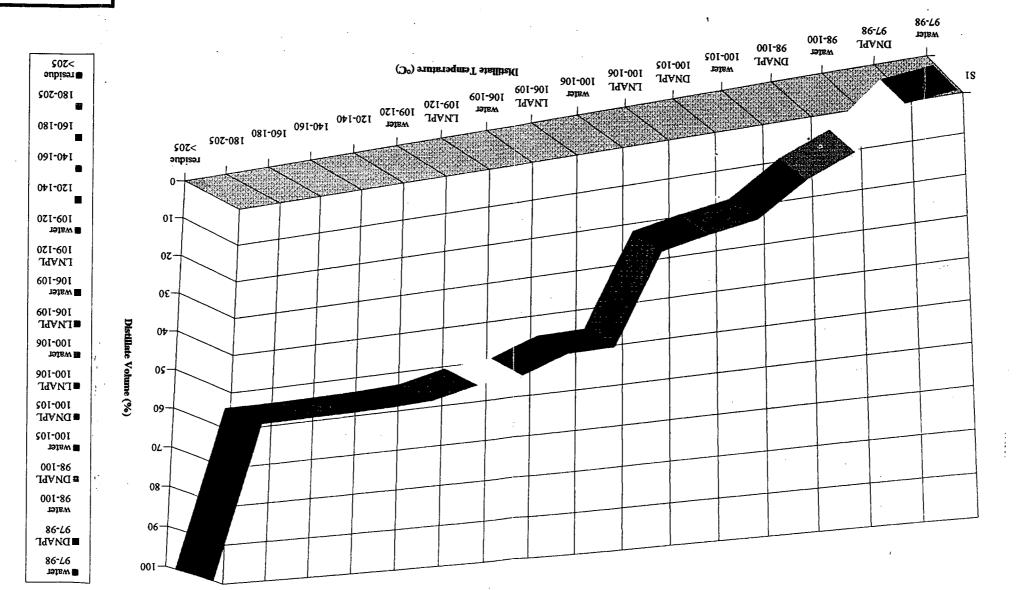
SVETM069 1=1

FIGURE 2.6-28 MAY 1995

DISTILLATE TEST VOLUME VS. TEMPERATURE PLOT

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Service de

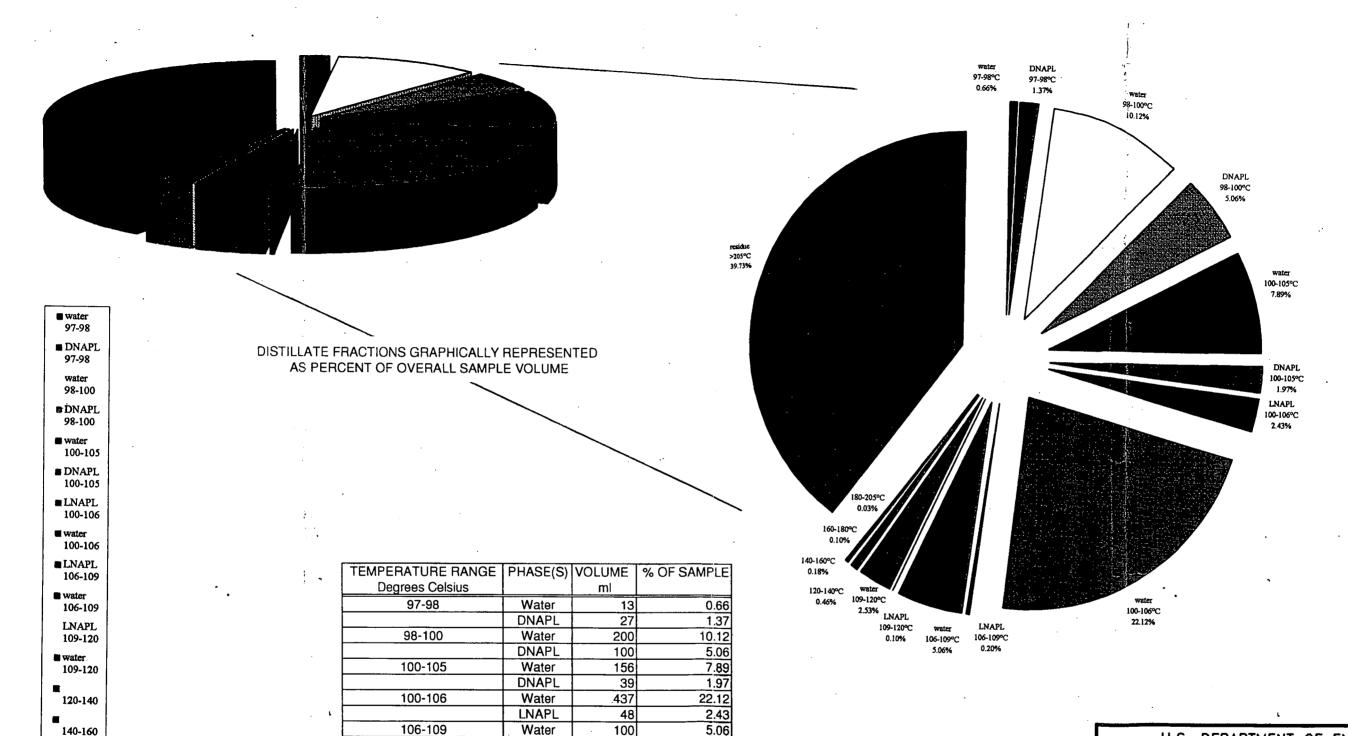
M mining

1. Trans. 2

f. 1. 2.

F ...

C 18



LNAPL

Water

LNAPL

One Phase

One Phase

One Phase

One Phase

Residue

50

3.5

0.5

785

1976.00

2.53

0.1

0.46

0.18

0.1

0.03

39.73

109-120

120-140

140-160

160-180

180-205

>205

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DISTILLATE TEST RESULTS

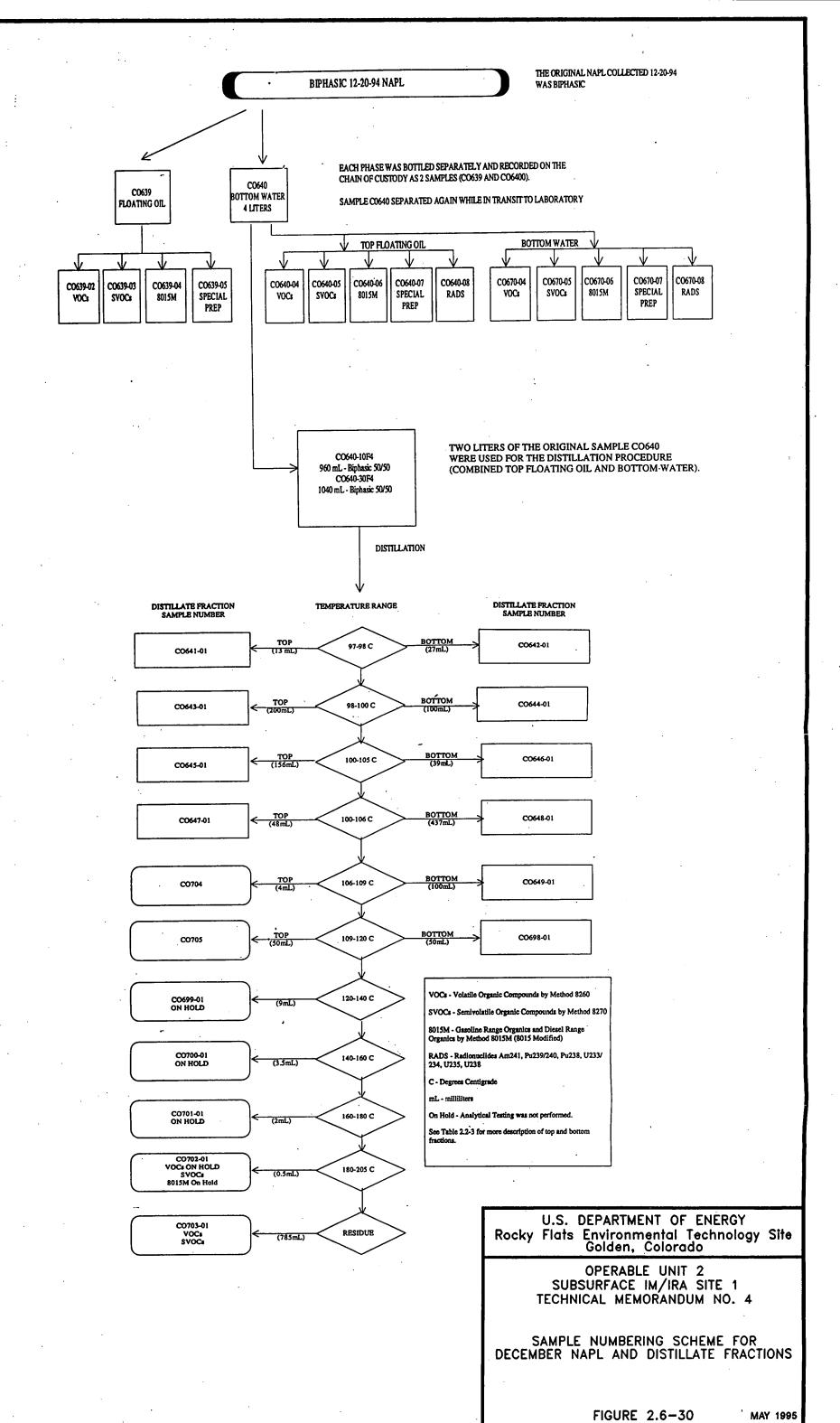
FIGURE 2.6-29

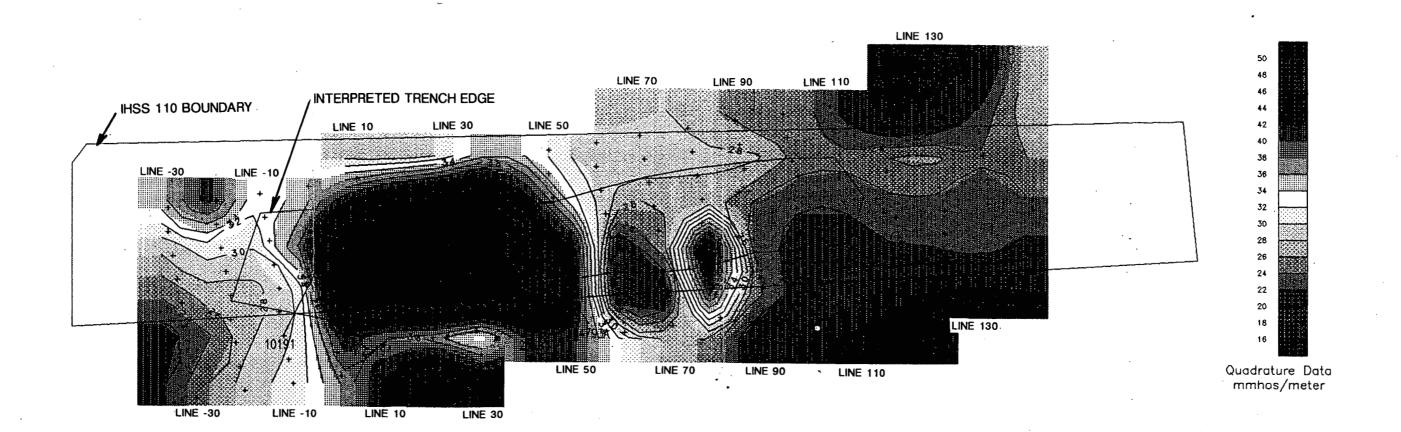
MAY 1995

160-180

180-205

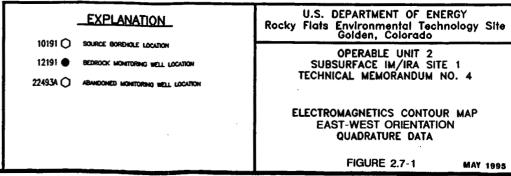
>205

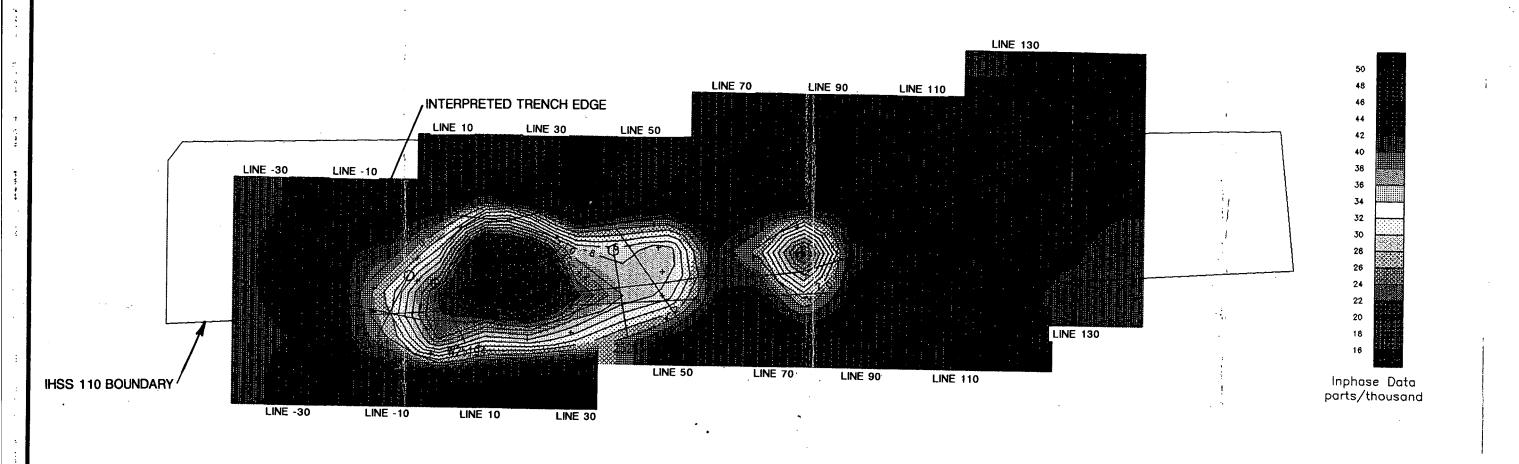




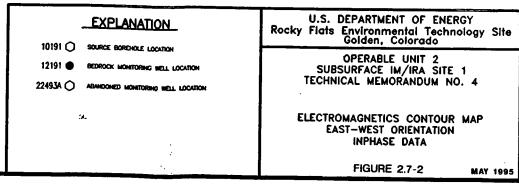
SCALE IN FEET

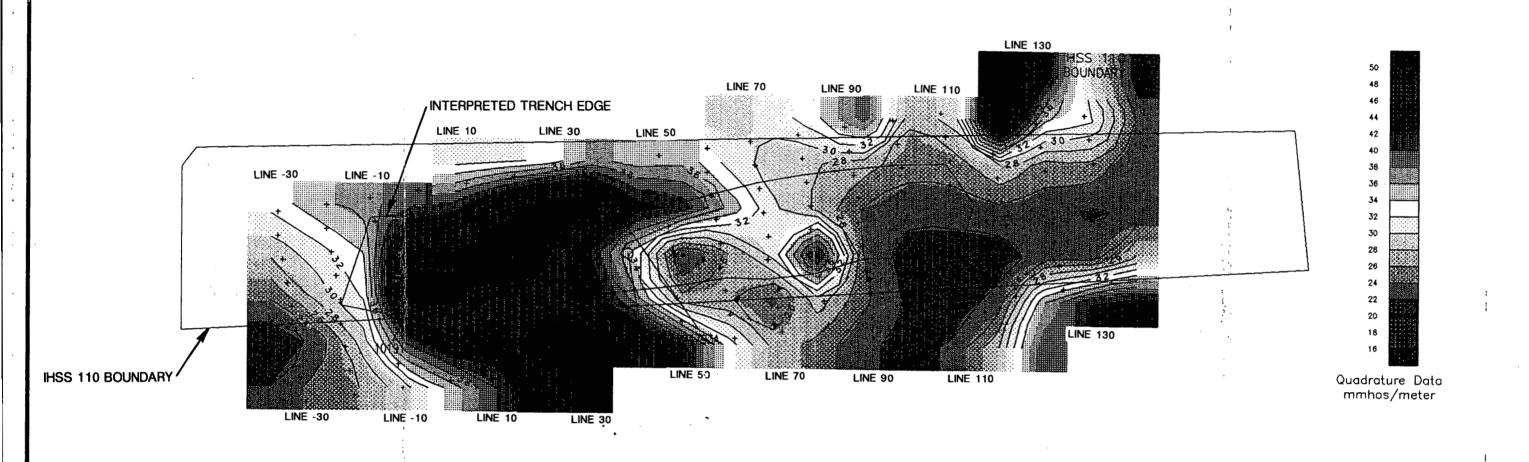






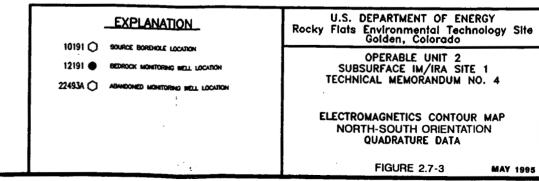
CONTOUR INTERVAL = 2 PARTS/THOUSAND

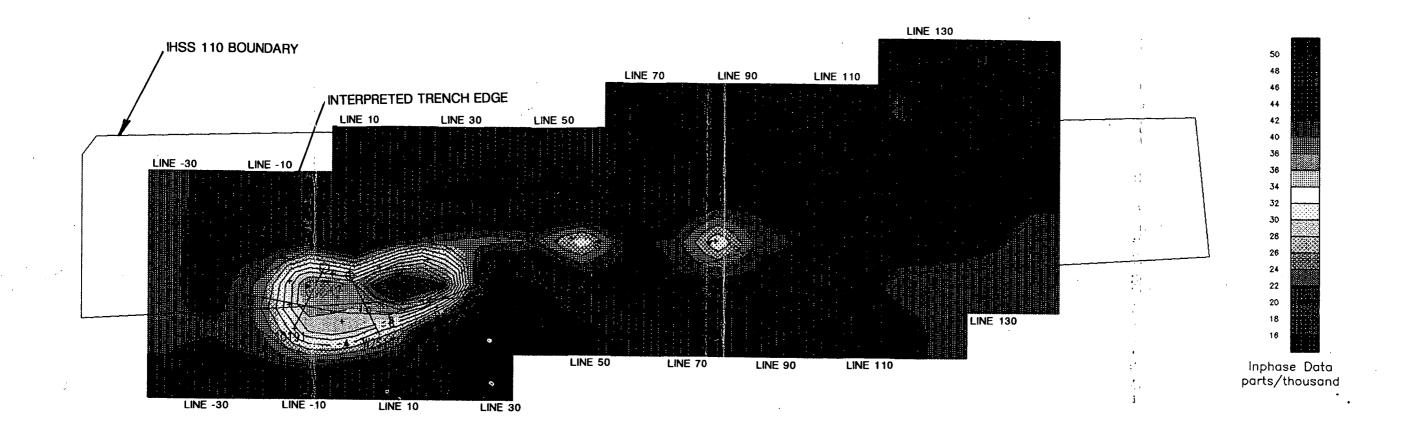


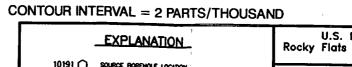


CONTOUR INTERVAL = 2mmhos/meter

SCALE IN FEET







0 10 20 12191 ● 12193 ○ 224934 ○ U.S. DEPARTMENT OF ENERGY Rocky Flats Environmental Technology Site Golden, Colorado

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ELECTROMAGNETICS CONTOUR MAP NORTH-SOUTH ORIENTATION INPHASE DATA

FIGURE 2.7-4

MAY 1995

